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1983 ANNUAL TROPICAL CYCLONE REPORT

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JOINT TYPHOON WARNING CENTER
GUAM, MARIANA ISLANDS

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FOREWORD

The Annual Tropical Cyclone Report is prepared by the staff of the Joint Typhoon Warning Center (JTWC), a combined USAF/USN organization operating under the command of the Commanding Officer, U.S. Naval Oceanography Command Center/Joint Typhoon Warning Center, Guam. JTWC was established in April 1959 when USCINCPAC directed USCINCPACFLT to provide a single tropical cyclone warning center for the western North Pacific region. The operations of JTWC are guided by USCINCPACINST 3140.1 (series).

The mission of the Joint Typhoon Warning Center is multi-faceted and includes:

- l. Continuous meteorological monitoring of all tropical activity in the Northern and Southern Hemispheres, from 180 degrees longitude westward to the east coast of Africa, to anticipate tropical cyclone development.
- Issuing warnings for all significant tropical cyclones in the above area of responsibility.
- Determination or reconnaissance requirements for tropical cyclone surveillance and assignment of appropriate priorities.
- 4. In depth post-storm analysis of all tropical cyclones occurring within the western North Pacific and North Indian Oceans for publication in this report.
- 5. Cooperation with the Naval Environmental Prediction Research Facility, Monterey, California, on the operational evaluation of tropical cyclone models and forecast aids, and the development of new techniques to support operational forecast scenarios.

Should JTWC become incapacitated, the Alternate JTWC (AJTWC), located at the U.S. Naval Western Oceanography Center, Pearl Harbor, Hawaii, assumes warning responsibilities. Assistance in determining satellite reconnaissance requirements, and in

obtaining the resultant data, is provided by Detachment 4, lww, Hickman AFB, Hawaii.

Satellite imagery used throughout this report represents data obtained by the tropical cyclone satellite surveillance network. The personnel of Det 1, lWW, colocated with JTWC at Nimitz Hill, Guam, coordinate the satellite acquisitions and tropical cyclone surveillance by the following units:

Det 5, lWW, Clark AB, RP
Det 8, lWW, Kadena AB, Japan
Det 15, 30WS, Osan AB, Korea
Det 4, lWW, Hickam AFB, Hawaii
Air Force Global Weather Central,
Offutt AFB, Nebraska

In addition, the Naval Oceanography Command Detachment, Diego Garcia, and DMSP equipped U.S. Navy aircraft carriers have been instrumental in providing vital satellite position fixes of tropical disturbances in the Indian Ocean.

In line with the proposals to implement metric units of measurements within the United States over the next few years, various civilian and military organizations have begun extensive educational programs through use of metric equivalents in their publications. This report will include metric unit equivalent measures whenever possible.

A special thanks is extended to the men and women of: 27th Communication Squadron, Operating Location C, for their continuing support by providing high quality, real-time satellite imagery; the Pacific Fleet Audio-Visual Center, Guam, for their assistance in the reproduction of satellite and graphics data for this report; to the Navy Publications and Printing Service Branch Office, Guam, for their efforts to meet publication deadlines; and to Mrs. Bernadita Manipol for her patience and perseverance in typing the many drafts and the final manuscript of the report.

NOTE: Appendix 5 contains information on how to obtain past issues of the Annual Typhoon Report (redesignated Annual Tropical Cyclone Report in 1980).

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CHAPTER I - OPERATIONAL PROCEDURES

1. GENERAL

The Joint Typhoon Warning Center (JTWC) provides a variety of routine services to the organizations within its area of responsibility, including:

- a. Significant Tropical Weather Advisories: issued daily, this product describes all tropical disturbances and assesses their potential for further development;
- b. Tropical Cyclone Formation Alerts: issued when synoptic. satellite and/or aircraft reconnaissance data indicate development of a significant tropical cyclone in a specified area is likely;
- c. Tropical Cyclone Warnings: issued periodically throughout each day for significant tropical cyclones, giving forecasts of position and intensity of the system; and
- d. Prognostic Reasoning Messages: issued twice daily for tropical storms and typhoons in the western North Pacific; these messages discuss the rationale behind the most recent warnings.

The recipients of the services of JTWC essentially determine the content of JTWC's products according to their ever-changing requirements. Thus, the spectrum of the routine services is subject to change from year to year; such changes are usually the result of deliberations held at the Annual Tropical Cyclone Conference.

2. DATA SOURCES

a. COMPUTER PRODUCTS:

A standard array of synoptic-scale computer analyses and prognostic charts are available from the Fleet Numerical Oceanography Center (FLENUMOCEANCEN) at Monterey, California. These products are provided via the Naval Environmental Data Network (NEDN).

b. CONVENTIONAL DATA:

This data set is comprised of land-based and shipboard surface and upper-air observations taken at or near synoptic times, cloud-motion winds derived twice daily from satellite data, and enroute meteorological observations from commercial and military aircraft (ATREPS) within six hours of synoptic times. Conventional data charts are prepared daily at 00002 and 12002 using hand-and computer-plotted data for the surface/gradient and 200 mb (upper-tropospheric) levels. In addition to these analyses, charts at the 850, 700, and 500 mb levels are computer-plotted from rawinsonde/pibal observations for the 12-hour synoptic times.

c. AIRCRAFT RECONNAISSANCE:

Aircraft weather reconnaissance data are invaluable for the position of the center of developing systems and essential for the accurate determination of numerous

parameters, including;

- eye/center temperature and dewpoint
- maximum surface and flight level wind
- minimum sea level pressure
 horizontal wind distribution

In addition, wind and pressure-height data at the 500 and/or 400 mb level, provided by the aircraft while enroute to, or from fix missions, provide a valuable supplement to the all too sparse data fields of JTWC's area of responsibility. A comprehensive discussion of aircraft weather reconnaissance is presented in Chapter II.

d. SATELLITE RECONNAISSANCE:

Meteorological satellite data obtained from Defense Meteorological Satellite Program (DMSP), and National Oceanic and Atmospheric Administration (NOAA), space-craft played a major role in the early detection and tracking of tropical cyclones in 1983. A discussion of the role of these programs is presented in Chapter II.

e. RADAR RECONNAISSANCE:

During 1983, as in previous years, land radar coverage was utilized extensively when available. Once a tropical cyclone moved within the range of land radar sites, their reports were essential for determination of small scale movement. Use of radar reports during 1983 is discussed in Chapter II.

3. COMMUNICATIONS

- a. JTWC currently has access to three primary communications circuits.
- (1) The Automated Digital Network (AUTODIN) is used for dissemination of warnings and other related bulletins to Department of Defense installations. These messages are relayed for further transmission over U.S. Navy Fleet Broadcasts, and U.S. Coast Guard CW (continuous wave Morse code) and voice broadcasts. Inbound message traffic for JTWC is received via AUTODIN addressed to NAVOCEANCOMCEN GUAM or JTWC GUAM.
- (2) The Air Force Automated Weather Network (AWN) provides weather data to JTWC through a dedicated circuit from the Automated Digital Weather Switch (ADWS) at Hickam AFB, Hawaii. The ADWS selects and routes the large volume of meteorological reports necessary to satisfy JTWC requirements for the right data at the right time. Weather bulletins prepared by JTWC are inserted into the AWN circuit via the NEDS and the Nimitz Hill Naval Telecommunication Center (NTCC) of the Naval Communications Area Master Station Western Pacific.
- (3) The Naval Environmental Data
 Network (NEDN) is the communications link
 with the computers at FLENUMOCEANCEN. JTWC
 is able to receive environmental data from
 FLENUMOCEANCEN and access the computers
 directly to run various program.

1

b. The Naval Environmental Display Station (NEDS) has become the backbone of the JTWC communications system; it is the terminal that provides a direct interface with the NEDN and AWN; and it is capable of preparing messages for indirect AUTODIN transmission. The NEDS also provides a means for the Typhoon Duty Officer (TDO) to request forecast aids which are processed on the FLENUMCCEANCEN computers and transmitted to the TDO over the NEDN circuit.

4. ANALYSES

A composite surface/gradient level (3000 ft (915 m)) manual analysis of the JTWC area of responsibility is accomplished on the 0000Z and 1200Z conventional data. Analysis of the wind field using streamlines is stressed for tropical and subtropical regions. Analysis of the pressure field is accomplished routinely by the Naval Oceanography Command Center (NOCC) Operations watch-team and may be used in conjunction with JTWC's analysis of tropical wind fields.

A composite upper-tropospheric manual streamline analysis is accomplished daily utilizing rawinsonde data from 300 mb through 100 mb, winds derived from cloud motion analysis, and AIREPS (plus or minus 6 hours) at or above 29,000 feet (8,839 m). Wind and height data are used to arrive at a representative analysis of tropical cyclone outflow patterns, mid-latitude steering currents, and features that may influence tropical cyclone intensity. All charts are hand-plotted over areas of tropical cyclone activity to provide all available data as soon as possible to the TDO. These charts are augmented by the computer-plotted charts for the final analysis.

Computer-plotted charts for the 850, 700, and 500 mb levels are available for streamline or height-change analyses from the 00002 and 1200Z data base. Additional sectional charts at intermediate synoptic times and auxiliary charts such as station-time plot diagrams and pressure-change charts are also analyzed during periods of significant tropical cyclone activity.

5. FORECAST AIDS

The following objective techniques were employed in tropical cyclone forecasting during 1983 (a description of these techniques is presented in Chapter IV):

a. MOVEMENT

- (1) 12-HR EXTRAPOLATION
- (2) CLIMATOLOGY
- (3) HPAC (Extrapolation/Climatology)
- (4) BPAC (Extrapolation/Climatology)
- (5) CYCLOPS (Steering)
- (6) TYAN78 (Analog)
- (7) ONE-WAY TROPICAL CYCLONE MODEL (Dynamic)
- (8) NESTED TROPICAL CYCLONE MODEL (Dynamic)

- (9) TAPT (Empirical)
- (10) COSMOS (Model Output Statistics)

b. INTENSITY

- (1) THETA E (Empirical)
- (2) WIND RADIUS (Analytical)
- (3) DVORAK (Empirical)

6. FORECAST PROCEDURES

a. INITIAL POSITIONING:

In the preparation of each warning an accurate location (fix) of the tropical cyclone's surface center within two to three hours of warning time is of prime importance. JTWC uses the Selective Reconnaissance Program (SRP) to levy an optimal mix of available resources to obtain the necessary fix information. Whenever a tropical cyclone is poorly defined or the actual surface center cannot be determined, and when conflicting fix information is received, the "best estimate" of the surface location is subjectively determined from the analysis of all available data. If the fix data are not available due to reconnaissance platform malfunctions or communication problems, synoptic data or extrapolation from previous fixes are used. The warning position is then obtained by determining the "best track" of the tropical cyclone up to the last fix, or best estimate of the position of its surface center, and forecasting its movement to the warning time.

b. TRACK FORECASTING:

A preliminary forecast track is developed based on an evaluation of the rationale behind the previous warning and the guidance given by the most recent objective techniques and numerical prognoses. This preliminary track is subjectively modified based on the following considerations:

- (1) The prospects for recurvature or erratic movement are evaluated. This evaluation is based primarily on the present and forecast, positions and amplitudes of the middle-tropospheric, mid-latitude troughs as depicted on the latest upper air analyses and numerical prognoses.
- (2) Determination of the best steering level is partly influenced by the maturity and vertical extent of the tropical cyclone. For mature tropical cyclones located south of the subtropical ridge, forecast changes in speed of movement are closely correlated with anticipated changes in the intensity or relative position of the ridge. When steering currents are relatively weak, the tendency for tropical cyclones to move northward due to internal forces is an important consideration.
- (3) Over the 12- to 72-hour forecast period, speed of movement during the early forecast period is usually biased toward persistence, while the subsequent forecast periods are biased toward objective

techniques. When a tropical cyclone moves poleward, and toward the mid-latitude steering currents, speed of movement becomes increasingly more biased toward a selective group of objective techniques capable of estimating significant increases in speed of movement.

(4) The proximity of the tropical cyclone to other tropical cyclones is closely evaluated to determine if there is a possibility of a Fujiwhara interaction (the apparent rotation of two or more cyclones about a common axis or axes).

A final check is made against climatology to determine whether the forecast track is reasonable. If the forecast deviates greatly from one of the climatological tracks, the forecast rationale may be reappraised.

c. INTENSITY FORECASTING:

In this parameter, heavy reliance is placed on intensity trends from aircraft reconnaissance reports, wind and pressure data from ships and land stations in the vicinity of the tropical cyclone, the Dvorak satellite interpretation model and other objective techniques. An evaluation of the entire synoptic situation is made, including the location of major troughs and ridges, the position and intensity of any nearby tropical upper-tropospheric troughs (TUTT), the vertical and horizontal extent of the tropical cyclone's circulation and the extent of the associated upper-level outflow pattern. An essential element affecting each intensity forecast is the accompanying forecast track and the influence of environmental parameters along that track, such as: sea thermal fronts, terrain influences, vertical wind shear, and an extratropical environment.

Once the forecast intensities have been derived, the horizontal distribution of destructive winds (greater than 30-, 50- and 100-knots) is determined. The most recent wind radii and associated asymmetries are deduced from all available surface wind observations and reconnaissance aircraft reports. Based on the current wind distribution, preliminary estimates of future wind radii are provided by an empirically derived objective technique. These estimates may be subjectively modified based on the anticipated interaction of the tropical cyclone's circulation with forecast locations of large-scale wind regimes and significant landmasses. Other factors including the tropical cyclone's speed of movement and possible extratropical transition are considered.

7. WARNINGS

Tropical cyclone warnings are issued when a definite closed circulation is evident and maximum sustained surface winds are forecast to increase to 34 knots (18 meters per second) within 48 hours, or if the tropical cyclone is in such a position that life or property may be endangered within 72 hours. Warnings may also be issued in other situations if it is determined that there is a need to alert military or civil interests to conditions which may become hazardous in a short period of time.

Each tropical cyclone warning is numbered sequentially and includes the following information: the position of the surface center; estimate of the position accuracy and the supporting reconnaissance (fix) platforms; the direction and speed of movement in the past six hours; the intensity and radial extent of surface winds over 30-, 50-, and 100-knots, when applicable. At forecast intervals of 12-, 24-, 48- and 72-hours, information on the tropical cyclone's anticipated position, intensity and wind radii is also provided.

Warnings in the western North Pacific and North Indian Ocean are issued every six hours valid at standard synoptic times (0000Z, 0600Z, 1200Z and 1800Z). All warnings are released to the communications network no earlier than synoptic time and no later than synoptic time plus two and one half hours so that recipients will have a reasonable expectation of having all warnings "in hand" by synoptic time plus three hours (0300Z, 0900Z, 1500Z and 2100Z).

Warning forecast positions are verified against the corresponding "best track" positions (post-storm analysis to determine actual path). A summary of the verification results from 1983 is presented in Chapter IV.

8. PROGNOSTIC REASONING MESSAGES

For tropical storms and typhoons in the western North Pacific Ocean, prognostic reasoning messages are transmitted following the 0000Z and 1200Z warnings, or whenever the previous reasoning is no longer valid. This plain language message is intended to provide meteorologists with the reasoning behind the latest JTWC forecast.

In addition to this message, prognostic reasoning information applicable to all customers is provided in the remarks section of warnings when significant forecast changes are made or when deemed appropriate by the TDO.

9. SIGNIFICANT TROPICAL WEATHER ADVISORY

This product contains a general, non-technical description of all tropical disturbances in the JTWC area of responsibility and an assessment of their potential for further (tropical cyclone) development. In addition, all tropical cyclones in warning status are briefly discussed. This message is issued by 0600Z daily and is reissued whenever the situation warrants.

10. TROPICAL CYCLONE FORMATION ALERT

Formation alerts are issued whenever interpretation of satellite imagery and other meteorological data indicates that the formation of a significant tropical cyclone is likely. These formation alerts will specify a valid period not to exceed 24 hours and must either be cancelled, reissued, or superseded by a tropical cyclone warning prior to the expiration of the valid time.

CHAPTER II - RECONNAISSANCE AND FIXES

1. GENERAL

The Joint Typhoon Warning Center depends on reconnaissance to provide necessary, accurate, and timely meteorological information in support of each warning. JTWC relies primarily on three reconnaissance platforms: aircraft, satellite, and radar. In data rich areas synoptic data are also used to supplement the above. Optimum utilization of all available reconnaissance resources is obtained through the Selective Reconnaissance Program (SRP); various factors are considered in selecting a specific reconnaissance platform including capabilities and limitations, and the tropical cyclone's threat to life/property afloat and ashore. A summary of reconnaissance fixes received during 1983 is included in Section 6 of this Chapter.

2. RECONNAISSANCE AVAILABILITY

a. Aircraft

Aircraft weather reconnaissance in the JTWC area of responsibility is performed by the 54th Weather Reconnaissance Squadron (54th WRS) located at Andersen Air Force Base, Guam. The 54th WRS is presently equipped with six WC-130 aircraft and, from July through October, is augmented by the 53rd WRS from Keesler Air Force Base, Mississippi, bringing the total number of available aircraft to nine. The JTWC reconnaissance requirements, provided daily throughout the year to the Tropical Cyclone Aircraft Reconnaissance Coordinator (TCARC), include system(s) to be fixed, fix times, and forecast positions for each fix. following priorities are utilized in acquiring meteorological data from reconnaissance aircraft in the western North Pacific area in accordance with USCINCPACINST 3140.1(series):

- (1) Investigative flights and vortex or center fixes.
- (2) Synoptic data acquisition in support of tropical cyclone warnings.
- (3) Supplementary fixes on tropical cyclones.

As in previous years, aircraft reconnaissance provided direct measurements of height, temperature, flight-level winds, sea level pressure, estimated surface wind (when observable), and numerous additional parameters. The meteorological data are gathered by the Aerial Reconnaissance Weather Officers (ARWO) and dropsonde operators of Detachment 4, Hq AWS, who fly with the 54th WRS. These data provide the Typhoon Duty Officer (TDO) with indications of changing tropical cyclone characteristics, radii of associated winds, and current tropical cyclone position and intensity. Another important aspect is the availability of the data for research on tropical cyclone analysis and forecasting.

b. Satellite

Satellite fixes from USAF/USN ground sites and USN ships provide day and night

Interpretation of this satellite imagery provides tropical cyclone positions and estimates of current and forecast intensities through the Dvorak technique.

c. Radar

Land radar provides positioning data on well developed tropical syclones when in the proximity (usually within 175 nm (324 km)) of the radar sites in the Philippines, Taiwan, Hong Kong, Japan, South Korea, Kwajalein, and Guam.

d. Synoptic

In 1983 JTWC also determined tropical cyclone positions based on the analysis of the surface/gradient level synoptic data. These positions were helpful in situations where the vertical structure of the tropical cyclone was weak or accurate surface positions from aircraft were not available due to flight restrictions.

3. AIRCRAFT RECONNAISSANCE SUMMARY

During the 1983 tropical season, the JTWC levied 157 vortex ixes and 53 investigative missions of which 4 were flown into disturbances which did not develop. In addition to the levied fixes, 168 supplemental fixes were also obtained. The average vector error for all aircraft fixes received at the JTWC during 1983 was 13 nm (24 km).

Aircraft reconnaissance effectiveness is summarized in Table 2-1 using the criteria set forth in USCINCPACINST 3140.1 (series).

TABLE 2-1. AIRCRAF EFFECTIVENESS COMPLETED ON TIME EARLY	NUM LEVI	AISSANCE BEF OF ED FIZES	
COMPLETED ON TIME EARLY	LEVI	ED TIZES	PERCENT
COMPLETED ON TIME EARLY	LEVI	ED TIZES	PERCENT
COMPLETED ON TIME EARLY			PERCENT
EARLY		146	
EARLY		140	
		1	93.0
LATE		7	0.6 4.5
MISSED		3	1.9
1113320		,	1.9
			
τα	ΓAL	157	100.0
10.		• • •	100.0
LEVIED	VS. MISS	ED FIXES	
	LEVIED	MISSED	PERCENT
AVERAGE 1965-1970	507	16	2.0
1971	802	61	7.6
1972	624	126	20.2
1973	227	13	5.7
1974	358	30	8.4
1975	217	7	3.2
1976	317	11	3.5
1977	203	3	1.5
1978	290	2	0.7
1979	289	14	4.8
1980	213	4	1.9
1981	201	3	1.5
1982	276	17	6.2
1983	157	3	1.9

4. SATELLITE RECONNAISSANCE SUMMARY

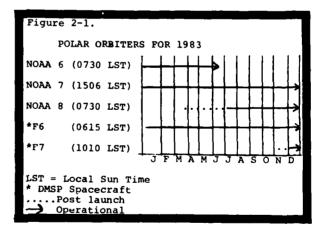
The Air Force provides satellite reconnaissance support to JTWC using imagery from a variety of spacecraft. The tropical cyclone satellite surveillance network consists of both tactical and centralized facilities. Tactical DMSP sites are located at Nimitz Hill, Guam; Clark AB, Republic of the Philippines; Kadena AB, Japan; Osan AB, Korea; and Hickam AFB, Hawaii. sites provide a combined coverage that includes most of the JTWC area of responsibility in the western North Pacific from near the dateline westward to the Malay Peninsula. The Naval Oceanography Command Detachment, Diego Garcia, provides NOAA polar-orbiting coverage in the central Indian Ocean as a supplement to Air Force Global Weather Central (AFGWC) support in this data sparse region. U.S. Navy ships equipped for direct readout also provide supplementary support.

AFGWC, located at Offutt AFB, Nebraska, is the centralized member of the tropical cyclone satellite surveillance network. support to JTWC, AFGWC processes stored imagery from DMSP and NOAA spacecraft. Imagery processed at AFGWC is recorded onboard the spacecraft as it passes over the earth. Later, these data are downlinked to AFGWC via a network of command/readout sites and communications satellites. This enables AFGWC to obtain the coverage necessary to fix all tropical systems of interest to JTWC. AFGWC has the primary responsibility to provide tropical cyclone surveillance over the entire Indian Ocean and portions of the western North Pacific on both sides of the dateline. Additionally, AFGWC can be tasked to provide tropical cyclone positions in the western North Pacific and South Pacific as backup to coverage routinely available in those regions.

The hub of the network is Det 1. lWW, colocated with JTWC on Nimitz Hill, Guam. Based on available satellite coverage, Det 1 coordinates satellite reconnaissance requirements with JTWC and tasks the individual network sites for the necessary tropical cyclone fixes. Therefore, when a position from a polar-orbiting satellite is required as the basis for a warning, called a "levied fix", a dual-site tasking concept is applied. Under this concept, two sites are tasked to fix the tropical cyclone from the same satellite pass. This provides the necessary redundancy to virtually guarantee JTWC a successful satellite fix on the tropical cyclone. Using this dual-site concept, the satellite reconnaissance network is capable of meeting all of JTWC's levied satellite fix requirements.

The network provides JTWC with several products and services. The main service is one of surveillance. Each site reviews its daily satellite coverage for indications of tropical cyclone development. If an area exhibits the potential for development, JTWC is notified. Once JTWC issues either a formation alert or warning, the network is tasked to provide three products: tropical cyclone positions, intensity estimates, and 24-hour intensity forecasts. Satellite tropical cyclone positions are assigned position code numbers (PCN) depending on the availability of geography for precise gridding, and the degree of organization of the tropical cyclone's cloud system (Table During 1983, the network provided JTWC with a total of 1755 satellite fixes on tropical systems in the western North Pacific. Another 70 were made for tropical systems in the North Indian Ocean. parison of those fixes made on numbered tropical cyclones in the western North Pacific with their corresponding JTWC best track positions is shown in Table 2-3. Estimates of the tropical cyclone's current intensity and a 24-hour intensity forecast are made once each day by applying the Dvorak technique (NOAA Technical Memorandum NESDIS 45 as revised) to visual imagery.
A similar technique using enhanced infrared imagery is under development.

Three polar orbiters were available throughout the season. Figure 2-1 shows the status of operational polar orbiters. DMSP F-7 became operational in December and should be of benefit in 1984.



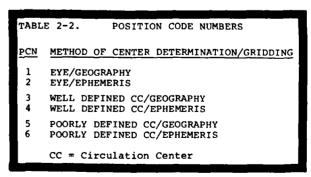


TABLE 2-3.	MEAN DEV	/IATION (NM) OF	ALL SAT	ELLITE	DERIVE	D TROPICAL
	CYCLONE	POSITION	S FROM	THE JTW	C BEST	TRACK	POSITIONS.
		NUMBER	OF CASI	ES (IN P	ARENTH	ESES).	

	WESTERN NORTH	PACIFIC OCEAN	NORTH INDIA	N OCEAN
	1974-1982 AVERAGE	1983	1980-1982	1983
PCN	(ALL SITES)	(ALL SITES)	(ALL SITES)	(ALL SITES)
1	13.5 (537)	13.0 (106)	15.9 (27)	- (0)
2	12.9 (376)	16.7 (24)	9.0 (4)	- (0)
3	19.1 (765)	21.6 (167)	25.1 (9)	19.9 (2)
4	18.2 (413)	22.5 (46)	19.1 (3)	24.4 (2)
5	35.8 (1839)	35.3 (218)	32.9 (65)	33.5 (22)
6	36.2 (1049)	32.3 (88)	35.4 (64)	29.6 (19)
1&2	13.3 (913)	13.7 (130)	15.0 (31)	- (0)
3&4	18.9 (1179)	21.8 (213)	23.6 (12)	22.2 (4)
5&6	36.0 (2888)	34.4 (306)	34.1 (129)	31.7 (41)_

5. RADAR RECONNAISSANCE SUMMARY

Fourteen of the 25 significant tropical cyclones in the western North Pacific during 1983 passed within range of land based radars with sufficient cloud pattern organization to be fixed. The land radar fixes that were obtained and transmitted to JTWC totaled 359.

The WMO radar code defines three categories of accuracy: good (within 10 km (5 nm)), fair (within 10 to 30 km (5 to 16 nm)), and poor (within 30 to 50 km (16 to 23 nm)). This year, 359 radar fixes were coded in this manner; 179 were good, 122 fair, and 58 poor. Compared to the JTWC best track, the mean vector deviation for land radar sites was 17 nm (32 km). Excellent support through timely and accurate radar fix positioning allowed JTWC to track and forecast tropical cyclone movement through even the most difficult and erratic tracks.

As in previous years, no radar reports were received on North Indian Ocean tropical cyclones.

6. TROPICAL CYCLONE FIX DATA

A total of 2541 fixes on 25 western North Pacific tropical cyclone and 70 fixes on three North India. Ocean tropical cyclones were received at JTWC. Table 2-4, Fix Platform Summary, delineates the number of fixes per platform for each individual tropical cyclone. Season totals and percentages are also indicated.

Annex A includes individual fix data for each tropical cyclone. Fix data are divided into four categories: Satellite, Aircraft, Radar, and Synoptic. Those fixes labelled with an asterisk (*) were determined to be unrepresentative of the surface center and were not used in determining the best tracks. Within each category, the first three columns are as follows:

FIX NO. - Sequential fix number

TIME (Z) - GMT time in day, hours and minutes

FIX POSITION - Latitude and longitude to the nearest tenth of a degree

Depending upon the category, the remainder of the format varies as follows:

a. Satellite

- (1) ACCRY Position Code Number (PCN) is used to indicate the accuracy of the fix positon. A "1" indicates relatively high accuracy and a "6" relatively low accuracy.
- (2) DVORAK CODE Intensity evaluation and trend (Figure 2-2, Table 2-5). (For specifics, refer to NOAA TM; NESDIS-45).
- (3) COMMENTS For explanation of abbreviations, see Appendix I.
- $\hspace{1.5cm} \textbf{(4)} \hspace{0.2cm} \textbf{SITE ICAO call sign of the specific satellite tracking station.} \\$

b. Aircraft

- (1) FLT LVL The constant pressure surface level, in millibars or altitude, in feet, maintained during the penetration. The normal level flow in developed tropical cyclones, due to turbulence factors, is 700 mb. Low-level missions are normally flown at 1500 ft (457 m).
- (2) 700 MB HGT Minimum height of the 700 mb pressure surface within the vortex recorded in meters.
- (3) OBS MSLP If the surface center can be visually detected (e.g., in the eye), the minimum sea level pressure is obtained by a dropsonde release above the surface vortex center. If the fix is made at the 1500-foot level, the sea level pressure is extrapolated from that level.
- (4) MAX-SFC-WND The maximum surface wind (knots) is an estimate made by the ARWO based on sea state. This observation is limited to the region of the flight path and may not be representative of the entire tropical cyclone. Availability of data is also dependent upon the absence of

TABLE 2-4. FIX PLATFORM SUMMARY FOR 1983 FIX PLATFORM SUMMARY WESTERN NORTH PACIFIC AI RCRAFT SATELLITE SYNOPTIC RADAR TOTAL (01W) SARAH 49 TIP VERA (02W) (03W) 66 10 103 185 54 184 55 29 STY WAYNE (04W) 86 (05W) (06W) (07W) (08W) STY ABBY TS TS CARMEN 10 BEN 11 6 48 82 20 DOM TS 20 102 TD 09W (09W) 23 85 TY TC ELLEN (10W) 46 153 287 02C (02C) 22 22 25 2 STY FORREST (11W) 66 223 50 43 47 57 TS GEORGIA (12W) HERBERT (13W) 48 TS --3 ----TY (14W) 36 IDA 106 JOE (15W) 60 32 101 KIM (16W) 65 69 LEX (17W) 11 109 96 29 94 72 77 43 MARGE (18W) 123 NORRIS (19W) 36 (20W) 48 ORCHID 37 PERCY (21W) 14 86 RUTH (22W) SPERRY (23W) TS 93 TS 51 THELMA (24W) TOTAL 325 1755 434 27 2542 Z OF TOTAL NR OF FIXES 12.8 69.1 17.1 1.0 100.0 INDIAN OCEAN SATELLITE SYNOPTIC TOTAL TC 01A TC 02B TC 03B 7 23 23 40 40 TOTAL 70 70 Z OF TOTAL NR OF FIXES 100.0 100.0

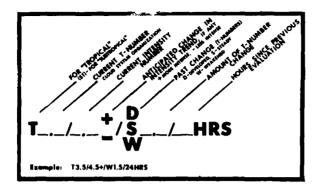


Figure 2-2. The current T-number is 3.5 but the current intensity estimate is 4.5 (equivalent to 17 kt). The cloud system has weakened by 1.5 T-numbers since the previous evaluation conducted 24 hours earlier. The plus (+) symbol indicates an expected reversal of the weakening trend or very little further weakening of the tropical cyclone during the next 24-hour period.

AS A F (CURRE NUMBER	UNCTION OF	WIND SPEED (KT) DVORAK CI & FI ST INTENSITY) M SEA LEVEL
TROPICAL CYCLONE	WIND	MSLP
		(NW PACIFIC)
INTENSITY NUMBER	SPEED	(NW FACIFIC)
1.0	25	
1.5	25	
2.0	30	1003
2.5	35	999
3.0	45	994
3.5	55	988
4.0	65	981
4.5	77	973
5.0	90	964
	102	954
5.5	115	942
6.0		
6.5	127	929
7.0	140	915
7.5	155	900
8.0	170	884

undercast conditions and the presence of adequate illumination. The positions of the maximum flight level wind and the maximum observed surface wind do not necessarily coincide.

(knots) at flight level is measured by the AN/APN 147 doppler radar system aboard the WC-130 aircraft. This measurement may not represent the maximum flight level wind associated with the tropical cyclone because the aircraft only samples those portions of the tropical cyclone along the flight path. In many instances, the flight path is through the weak sector of the tropical cyclone. In areas of heavy rainfall, the doppler radar may track energy reflected from precipitation rather than from the sea surface, thus, preventing accurate wind speed measurement. In obvious cases, such erroneous wind data will not be reported. In addition, the doppler radar system on

the WC-130 restricts wind measurements to drift angles less than or equal to 27 degrees if the wind is normal (perpendicular) to the aircraft heading.

- (6) ACCRY Fix position accuracy. Both navigational (OMEGA and LORAN) and meteorological (by the ARWO)estimates are given in nautical miles.
- (7) EYE SHAPE Geometrical representation of the eye based on the aircraft radar presentation. The eye shape is reported only if the center is 50 percent or more surrounded by wall cloud.
- (8) EYE DIAM/ORIENTATION Diameter of the eye in nautical miles. When an elliptical eye is present, the lengths of the major and minor axes and the orientation of the major axis are respectively listed. When concentric eye walls are present, each diameter is listed.

c. Radar

- (1) RADAR Specific type of platform (land, aircraft, or ship) utilized for fix.
- (2) ACCRY Accuracy of fix position (good, fair, or poor) as given in the WMO ground radar weather observation code (FM20-V).
- (3) EYE SHAPE Geometrical representation of the eye given in plain language (circular, elliptical, etc.).
- (4) EYE DIAM Diameter of eye given in kilometers.
- (5) RADOB CODE Taken directly from WMO ground weather radar observation code FM20-V. The first group specifies the vortex parameters, while the second group describes the movement of the vortex center.
- $\mbox{(6)}$ RADAR POSITION Latitude and longitude of tracking station given in tenths of a degree.
- $\mbox{(7)}$ SITE WMO station number of the specific tracking station.

CHAPTER III - SUMMARY OF TROPICAL CYCLONES

1. WESTERN NORTH PACIFIC TROPICAL CYCLONES

During 1983, the western North Pacific experienced the fifth consecutive year of below average tropical cyclone activity.
Twenty-five tropical cyclones occurred in 1983, six and one-half less than the annual average. Only two significant tropical cyclones failed to develop beyond the tropical depression (TD) stage and eleven tropical storms (TS) failed to reach typhoon intensity. Of the 12 tropical cyclones that developed to typhoon (TY) intensity, four reached the 130 kt (67 m/s) intensity necessary to be classified as super typhoons (STY). In the western North Pacific, tropical cyclones reaching tropical storm intensity or greater are assigned names in alphabetical order from

a list of alternating male/female names (refer to Appendix 3). Table 3-1 provides a summary of key statistics for western North Pacific tropical cyclones. Each tropical cyclone's maximum surface wind (in knots) and minimum observed sea level pressure (in millibars) were obtained from best estimates based on all available data. The distance traveled (in nautical miles) was calculated from the JTWC official best tracks (see Annex A).

Tables 3-2 through 3-5 provide further information on the monthly distribution of tropical cyclones and statistics on Tropical Cyclone Formation Alerts and Warnings.

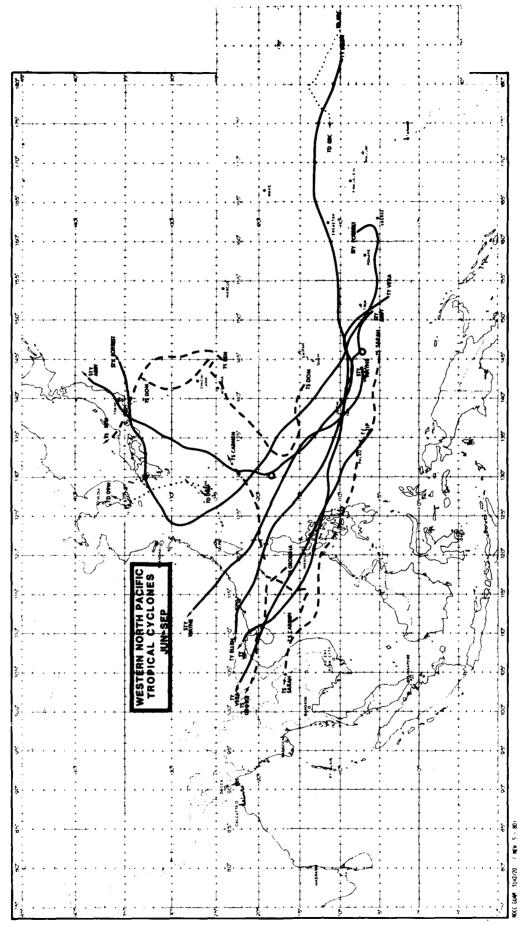
TABLE 3-1. WESTERN NORTH PACIFIC									
1983 SIGNIFICANT	TROPICAL CYCLONES								
TROPICAL CYCLONE	PERIOD OF WARNING	CALENDAR DAYS OF WARNING	NUMBER OF WARNINGS ISSUED	MAXIMUM SURFACE WINDS (KT)	OBSERVED MSLP (MB)	BEST TRACK DISTANCE TRAVELED (NM)			
01w TS SARAH	24 JUN - 26 JUN	3	6	35	999	1948			
02C TC 02C	31 AUG - 2 SEP	3	5	30	1010	773			
02W TY TIP	10 JUL - 13 JUL	4	14	65	978	1206			
03W TY VERA	12 JUL - 18 JUL	7	25	90	952	2546			
04W STY WAYNE	22 JUL - 25 JUL	4	14	135	920	1739			
05W STY ABBY	5 AUG - 17 AUG	13	51	145	888	2031			
06W TS CARMEN	12 AUG ~ 15 AUG	4	11	45	992	1186			
07W TS BEN	12 AUG ~ 15 AUG	4	12	50	989	968			
08W TS DOM	19 AUG - 26 AUG	8	23	55	995	1859			
09W TD 09W	26 AUG - 27 AUG	2	4	30	996	522			
10W TY ELLEN	29 AUG - 9 SEP	12	47	125	928	1462			
11W STY FORREST	20 SEP - 29 SEP	10	32	150	883	2191			
12W TS GEORGIA	29 SEP ~ 1 OCT	3	11	55	987	825			
13W TS HERBERT	7 OCT ~ 8 OCT	2	8	50	987	445			
14W TY IDA	7 OCT ~ 11 OCT	5	15	65	973	1889			
15W TY JOE	10 OCT - 13 OCT	4	15	65	975	1654			
16W TS KIM	16 OCT ~ 20 OCT	5	3	40	993	1224			
17W TY LEX	22 OCT - 26 OCT	5	18	70	971	718			
18W STY MARGE	31 OCT ~ 7 NOV	8	27	145	896	2370			
19W TS NORRIS	9 NOV - 11 NOV	3	7	50	994	721			
20W TY ORCHID	17 NOV ~ 27 NOV	1.	38	125	928	2214			
21W TY PERCY	19 NOV - 24 NOV	6	23	70	970	1123			
22W TS RUTH	23 NOV - 30 NOV	8	16	60	993	1615			
23W TS SPERRY	2 DEC ~ 5 DEC	4	10	55	996	350			
24W TS THELMA	16 DEC ~ 18 DEC	3	10	55	990	1165			
	1983 TOTALS:	111*	445						
* OVERLAPPING DA	AYS INCLUDED ONLY ON	ICE IN SUM							

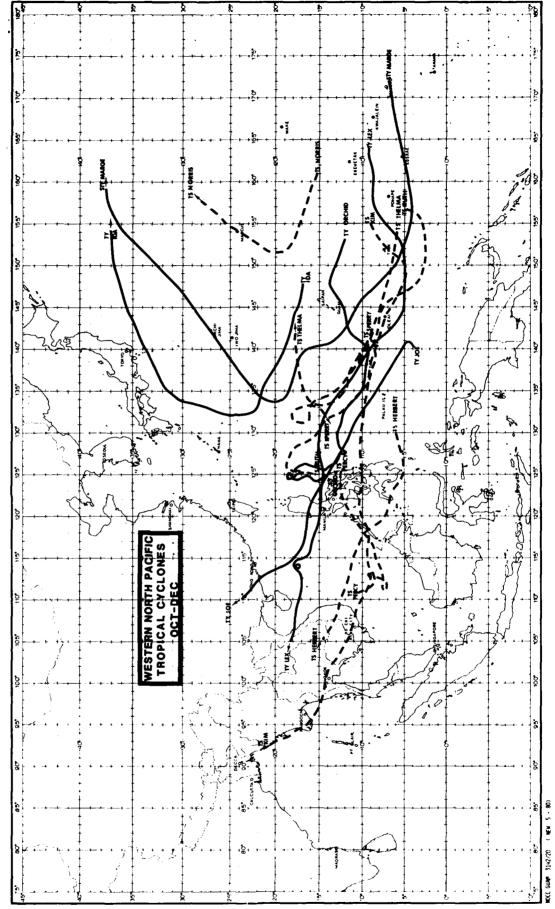
TABLE 3-2. WESTERN	1983 SIGNIFICANT TROPICAL CYCLONES WESTERN														
	<u>JAN</u>	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL	(1959-1 AVERAGE	
TROPICAL DEPRESSIONS	0	0	0	0	0	0	0	2	0	0	0	0	2	3.9	93
TROPICAL STORMS	3 0	0	0	0	0	1	0	3	1	2	2	2	11	9.7	232
TYPHOONS	0	0	0	0	0	0	3	2	1	4	2	0	12	17.8	428
ALL TROPICAL CYCLONES	0	0	0	0	0	1	3	7	2	6	4	2	25	31.4	753
1959-1982		PREVIOUS													
AVERAGE	. 5	. 3	. 8	.9	1.4	2.0	5.0	6.2	5.9	4.4	2.6	1.4	31.4	24-¥	EAR
CASES	13	8	18	22	33	48	119	149	142	105	63	33	753	ніст	ORY
FORMATION ALERTS: 25 of 31 Formation Alerts developed into significant tropical cyclones. Tropical Cyclone Formation Alerts were issued for all significant tropical cyclones that developed during 1983.															
WARNINGS:	Number of warning days: 111														
	Number of warning days with two tropical cyclones in region: 18														
	Number of warning days with three or more tropical cyclones in region: 6														

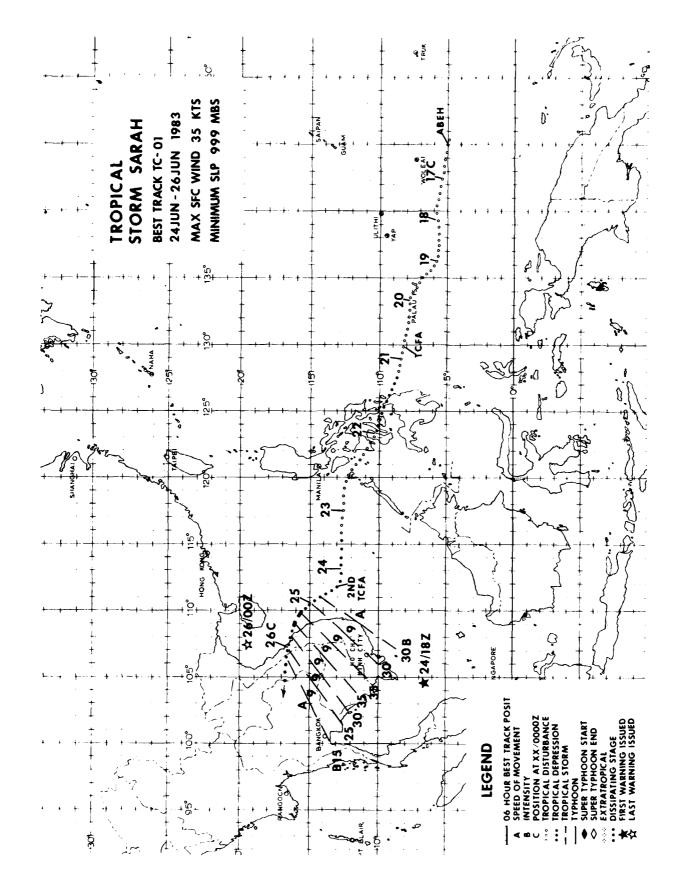
FREQUENCY OF TYPHOONS BY MONTH AND YEAR YEAR JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC TOTAL (1945-1958) AVERAGE .4 .1 .3 .4 .7 1.1 2.0 2.9 3.2 2.4 2.0 .9 16.3 1959 0 0 0 0 1 0 0 1 5 3 3 2 2 17 1960 0 0 0 1 0 2 2 8 0 4 1 1 1 19 1961 0 0 1 0 2 1 3 3 5 3 1 1 20 1962 0 0 0 1 2 2 5 7 2 4 3 0 24 1963 0 0 0 0 1 1 2 2 5 7 3 3 4 0 2 19 1964 0 0 0 0 1 2 2 6 3 5 3 3 4 1 26 1965 1 0 0 1 2 2 6 3 5 3 3 4 1 26 1966 0 0 0 0 1 2 2 6 3 5 3 3 0 2 19 1966 0 0 0 1 2 2 1 3 3 5 3 1 1 20 1967 0 0 1 2 2 4 3 5 2 1 0 21 1968 0 0 0 0 1 2 1 3 3 6 4 2 0 1 20 1968 0 0 0 1 1 1 0 1 3 4 4 3 3 0 20 1969 1 0 0 0 1 1 0 1 3 4 4 3 3 0 20 1969 1 0 0 0 1 1 1 1 1 1 1 4 3 5 4 0 20 1969 1 0 0 0 1 1 1 0 1 3 4 4 3 3 1 0 12 1970 0 1 0 0 0 1 0 0 2 3 2 3 2 3 1 0 13 1970 0 0 1 0 0 0 1 0 0 2 3 2 2 2 2 2 2 2 1973 0 0 0 0 0 1 1 1 4 4 3 4 2 2 22 1973 0 0 0 0 0 1 1 1 4 4 3 4 2 2 22 1973 0 0 0 0 0 1 2 1 2 2 2 4 0 0 1 20 1970 1 0 0 0 0 1 0 0 0 1 0 4 2 2 1 1 1 0 15 1977 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1	TABLE 3-3.				_					_	_			
YEAR (1945-1958) JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC TOTAL (1945-1958) .4 .1 .3 .4 .7 1.1 2.0 2.9 3.2 2.4 2.0 .9 16.3 1959 0 0 0 1 0 0 1 5 3 3 2 2 17 1960 0 0 0 1 0 2 1 3 3 2 2 17 1960 0 0 0 1 0 2 1 3 3 5 3 1 1 20 1961 0 0 1 0 2 1 3 3 5 3 1 1 20 1962 0 0 0 1 1 2 0 4 1 26 1963 0 0 0 1 2 2 4 3 5 <td>TABLE 3-3.</td> <td></td> <td>F</td> <td>PFOLIE</td> <td>NCV O</td> <td>ድ ጥ∨ኮ</td> <td>иоомс</td> <td>BV M</td> <td>ONTH</td> <td>AND V</td> <td>FAD</td> <td></td> <td></td> <td></td>	TABLE 3-3.		F	PFOLIE	NCV O	ድ ጥ∨ኮ	иоомс	BV M	ONTH	AND V	FAD			
(1945-1958) AVERAGE .4 .1 .3 .4 .7 1.1 2.0 2.9 3.2 2.4 2.0 .9 16.3 1959			•	KEQUE	NCI O		1100113	DI 11	ONTIN	AIRD I	DAIN			
AVERAGE	YEAR	<u>JAN</u>	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1959	(1945-1958)													
1960	AVERAGE	. 4	.1	. 3	. 4	.7	1.1	2.0	2.9	3.2	2.4	2.0	.9	16.3
1961			0		1	0						2		
1962		-												
1963														
1964 0 0 0 0 0 2 2 6 3 5 3 4 1 26 1965 1 0 0 1 2 2 2 4 3 5 2 1 0 21 1966 0 0 0 1 2 1 3 6 4 2 0 1 20 1967 0 0 1 1 0 1 3 4 3 3 0 20 1968 0 0 0 1 1 1 1 1 4 3 5 4 0 20 1969 1 0 0 1 0 0 2 3 2 3 1 0 13 1970 0 1 0 0 0 1 0 4 2 3 1 0 12 1971 0 0 0 0 3 1 2 6 3 5 3 1 0 12 1972 1 0 0 0 0 1 1 4 4 3 4 2 2 22 1973 0 0 0 0 0 1 1 4 4 3 4 2 2 22 1973 0 0 0 0 0 0 1 2 1 2 1 2 3 4 2 0 14 1975 1 0 0 0 0 0 1 2 1 2 1 2 3 4 2 0 14 1976 1 0 0 0 1 2 2 2 2 1 4 1 1 0 15 1977 0 0 0 0 0 0 0 0 0 1 3 4 3 2 0 15 1978 0 0 0 0 1 2 2 2 2 1 4 1 1 0 15 1979 1 0 1 1 0 0 0 2 2 2 2 3 2 1 1 1 1978 0 0 0 0 0 0 0 0 2 2 2 3 2 1 1 1 1978 0 0 0 0 0 0 0 2 2 2 2 3 2 1 1 1 1980 0 0 0 0 0 2 0 3 2 5 2 1 0 15 1981 0 0 1 0 0 2 2 2 2 4 1 2 2 16 1982 0 0 2 0 1 1 2 2 5 3 3 1 1 19 1983 0 0 0 0 0 0 0 0 0 3 2 1 4 2 0 12											-	-		
1965												-		
1966	1964	0	0	0	0	2	2	6	3	5	3	4	1	26
1966	1965	1	0	0	1	2	2	4	3	5	2	1	0	21
1967			-	_			_	3				0	1	20
1969							ī	3	4	4		3	0	20
1970	1968	Ó	Ō	0	1	1	1	1	4			4	0	
1971	1969	1	0	0	1	0	0	2	3	2	3	1	0	
1972	1970	0	1	0	0	0	1	0	4	2	3	1	0	12
1973		0	0	0	3	1		6			3			
1974 0 0 0 0 0 1 2 1 2 3 4 2 0 14 1975 1 0 0 0 0 0 0 1 3 4 3 2 0 15 1976 1 0 0 1 2 2 2 1 4 1 1 0 15 1977 0 0 0 0 0 0 0 3 0 2 3 2 1 11 1978 0 0 0 0 1 0 0 3 2 4 3 2 0 15 1979 1 0 1 1 0 0 2 2 3 2 1 1 14 1980 0 0 0 0 2 0 3 2 5 2 1 1 1 14 1980 0 0 0 0 2 2 3 2 1 1 1 14 1981 0 0 1 0 0 2 2 2 3 2 1 1 1 14 1982 0 0 0 2 0 1 1 2 2 2 16 1982 0 0 2 0 1 1 2 5 3 3 1 1 19 1983 0 0 0 0 0 0 0 3 2 1 4 2 0 12 (1959-1983)		1	0	0	0	1	1	4			-			
1975						-		-			•	_	-	
1976					-						-		-	
1977		_		-	-	_				-			-	
1978 0 0 0 1 0 0 3 2 4 3 2 0 15 1979 1 0 1 1 0 0 2 2 3 2 1 1 14 1980 0 0 0 0 0 2 0 3 2 5 2 1 0 15 1981 0 0 1 0 0 2 2 2 4 1 2 2 16 1982 0 0 2 0 1 1 2 5 3 3 1 1 19 1983 0 0 0 0 0 0 0 3 2 1 4 2 0 12 (1959-1983)	1976	1	0	0	1	2	2	2	1	4	1	1	0	15
1979	1977	0	0	0	0	0	0							
1980 0 0 0 0 2 0 3 2 5 2 1 0 15 1981 0 0 1 0 0 2 2 2 4 1 2 2 16 1982 0 0 2 0 1 1 2 5 3 3 1 1 19 1983 0 0 0 0 0 0 3 2 1 4 2 0 12 (1959-1983)				_		-	-			_		_	-	
1981 0 0 1 0 0 2 2 2 4 1 2 2 16 1982 0 0 2 0 1 1 2 5 3 3 1 1 19 1983 0 0 0 0 0 0 0 3 2 1 4 2 0 12 (1959-1983)		_		-	_	-	-					-	_	
1982 0 0 2 0 1 1 2 5 3 3 1 1 19 1983 0 0 0 0 0 0 3 2 1 4 2 0 12 (1959-1983)		-			-									
1983 0 0 0 0 0 0 3 2 1 4 2 0 12 (1959-1983)					-	-				•				
(1959–1983)		_				_					-			
	1983	0	0	0	0	0	0	3	2	1	4	2	0	12
AVERAGE .2 .04 .2 .6 .8 .9 2.8 3.3 3.2 3.0 1.6 .6 17.4														
	AVERAGE	. 2	.04	. 2	. 6	.8	. 9	2.8	3.3	3.2	3.0	1.6	.6	17.4
CASES 6 1 6 15 20 23 69 83 81 76 40 15 435	CASES	6	1	6	15	20_	23	69	83	81	76	40	15	_435

TABLE 3-4.								_					
	FREQUE	NCY O	F TRO	PICAL	STOR	MS AN	D TYP	HOONS	BY N	ONTH	AND Y	EAR	
YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
(1945-1958)													
AVERAGE	. 4	. 1	. 4	.5	. 8	1.3	3.0	3.9	4.1	3.3	2.7	1.1	21.6
1959	0	1	1	1	0	0	3	6	6	4	2	2	26
1960	0	0	0	1	1	3	3	10	3	4	1	1	27 31
1961	1	1	1	1	3	2	5 6	4 7	6 3	5 5	1	1 2	30
1962 1963	0	1 0	0	1 1	2 1	0 3	4	3	5	5	0	3	25
1964	Ö	Ŏ	Ö	ō	2	2	7	9	7	6	6	í	40
1965	2	2	1	1	2	3	5	6	7	2	2	1	34
1966	0	0	0	1	2	1	5	8	7	3	2	1	30
1967	1	0	2	1	1	1	6	8	7	4	3	1	35
1968	0	0	0	1	1	1	3	8	3	6	4	0	27 19
1969	1	Ō	1	1	0	0	3 2	4 6	3 4	3 5	2 4	1 0	24
1970	0	1	0	0	0	2	2	6	4	5	4	U	24
1971	1	0	1	3	4	2	8	4	6	4	2	0	35
1972	1	0	0	0	1	3	6	5	4	5	2	3	30
1973	0	0	0	0	0	0	7	5	2	4	3 4	0	21 32
1974	1	0	1	1 0	1 0	4 0	4 2	5 4	5 5	4 5	3	2 0	20
1975 1976	1 1	1	0	2	2	2	4	4	5	1	i	2	25
1976	1	•	Ū	2	2	-	•	•	,	•	-	~	~~
1977	0	0	1	0	0	1	4	1	5	4	2	1	19
1978	1	0	0	1	0	3	4	7	5	4	3	0	28
1979	1	0	1	1	1	0	4	2	7	3	2	2	24 24
1980	0	0	0 1	1	4	1	4 5	2 7	6 4	4 2	1	1 2	24 28
1981 1982	0	0	3	2 0	1	2 3	4	5	5	3	1	1	26
1982	Ö	Ö	0	0	0	1	3	5	2	5	5	2	23
(1959-1983)													
AVERAGE	.5	. 3	.6	. 8	1.2	1.6	4.4	5.4	4.9	4.0	2.5	1.2	27.3
CASES	12	7	14	21	29	40	111	135	122	100	62	30	683

TABLE 3-5.												
li.	FORMATION ALERT SUMMARY											
		WESTERN NORTH PA	ACIFIC									
<u>YEAR</u>	NUMBER OF ALERT SYSTEMS	ALERT SYSTEMS WHICH BECAME NUMBERED TROPICAL CYCLONES	TOTAL NUMBERED TROPICAL CYCLONES	DEVELOPMENT RATE								
1972	41	29	32	71%								
1973	26	22	23	85%								
1974	35	30	36	86%								
1975	34	25	25	74%								
1976	34	25	25	74%								
1977	26	20	21	77%								
1978	32	27	32	84%								
1979	27	23	28	85%								
1980	37	28	28	76%								
1981	29	28	29	97%								
1982	36	26	28	72%								
1983	31	25	25	81%								
(1972-1983) AVERAGE	32.3	25.7	27.7	808								
CASES	388	308	332									







The formation of Tropical Storm Sarah in the South China Sea during late June marked the beginning of the 1983 tropical cyclone season for the northwestern Pacific. This was the latest season-opener since 1973 when JTWC issued its first warning of the year in July.

The disturbance that was to eventually spawn Sarah was first detected using satellite imagery on 16 June. It was described on that day in the Significant Tropical Weather Advisory (ABEH PGTW) as a poorly organized area of convection centered near 5N 145E.

An upper-level trough located 600 nm (1111 km) to the northwest contributed to the formation of an area of strong upper-level divergence which appeared to be associated with the convection. As the upper-level trough pushed westward over the next few days, the area of enhanced convection maintained its relative position to the southeast and moved west as well.

It was not until the 19th that a weak surface circulation became apparent from satellite imagery near 6N 136E in the low-level easterly flow. This circulation was located along the southern tip of a narrow band of heavy convection extending northward to near the position of the upper-level trough. As the circulation moved westward, the strongest area of convection remained well to the north. A TCFA was issued at 201930Z when it became apparent from satellite imagery that the convection had become more organized around the circulation and that an upper-level anticyclone had developed over the system. However, the ensuing daylight aircraft investigative mission, at 210025Z found only a weakly defined, 1009 mb surface circulation with winds in excess of 15 kt (8 m/s) observed only in the trade wind flow to the north of the circulation.

Convective activity associated with the circulation persisted and increased sharply as the circulation approached the northern tip of Mindanao. The system was continued

in alert status and monitored closely as it crossed the southern Philippines. Synoptic data during this interval indicated the presence of a weak 10-15 kt (5-8 m/s) disturbance which was difficult to track as it crossed the islands. The formation alert was cancelled at 220445Z when satellite imagery indicated that the system had lost its upper-level anticyclone and that its convection had broken up over the mountainous terrain.

Over the next two days the remaining weak surface circulation was observed moving westward into the South China Sea. Convection associated with the circulation was unorganized and strong upper-level northeasterly flow presented a shearing environment that was not considered favorable for further development.

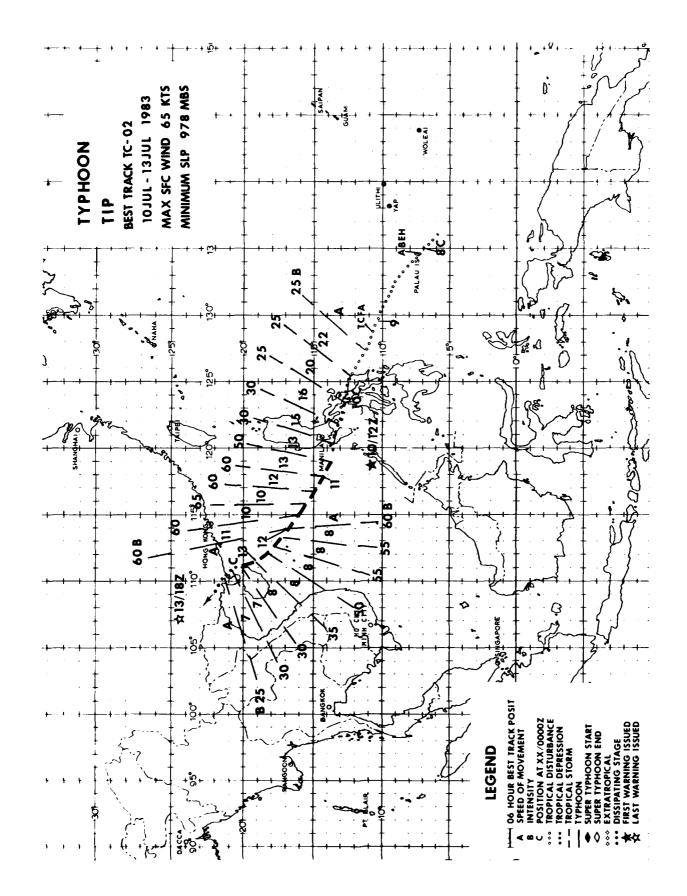
The third, and final, formation alert on this system was issued at 240930Z after convective activity associated with the circulation underwent a marked increase in intensity and organization. Continued intensification, evident from satellite imagery, combined with synoptic reports indicating the presence of 25-30 kt (13-15 m/s) winds, prompted the issuance of the first warning of the 1983 season at 241830Z.

Tropical Storm intensity was reached 12 hours later as Sarah drifted northwestward toward Vietnam. Figure 3-01-1 shows Sarah near maximum intensity off the coast of Vietnam. Further intensification was prevented by intense vertical shear-satellite-derived winds up to 45 kt (23 m/s) over the system--which displaced Sarah's convection to the west.

Under the effects of this hostile shearing environment, Sarah was not able to maintain vertical organization and weakened while approaching the coast of Vietnam. The final warning was issued at 260300Z as Sarah, a fully exposed low-level circulation moved inland north of Hue and dissipated rapidly.



Figure 3-01-1. Tropical Storm Sarah at maximum intensity approaching the coast of Vietnam.



During late June and early July several tropical disturbances were monitored by JTWC. All of these, with the exception of Tropical Storm Sarah (01W), originated in the Philippine Sea and moved westward without developing into significant tropical cyclones. The combination of the rugged Philippine terrain and strong upper-level flow in the South China Sea was sufficient deterrent to development.

On 8 July another disturbance became evident in the Philippine Sea as a persistent area of convective activity near 8N 134 E. Synoptic data indicated that the disturbance was poorly organized with an MSLP of 1008 mb.

On the following day, the disturbance was located near 11N 129E and appeared somewhat more organized on satellite imagery. A weather reconnaissance aircraft on an investigative mission east of Samar was unable to locate a closed circulation, but found a broad area of low presures with maximum surface winds of 25 kt (13 m/s) and MSLP of 1004 mb. In spite of the apparent absence of a well defined surface circulation, a TCFA was issued at 090841Z. The alert was issued because the disturbance was entering an area of strong upper-level divergence associated with a TUTT cell to the northeast. JTWC continued to monitor this disturbance as it moved rapidly across the Philippines, however synoptic data from Philippine land stations indicated that the disturbance remained loosely organized.

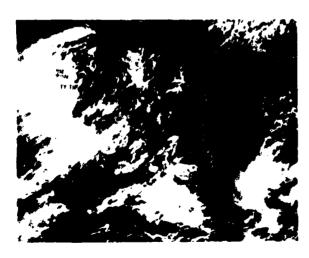


Figure 3-02-1. Typhoon Tip at maximum intensity in the South China Sea. Note the effects of the strong upper-level flow, displacing Tip's convection to the southwest and exposing the low-level circulation (1106442 NOAA 7 visual imagery).

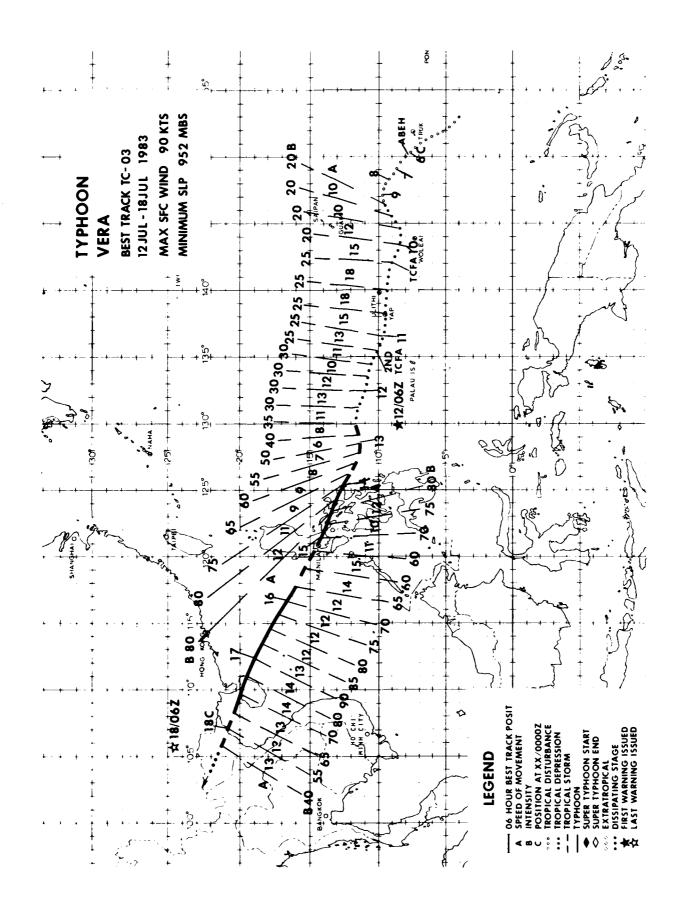
The first warning was issued as the disturbance, now tropical depression 02W, entered the South China Sea north of Mindoro. Synop, ic data indicated the presence of a well defined surface circulation with 30 kt (15 m/s) winds and MSLP of 998 mb. From the initial warning, movement to the northwest toward Hainan Island was forecast, with continued intensification and then weakening late in the period. This forecast scenario was based on the expectation that the midlevel easterly steering currents and strong vectical shear in the area whould persist through the forecast period.

Tip lived up to expectations, moving as expected and achieving typhoon intensity at 111200Z. Figure 3-02-1 shows Tip near maximum intensity on the 11th. The effects of the strong upper-level flow are apparent as Tip appears as an exposed low-level circulation with its convection displaced to the southwest. The circulation appearing on the right hand side of the picture is the disturbance which later developed into Typhoon Vera (03W). Figure 3-02-2 is the 200 mb analysis for the area at the time of Tip's maximum intensity. Note the strong northeasterly flow over Tip and the divergent area in which Tip formed to the east.

After attaining maximum intensity of 65 kt (33 m/s) on the 11th, Tip continued to move northwestward and weakened as an exposed low-level circulation. Tip made landfall near Chan Chiang, China on the 13th with maximum sustained winds of 30 kt (15 m/s) and dissipated rapidly over land.



Figure 3-02-2. 1112007 July 200 mb analysis. Note strong northeasterly flow in the South China Sea.



In the week that preceded the development of Typhoon Vera, the monsoon trough extended eastward from the Philippines to 160E as a nearly continuous zone of light surface winds and unorganized convection. However, on 4 July, surface westerlies increased to 15 kt (8 m/s) south of the trough and one circulation center, located near Truk Atoll (WMO 91334) became a persistent feature on JTWC gradient-level charts. noticeable change in convective activity was observed on 8 July, as two distinct cloud masses began to develop within the monsoon trough. This change occurred as two upper-tropospheric cyclones intensified over the Philippine Sea, one east of Luzon about 125E and the other west of Guam about The upper cyclones increased the 140E. upper-level divergence near both convective disturbances and were instrumental in sustaining the development of each during the subsequent three day period. The westernmost disturbance became Typhoon Tip (02W) and the disturbance which moved northwestward from the Truk area became Typhoon Vera.

The first of two TCFAs on Vera was issued at 100600Z, when satellite imagery and 200 mb wind data indicated that a well-defined upper-level circulation had developed over the system. Development of a well-defined surface circulation was slow and the formation alert was reissued at 110600Z after a reconnaissance aircraft investigative mission could not locate a circulation center in the low-level wind field. Figure 3-03-1 shows the suspect dis-

turbance as it appeared on satellite imagery at the time of this reconnaissance mission. Twenty-four hours later, the initial warning was issued for Tropical Depression 03W when data from the next reconnaissance aircraft mission indicated a closed surface circulation with 30 kt (15 m/s) winds and a 1004 mb central sea level pressure.

During the first 36 hours in warning status, Vera intensified quite rapidly and reached typhoon strength by 1318002. During During this period, Vera slowed from an average speed of 12 kt (22 km/hr) to less than 6 kt 12 kt (22 km/hr). Vera skirted the north-eastern portion of the island of Samar at Vera skirted the north-140000Z, with maximum sustained surface winds near 75 kt (39 m/s). Figure 3-03-2 shows Typhoon Vera as it entered the Philippines near the island of Samar. Forecasts from this point forward anticipated that Vera would weaken as it tracked through the Philippines. However, satellite imagery continued to indicate an increase in Vera's central cloud features until it reached the rugged terrain east of Manila at 1500002. Vera then moved into Manila Bay, packing winds near 60 kt (31 m/s), and brought extensive flooding into low-lying areas of the Bay, especially

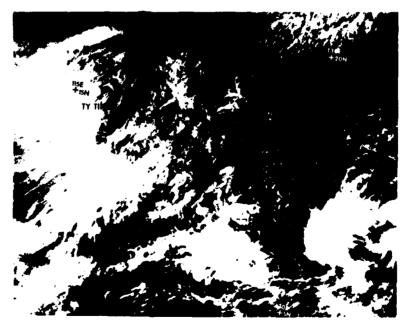


Figure 3-03-1. Typhoon Vera developing 160 nm (296 km) north of Koror at the time that the second formation alert was issued. Typhoon Tip is located to the west in the South China Sea [110644Z NOAA 7 visual imagery].

on Corregidor. Vera passed just southwest of the Naval Air Station, Cubi Point, at 150630Z and into the South China Sea. In its wake, Vera left thousands homeless, nearly 100 people dead and extensive property damage to the southern two-thirds of Luzon.

Track forecasts for Vera were quite good except for an anticipated turn northward as the system moved into the South China Sea. Figure 3-03-3 depicts the 48-hour NOGAPS 700 mb prog valid for 161200Z and the verifying analysis. The significant difference between the prognostic chart and the analysis was the extent and orientation of the subtropical ridge over eastern China. The prognostic fields suggested that a track

northward was possible; however, as Vera moved west-northwestward into the South China Sea, the ridge built westward and also became narrower between 20N and 30N. As a result, the forecast northward track never materialized and Vera persisted on its west-northwestward track.

On 17 July, as Vera approached Hai-Nan Island, a peak intensity of 90 kt (46 m/s) was attained. Crossing Hai-Nan and moving into the northern portion of the Gulf of Tonkin, Vera slowly weakened before making landfall near Haiphong, Vietnam, at 180000Z. It then weakened rapidly over the mountainous terrain of northern Vietnam.

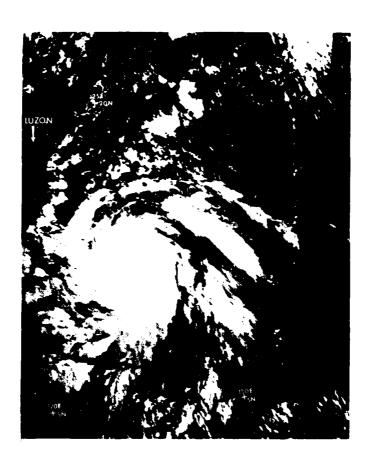
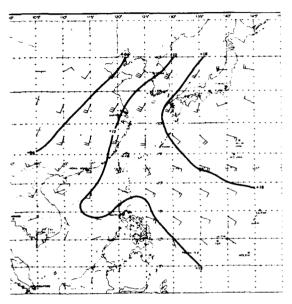
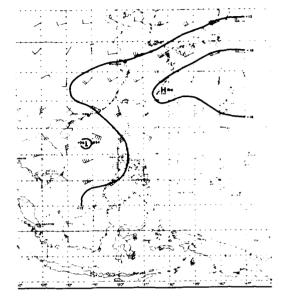


Figure 3-03-2. Typhoon Vera, located just east of Samar, with maximum winds near 10 kt (36 m/s). (1322527 NOAA 8 visual imagery).

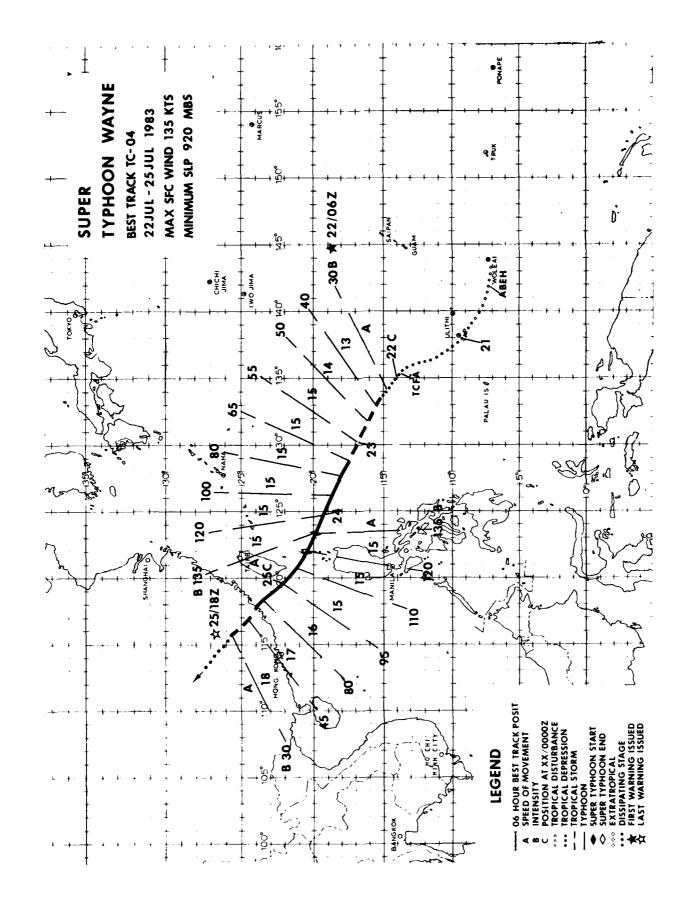




a. 48-HOUR 700mb PROG

b. 700mb ANAL

Figure 3-03-3. NOGAPS 48-hour 700 mb prog (a) and verifying analysis (b) valid for 1612007. Track forecasts toward southern China were influenced by a series of numerical progs which indicated that a pronounced southerly flow would develop in the middle and lower levels over the South China Sea.



Cyclogenesis of Super Typhoon Wayne began in an elongated east-west surface trough west of Truk (WMO 91334). Initial satellite imagery on 19 July at 12002 indicated a widespread area of poorly organized convective activity supported by a weak upper-level anticyclone. This area remained poorly developed until 1200Z on the 21st when of an upper trough northwest of the system (Figure 3-04-1). This served to support the development of the upper-level anticyclone. Subsequent satellite imagery indicated an increase in the organization and convective activity of the system. Based on this evidence and the potential for further development, a TCFA was issued at 212130Z. Initial aircraft reconnaissance at 220457Z revealed a weak tropical depression with an MSLP of 1005 mb and maximum surface winds of 25 kt (13 m/s). The first warning on Wayne was issued shortly thereafter at 220630Z.

During the next 24 hours, Wayne more

than doubled in intensity to 65 kt (32 m/s) and began to track northwestward at 15 kt (26 km/hr). Aircraft reconnaissance at 230830Z reported very high 700 mb heights just prior to entering the eyewall of Wayne, followed by an extremely sharp pressure gradient on penetration to the center of the system. Wayne continued to intensify rapidly, again doubling in intensity over a 24 hour period as it moved westward along the southern periphery of the subtropical ridge. Maximum intensity of 135 kt (67 m/s) occurred at 240600Z only two days after the first warning on the system as a 25 kt (13 m/s) tropical depression.

Wayne's rapid intensification is evident in Figure 3-04-2. Note the generally good agreement between Dvorak intensity estimates and those from reconnaissance aircraft. Figure 3-04-3 shows Wayne near maximum intensity with a wall-developed anticyclone and gravity waves evident in the cloud features near the eye.

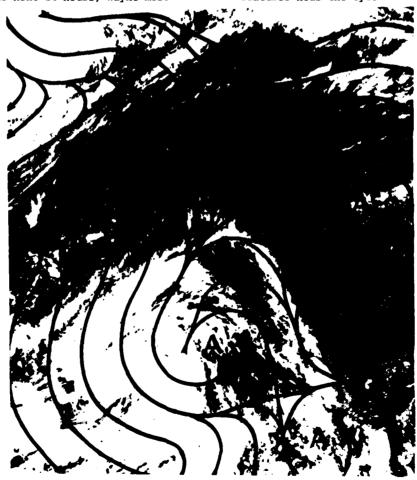


Figure 3-04-1. Overlay of 200 mb analysis with satellite imagery during early stages of development of Super Typhoon Wayne (2120392 July DMSP infrared imagery).

As Super Typhoon Wayne passed north of Luzon, the low-level surface flow was disrupted north of the storm by the topography of Taiwan, setting up a leeside trough in the Formosa Straits. Wayne responded to this trough, taking a more northward track and making landfall approximately 300 nm (556 km) east of Hong Kong (WMO 45005). Wayne struck the coast of China with typhoon strength, but rapidly dissipated as it moved inland over the mountainous terrain of southeastern China.

JTWC was successful in forecasting Wayne's track westward, but encountered problems forecasting speed of movement, which averaged 15 kt (26 km/hr), and intensity, which went from 25 kt (13 m/s) to 135 kt (67 m/s) in just 48 hours. Wayne's rapid

intensification was a product of the supportive upper-level conditions which existed throughout its lifetime. Wayne's initial favorable position with respect to upper-level features (5-7 degrees southeast of a TUTT cell), was maintained throughout its westward track resulting in the development of well defined outflow channels to the northeast and southwest.

Although Wayne did not make landfall in the Philippines, high winds and torrential rainfall associated with its peripheral circulation brough destruction to areas far removed from the center. At least twenty people were killed and more than one hundred were reported missing when a bridge collapsed 300 nm (556 km) southeast of Manila (WMO 98426).

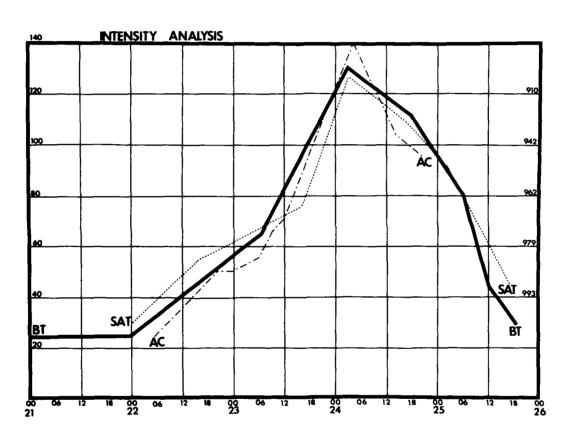
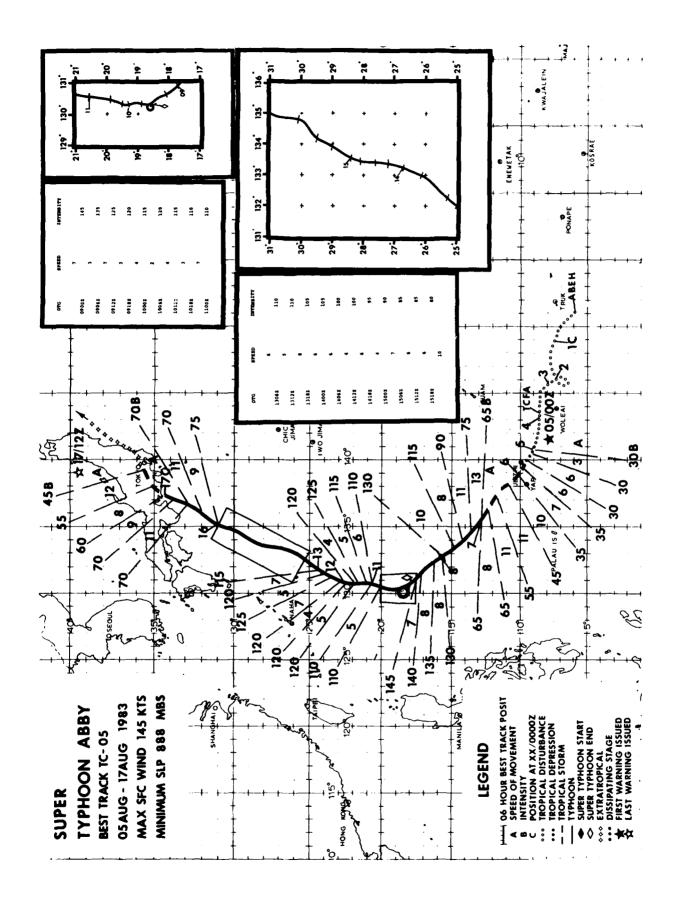


Figure 3-04-2. Satellite intensity estimates (Dvorak, 1913) and intensities measured by reconnaissance aircraft. Best track intensities are represented as a continuous line.



Figure 3-04-3. Super Typhoon Wayne at maximum intensity - 135 kt (67 m/s).



MANAGER BENEVER PROPERTY

The tropical disturbance which eventually developed into the second super typhoon of the season was first detected on satellite imagery on 31 July as an area of enhanced convective activity to the southeast of Guam. This disturbance was located near 6N 152E in close proximity to an upper-level anticyclone. Surface data indicated that a weak surface circulation was centered approximately three degrees to the north of the area of convection. Over the next nine days, this circulation developed into an intense super typhoon with maximum sustained winds of 145 kt (75 m/s) and a massive circulation which was the dominant synoptic feature in the western Pacific. Abby's huge circulation system provided the environment for the development of a second tropical system (Tropical Storm Ben), and eventually caused the dissipation of Ben and another tropical storm (Carmen).

The first four days of Abby's development were unimpressive. The disturbance was monitored closely during this period as it moved slowly westward south of Guam. Although diurnal variations in the convective pattern associated with the disturbance made it appear at times that the system was becoming better organized, no consistent increase in organization was apparent until 3 August.

At 2300Z on 3 August, a TCFA was issued for an area to the south-southwest of Guam based on the consistent increase in organization of the system observed on satellite imagery. A weather reconnaissance aircraft was launched soon after the TCFA was issued, but it was unable to close off a surface circulation even though several hours were spent investigating the suspect area. The mission did succeed in locating a circulation at flight level (1500 ft - 457 m), and at the 700 mb level.

The second aircraft reconnaissance mission was able to close off a surface circulation the following morning at 050034Z. Maximum sustained winds observed were 30 kt (15 m/s) and the MSLP was 1004 mb. On the basis of this report, the first warning was issued on the system as a tropical depression. The forecast called for continued movement towards the west-northwest with slow intensification.

Initial expectations proved reliable for the first 24 hours in warning status. The system was upgraded to a tropical storm at 050600Z on the basis of an increase in convective organization apparent from satellite imagery. At 060000Z Abby's intensity and position were close to forecast expectations.



Figure 3-05-1. Super Typhoon Abby near maximum intensity (0909462 August DMSP infrared imagercu).

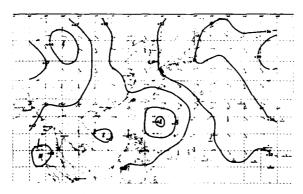
Abby started to move on a more northwestward track after 060000Z, even though all JTWC forecast aids were indicating west-northwestward movement. This was a problem that persisted for the next ll days. Abby continually tracked to the right of JTWC forecasts even though the forecast aids and numerical progs were all consistently in good agreement on a west-northwestward track for Abby.

Intensity forecasting also proved to be difficult. Initial expectations were quite accurate for the first 48 hours in warning status. As expected, Abby was upgraded to typhoon at 061800Z when satellite imagery indicated the presence of a weakness in the central dense overcast. The presence of an eye and the accuracy of the intensity estimate by satellite were confirmed five hours later by reconnaissance aircraft reports of 65 kt (33 m/s) winds and MSLP of 973 mb.

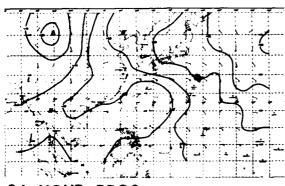
On the 7th of August, Abby began to intensify rapidly, far exceeding initial forecast expectations. Reconnaissance aircraft at 0711412 reported a MSLP of 946 mb, a decrease of 27 mb in approximately 12 hours. Other data (MSLP and equivalent potential temperature relationships (Dunnavan, 1981))

collected on the aircraft reconnaissance mission indicated that Abby was about to undergo rapid intensification. The 0712002 warning called for continued rapid intensification on the basis of this information. This forecast proved to be accurate as Abby continued to intensify rapidly over the next 30 hours reaching 120 kt (62 m/s) intensity within 12 hours and maximum intensity of 145 kt (75 m/s) at 0818002. Abby's lowest central pressure was recorded at 0820492 when dropsonde data from reconnaissance aircraft indicated a measurement of 888 mb. Figure 3-05-1 shows Abby near maximum intensity. Except for minor fluctuations, Abby's intensity decreased slowly and steadily from this point on.

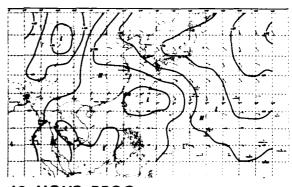
This decrease in intensity was accompanied by a decrease in forward speed as Abby began a slow northward movement for the next two and one-half days. JTWC forecasts for this two and one-half day period called for slow movement to the north followed by a turn to the northwest toward the island of Okinawa. This forecast track was supported by the FLENUMOCEANCEN numerical prog series which indicated that the subtropical ridge over southern Japan would strengthen and induce a northwestward movement. An example



ANALYSIS



24-HOUR PROG



48-HOUR PROG

Figure 3-05-2. FLENUMOCEANCEN prog series for 850 mb at 0912002 August. Note that the subtropical ridge over Japan is forecast to remain as a block to northeastward movement.

of the prog series can be seen in Figure 3-05-2 which depicts the 850 mb prog series for 0912002.

The intensification of the subtropical ridge over Japan that was consistently forecast in the prog series never occurred. An extensive post-analysis of the height fields over Japan and the islands to the south of Japan indicated that the subtropical ridge weakened continuously in this area over the eight day period following the analysis in Figure 3-05-2.

On the 12th of August, Abby began moving northeastward toward Honshu. Also on the 12th, two other tropical systems developed in the western Pacific; Tropical Storm Carmen (06W) in the South China Sea west of Luzon, and Tropical Storm Ben (07W) to the east of Abby near 26N 146E. The interaction of Abby's outflow with a TUTT cell to the northeast created an area of intense upperlevel divergence under which Ben formed. The presence of both of these smaller systems had little effect on Abby, except for drawing some of the inflow away; but in the end, it was Abby which led to the demise of both Ben and Carmen when they became embedded in Abby's massive circulation.

As Abby continued its movement towards the northeast, the forecast emphasis changed from a northwest movement to that of a northnorthwest movement towards the island of Kyushu. This forecast track was based on the strengthening of the subtropical ridge to the north and east of Abby; but as stated earlier, the ridge did not strengthen and Abby continued to move toward the northeast and weaken slowly. Aircraft reconnaissance data at 1410352 indicated that Abby's central pressure had risen to 942 mb and that the eyewall was beginning to deteriorate. Abby's intensity fell below 100 kt (51 m/s) at 141800Z for the first time in 7 days.

Abby continued moving to the northeast on the 15th of August with a slight increase in forward speed. Application of an objective technique for predicting acceleration (Weir, 1982) led to a forecast of rapid acceleration to the north through central Japan and extratropical transition over the Sea of Japan. This was based on the expectation that Abby would come under the influence of strong southerly flow in advance of a major trough over northern China. The predicted acceleration never materialized as an upper-level ridge developed over the Sea of Japan to the northwest of Abby (Figure 3-05-3) and effectively blocked this interaction.

Japanese weather radar stations started fixing Abby after 1600002, with all of the fixes showing continued northeast movement. Data from reconnaissance aircraft, satellite imagery, and synoptic reports indicated that Abby was weakening as it underwent extratropical transition. Abby was downgraded to tropical storm at 1700002 and soon after made landfall near Hamamatsu Japan (WMO 47654). After making landfall, Abby moved eastward following the rugged terrain toward Tokyo, weakening rapidly as it interacted with the mountains. At 1712002, satellite imagery and synoptic data indicated that Abby had completed extratropical transition, and the final warning by JTWC was issued.

Abby's movement through central Japan caused serious damage over a widespread area. Initial reports indicated that at least two people were killed, 29 others were injured, and one person was missing. The torrential rains generated by Abby resulted in widespread flooding, causing numerous landslides and the destruction of 19 bridges. The heavy rains also severly disrupted road, rail, sea and air service in central Japan.

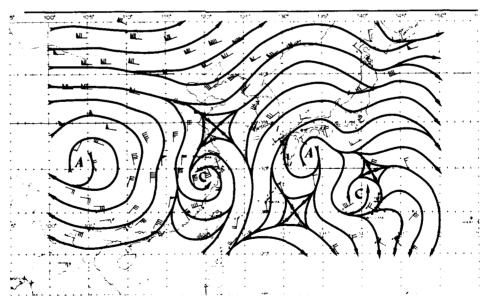
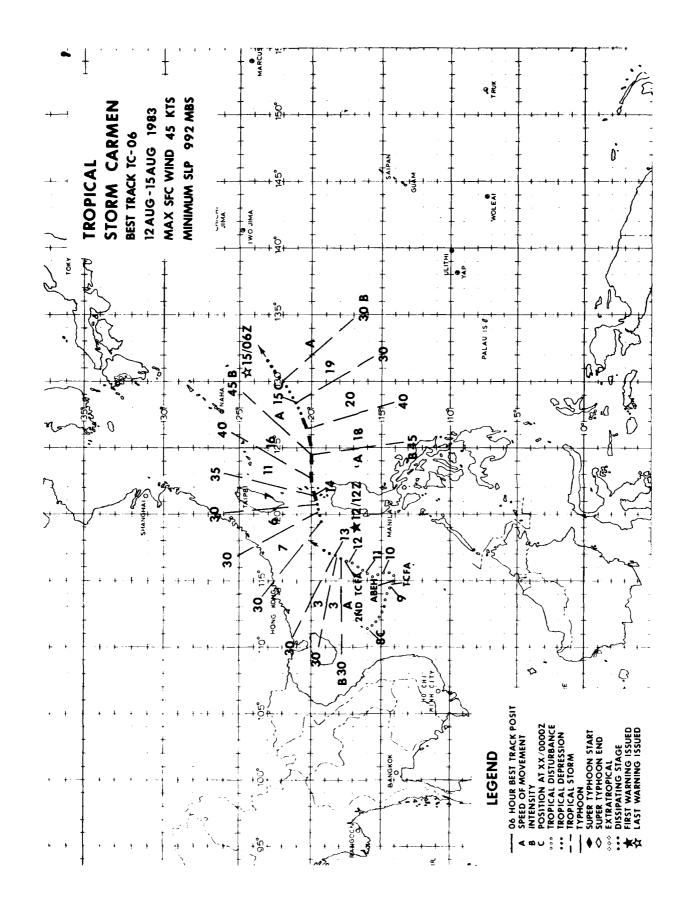


Figure 3-05-3. 200 mb analysis for 1700007 August showing the ridge over the Sea of Japan which prevented Abby from interacting with the westerlies and accelerating northeastward.



Tropical Storm Carmen had its origins in the monsoon trough which was well established over Southeast Asia and moved into the South China Sea in early August. A low level circulation first located about 200 nm (370 km) east of Vietnam persisted as a closed circulation on the surface streamline analysis and as an area of enhanced convective activity on satellite imagery for several days while moving slowly eastward along the trough axis. At the same time, Super Typhoon Abby was undergoing rapid intensification in the Philippine Sea. Abby's outflow generated a strong easterly flow at upper-levels which was expected to inhibit the development of the tropical disturbance in the South China Sea. However, on 9 August, satellite imagery at 0000Z indicated that outflow was developing over the South China Sea disturbance. Synoptic data also indicated that the lowlevel circulation had become better organized and had associated surface winds of 20 kt (10 m/s) and an MSLP of 1002 mb. This increase in organization prompted the issuance of a TCFA at 0903002.

The disturbance remained in alert status for the next three days as it tracked slowly north-northeastward with little change in intensity. Aircraft reconnaissance at 120247z indicated that the disturbance was still poorly organized with an MSLP of 1000 mb. Satellite imagery during this period also indicated little increase in convective organization. At 120900z, satellite imagery indicated that the disturbance had developed a small central convective feature. The initial warning for Carmen as a tropical depression was issued at 121200z on the basis of this increase in convective organization.

For the rest of the day, Carmen tracked slowly north-northeastward without any further development in convective organiza-

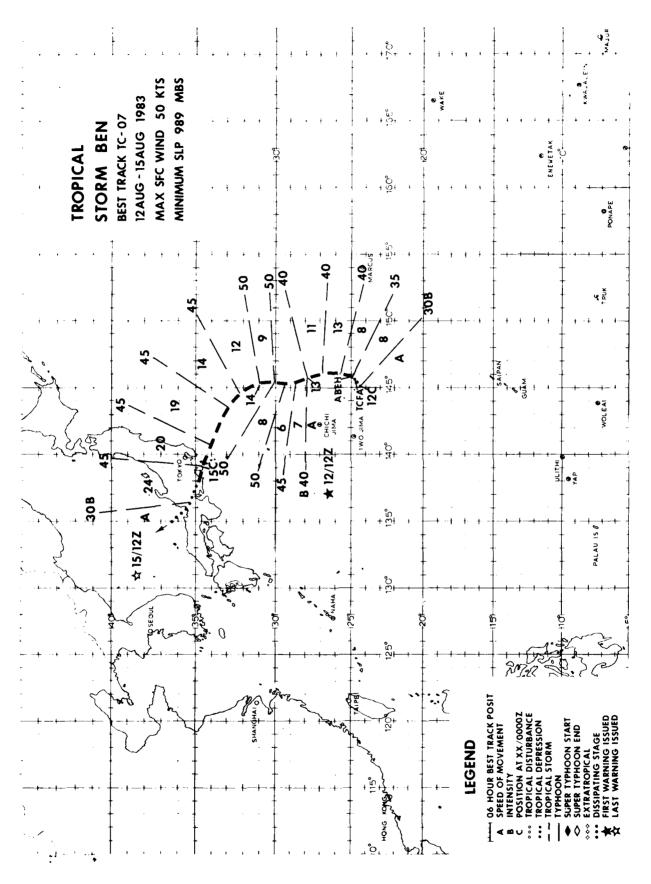
tion. Suddenly, between 1300002 and 130600Z, the depression appeared to rapidly accelerate from 3 to 26 kt (2-13 m/s) and move east-northeastward toward the Luzon Warnings at the time reflected Straits. this rapid acceleration. However, in post-analysis, satellite imagery indicated the presence of several weak circulations (eddies) near the Luzon Straits during this period. A new circulation established itself 70 nm (130 km) to the northwest of Luzon, approximately 170 nm (315 km) east of It was this new circulation that was tracked from 130600Z onward as Carmen. The disturbance that was initially designated Carmen, continued its north-northeastward track and persisted as a small area of convection for another 18 hours before eventually dissipating over water on The new disturbance that was now 14 August. designated Carmen, moved east-northeastward through the Luzon Straits, embedded in the low-level flow feeding into Super Typhoon Abby in the Philippine Sea. In spite of the hostile shearing environment and the fact that the depression was embedded in Abby inflow, intensification of this circulation continued and upgrade to tropical storm occurred on the 131800Z warning.

Carmen continued to intensify, reaching maximum intensity of 45 kt (23 m/s) at 1412002 while accelerating toward Abby. Figure 3-06-1 shows Carmen near maximum intensity 100 nm (185 km) northeast of Luzon. Less than 12 hours later, at 142300Z, Carmen was almost completely absorbed into Abby's circulation and was no longer "fixable" by reconnaissance aircraft.

The final warning on Carmen, now a tropical depression, was issued on the 15th at 0600Z when it became impossible to identify the remnants of the system on satellite imagery.



Figure 3-06-1. Tropical Storm Carmen near maximum intensity 100 nm (185 km) northeast of Luzon. Super Typhoon Abby (upper right) completely absorbed Carmen into its circulation less than a day later (1406322 NOAA 7 visual imagery).



TROPICAL STORM BEN (07W)

As Typhoon Abby approached Japan from the southwest, satellite imagery indicated that an area of intense convection was forming on the eastern periphery of its circulation (Figure 3-07-1). Surface and 200 mb analyses at the time (Figure 3-07-2 and 3-07-3) indicated that the convection was not associated with a separate surface circulation but with an area of highly divergent flow at upper-levels. This flow was associated with a TUTT cell located to the northeast of Abby.

This area of active convection persisted with no apparent associated low-level circulation until 12 August, when visual satellite imagery indicated the presence of a low-level circulation on the western edge of the convective activity. The presence of a surface circulation in an area of such strong upper-level divergence prompted the issuance of a TCFA at 1204192.

Reconnaissance aircraft investigated this area later in the day and located a poorly defined circulation with a highly asymmetric wind field. Winds of 40 kt

(21 m/s) were observed over a broad area in the southeastern semicircle of the circulation but winds to the north and west were in the 10-20 kt (5-10 m/s) range. The first warning for Tropical Storm Ben was issued at 121200Z and forecasted northwestward movement up the eastern coast of Japan at the periphery of the subtropical ridge. This forecast scenario appeared valid for the next 24 hours as Ben moved northward and turned westward as expected. However, westward motion was greater than originally forecast and Ben moved rapidly along the southern coast of Honshu prior to making landfall west of Hamamatsu (WMO 47654). Ben moved westward, it entered an area of strong upper-level flow associated with outflow from Typhoon Abby. Satellite imagery indicated that the convection associated with Ben was dissipating and appearing at successively greater separation distances to the east of the low-level circulation center.

By 14 August, Ben was a completely exposed low-level circulation and remained so until dissipation in the Sea of Japan at 1512002.

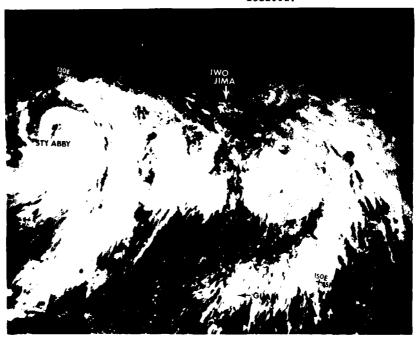


Figure 3-07-1. Typhoon Abby (left) and the area of enhanced convective activity to the east where Tropical Storm Ben formed. (1105272 NOAA 7 visual imagery).

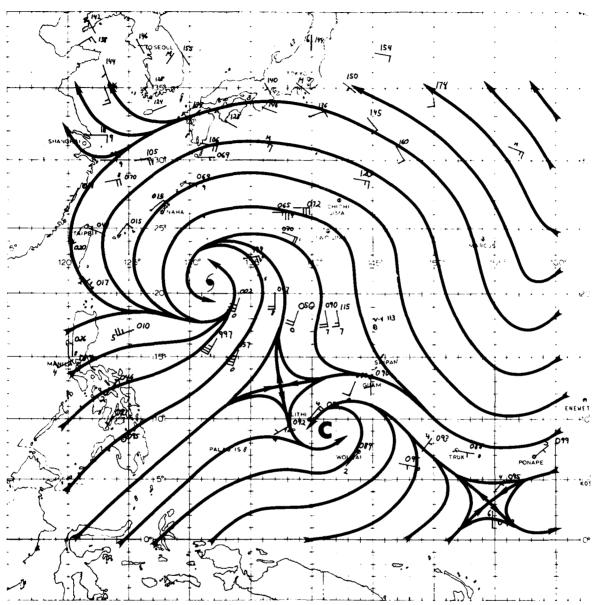


Figure 3-07-2. 1100002 surface analysis. Although analysis time corresponds closely with the time of the satellite picture shown in Figure 3-07-1, there is no indication of a surface circulation in the area where Ben formed 24 hours later.

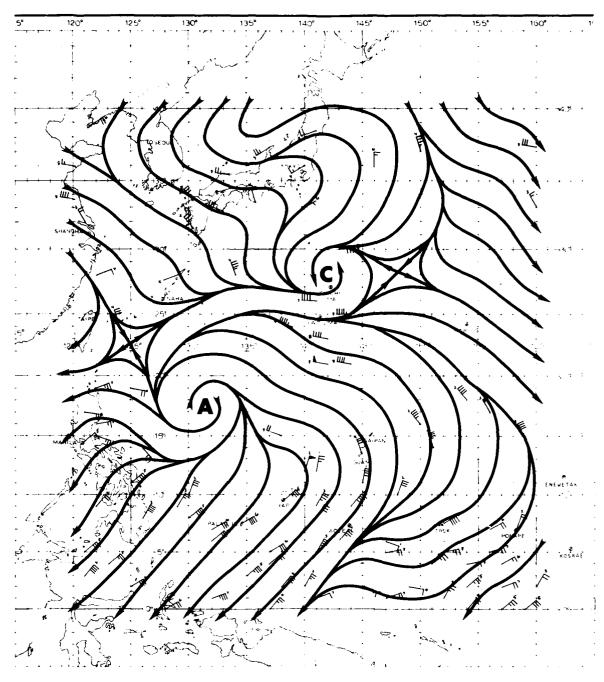
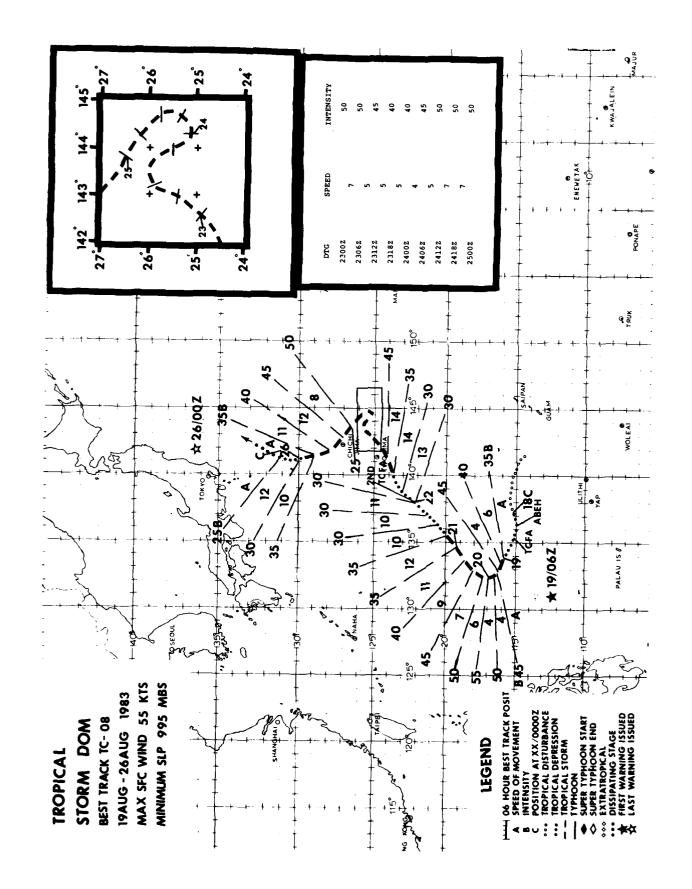


Figure 3-07-3. 110000Z 200 mb analysis. The area of enhanced convective activity to the east of Abby in Figure 3-07-1 corresponds to an area of highly divergent upper-level flow created by the interaction of Abby's outflow with a TUTT cell.



Tropical Storm Dom developed from a disturbance which was initially detected west of Guam on 17 August. Over the 10 day period of its life, Dom underwent radical changes in track and intensity. These changes and Dom's lack of significant vertical development created difficulties for JTWC forecasters. Radical intensity changes resulted in a 36-hour period when no numbered tropical cyclone warnings were issued on Dom by JTWC (21-23 August).

As Super Typhoon Abby approached Tokyo on 17 August, low latitude wind regimes began to return to their seasonal mean locations. Figure 3-08-1 shows the orientation of the low-level monsoon and upper-tropospheric troughs on 17 August, as well as the climatological positions for each for the month of August. Of significance is the position of the low-level trough to the west of the upper-level trough, which was anchored to an intense upper-tropospheric cyclone near Guam. As this occurred, an area of strong upper-level divergence formed in the northeaster-lies to the west of the upper-level cyclone and a convective disturbance developed within the low-level trough.

On 18 August, a reconnaissance aircraft investigated the disturbance at 700 mb and reported flight level winds of 25 kt (13 m/s) and an extrapolated MSLP of 999 mb. On the basis of this report and subsequent satellite imagery which indicated increased convective organization, a TCFA was issued at 181100Z. The next reconnaissance aircraft mission, at 190735Z, located a well defined surface circulation with an MSLP of 1004 mb and maximum sustained surface winds of 40 kt (21 m/s). The initial warning for Tropical Storm Dom was issued on receipt of this information from the aircraft.

During the two-day period prior to initial warning, Dom had tracked steadily westward at 9 kt (5 km/hr). In spite of this, continued westward movement was rejected by JTWC forecasters and Dom was forecast to move northward from the initial warning. Figure 3-08-2 shows the guidance available to JTWC forecasters from the objective forecasting techniques for the 1912002 warning (Note: objective techniques are originated from a preliminary best track position six hours prior to warning time in this case 1906002). Although there were considerable differences in the forecast aids, both dynamic models (NTCM and OTCM) predicted northward movement, reflecting the absence of a strong subtropical ridge. The Prognostic Reasoning Message (WDPA1 PGTW) which was issued following the 1912002 warning is the best summary of the situation.

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"Dom is forecast to turn northward during the next 24 hours. Lowlevel steering is predominately from south-to-north and the presence of middle-tropospheric westerlies north of 22N is seen as evidence of the overall weakness of the subtropical ridge over the Philippine Sea. "The most significant feature on the charts is a deep, complex low pressure area which extends eastward from Japan. The FLENUMOCEANCEN prognosis series maintains this mid-latitude trough throughout the forecast period. Its influence is expected to maintain the weakness in the ridge and allow Dom to move northward. Not forecast by the numerical prognoses, but considered possible, is an increase in the southwest monsoonal flow over the Philippine Sea. A linkage between the southwest monsoon and the midlatitude trough, east of Japan, could cause Dom to track northeastward

The alternate scenario proved correct, as Dom turned sharply northeastward on 20 August.

Throughout much of its life, Dom's low-level center was located northeast of its significant convection. Strong upper-level northeasterlies were exerting considerable pressure on the atmospheric column above Dom, resulting in the consistent tilt toward the southwest. The mission ARWO1 on the 1923302 fix mission observed "The extremely slight pressure gradient indicated that this was probably a shallow tropical cyclone...the 700 mb center was located southwest, relative to the surface center, but even further displaced (from the earlier penetration). A solid "wall" of convective activity seemed to be developing at this time, extending through the southwest quadrants." This observation was made at Dom's peak intensity of 55 kt (28 m/s).

As Dom turned northeastward, the area of strongest convective activity became further separated from the surface center (Figure 3-08-3) and eventually weakened. On 21 August, reconnaissance aircraft verified the weakening of the system as observed on satellite imagery. Surface winds near the center were light and surface pressures were up significantly although stronger, near gale-force, winds were present 50 to 60 nm (93 to 111 km) southeast of the surface center, within the monsoonal flow. Since Dom was not expected to reintensify in such a hostile shearing environment, tropical cyclone warnings were suspended after the issuance of the 211200Z warning. In the

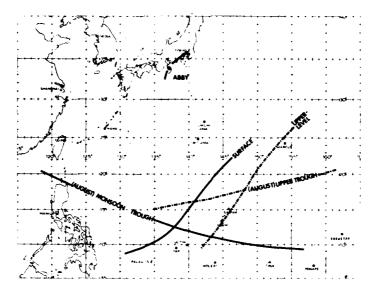


Figure 3-08-1. Location of the axis of the low-level and upper-level troughs on 17 August and the monthly climatological position of the monsoon (low-level) and tropical upper-tropospheric troughs for August. Note the northeast to southwest orientation of each trough on the 11th, and the atypical location of the low-level trough west of the upper-level trough.

subsequent 12 hours, satellite imagery indicated that convective activity was increasing near the center, prompting the issuance of a TCFA at 212330Z. An aircraft reconnaissance mission was flown at 220612Z and found 30 kt (15 m/s) surface winds more than 200 nm (370 km) southeast of a 1003 mb surface center. However, the next mission, at 222351Z found a 995 mb center with a 40 kt (21 m/s) maximum wind 10 nm (19 km) east of the surface center. On the basis of this report, Tropical Storm Dom was returned to warning status at 230000Z while the aircraft was still in the center. As the aircraft exited to the south, it encountered even stronger winds than those previously reported. The following was extracted from the ARWO's² post flight mission report:

"This system continued to have a majority of its weather concentrated in the south....showers were very heavy and ominous looking, in fact, I observed a waterspout trailing from one of the heavier showers. Even though we were only 60 to 100 nm (111 to 185 km) from the center during the invest, we found light and variable winds, especially in the northern half I was hard pressed of the storm. to close off the circulation in the northwest quadrant. Once closed off, the storm showed itself to be a highly compact area of 40 kt (21 m/s) surface winds, extending 45 nm (83 km) from the The center itself was a

¹Mission ARWO (Aerial Reconnaissance Weather Officer), 1Lt Gregory T. Marx, USAF.

 $^{2}\mbox{Mission ARWO, Capt Stephen W. Lizon, USAF.}$

small area, 3 to 5 nm (6 to 9 km), where the pressure dropped rapidly. This area of low pressure was very definite, but difficult to hit exactly due to its highly localized area. After the fix, we headed due south and, in a 30 nm (56 km) wide band beginning 20 nm (37 km) from the surface center, I observed surface winds reaching 50 kt (26 m/s) with gusts to 60 kt (31 m/s)."

Figure 3-08-4 shows Dom just prior to this aircraft mission.

During Dom's northeastward trek, its movement was correlated to the monsoon southwesterlies and a stationary midlatitude trough located east of Japan. On 22 August, this trough, including the extratropical remains of Super Typhoon Abby (05W) began to move eastward and weaken. This change, along with a lessening of the influence of the upper-tropospheric northeast-erlies over Dom, were contributing factors in Dom's reintensification. It also marked a change in steering influences which resulted in Dom moving erratically from 231200Z to 241200Z, prior to assuming a north-northwestward track. During this period, Dom's intensity dropped slightly, to 40 kt (21 m/s) but peaked again briefly as an upper-level anticyclone became established over the system (Figure 3-08-5). However, this upper-level support proved to be short-lived and Dom was reduced to an exposed low-level circulation of tropical depression intensity a day later.

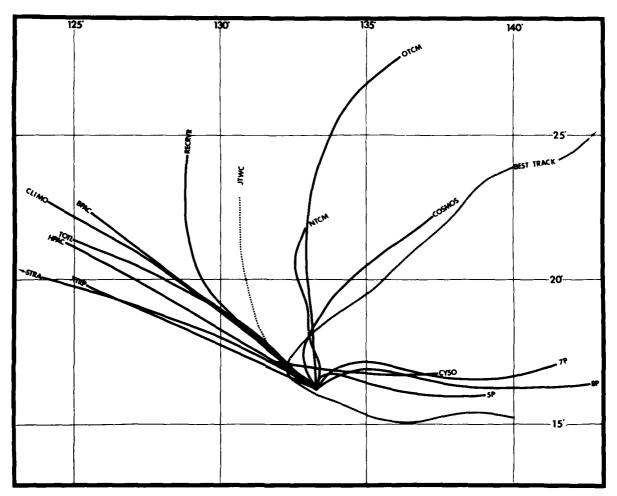


Figure 3-08-2. The standard array of JTWC's objective forecasting techniques available to support the 1912007 warning. Included is the forecast issued at 1912007 and the eventual best track. Note that the technique "COSMOS", currently under test and evaluation at JTWC, did a superior job in forecasting the eventual track.

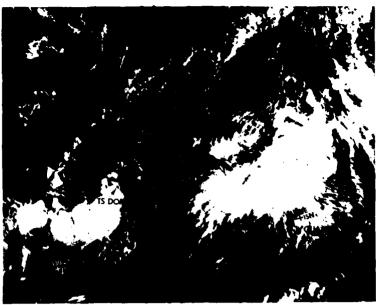


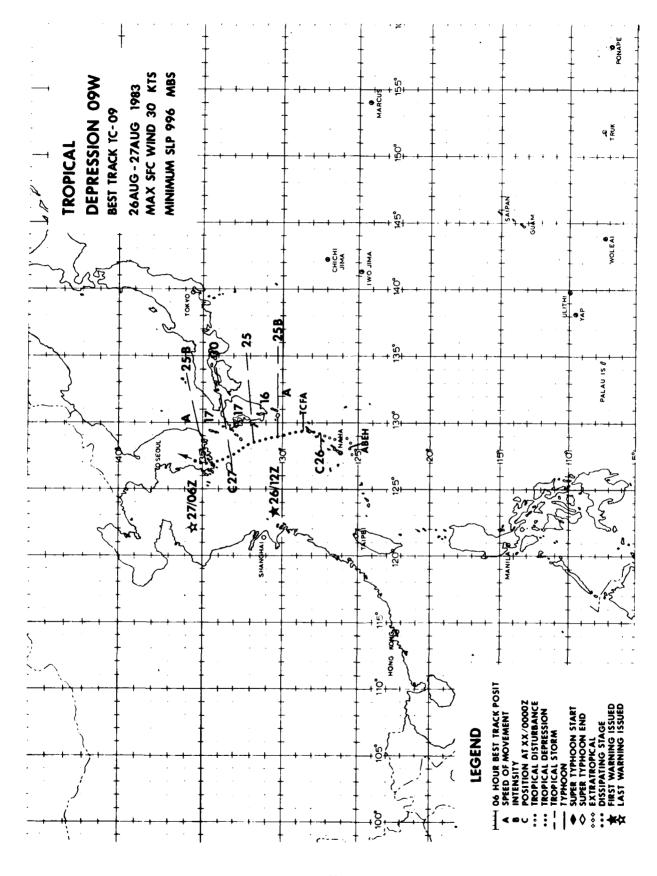
Figure 3-08-3. Satellite imagery shows several convective cells extending toward the southwest and west of Dom's low-level center (2022347 August NOAA 8 visual imagery).



Figure 3-08-4. Satellite imagery received just prior to aircraft data indicates that the system had reintensified. Note the low-level cloud lines which correspond to the ARWO's description of the system (2221507 August NOAA 8 visual imagery).



Figure 3-08-5. In a last, but brief, period of reintensification, satellite imagery indicates an upperlevel anticyclone forming over Dom's low-level center (2420337 August DMSP visual imagery).



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TROPICAL DEPRESSION (09W)

Tropical Depression 09W was unusual in that it developed in an area where tropical cyclogenesis is a rare event. It was first detected as a tropical disturbance located 60 nm (111 km) south of Okinawa on the 25th of August. At this time, the monsoon trough was displaced far to the north of its climatological position following the passage of Tropical Storm Dom. Tropical Depression 09W formed to the west of Dom in an area of highly convergent low-level flow.

Tropical Depression 09W was first mentioned in the Significant Tropical Weather Advisory (ABEH PGTW) at 0600Z on the 25th. Upper-level flow in the vicinity of the circulation was highly divergent and Dvorak intensity estimates indicated that maximum sustained winds associated with the circulation were 30 kt (15 m/s). Tropical Depression 09W showed no signs of further development in the next 24 hours of its existence. However, a TCFA was issued at 260400Z because the favorable upper-level conditions indicated a good potential for intensification of the circulation.

Soon after the TCFA was issued, satellite imagery (Figure 3-09-1) revealed an exposed low-level circulation with associated convective activity displaced 300 nm (555 km)

to the south. Synoptic data at the time indicated that the central pressure of the depression was below 1000 mb but the area of maximum winds was 100 nm (185 km) from the center. At this point, it was expected that the circulation would become better organized and pose a threat to nearby population centers in Japan and Korea. Accordingly, the first warning on Tropical Depression 09W was issued at 261200Z.

The only aircraft reconnaissance mission flown on this system was conducted at 2330Z on the 26th. Terrain in the area precluded a low-level flight and severaly restricted the collection of peripheral data. However, the height of the 700 mb center supported a maximum surface wind speed of 30 kt (15 m/s). This intensity was in perfect agreement with simultaneous estimates using satellite imagery.

Tropical Depression 09W never developed into a tropical storm and dissipated rapidly after making landfall on the southern coast of Korea. Although the East China Sea was dominated by cloudiness and rain showers during its passage, there were no reports of injury or property damage related to this depression.

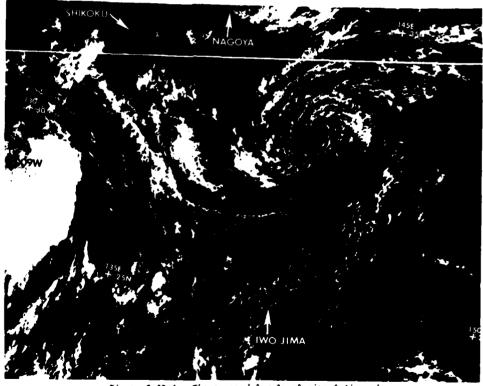
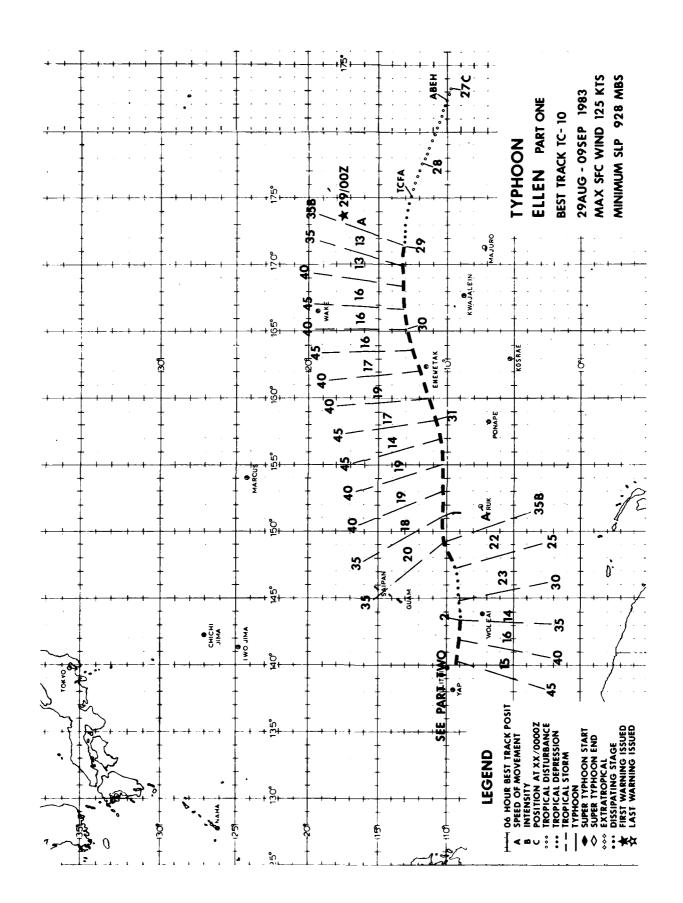
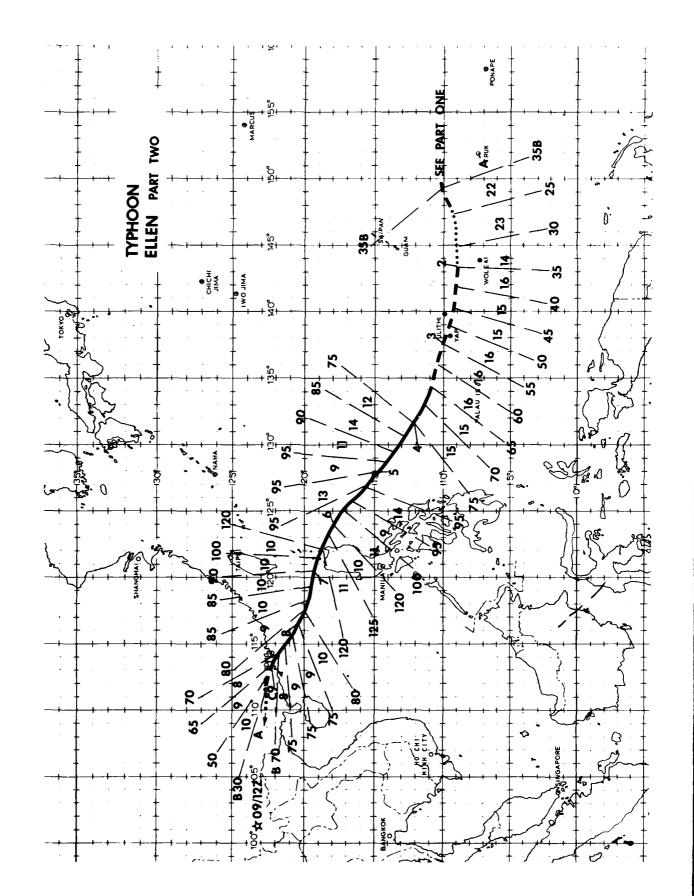


Figure 3-09-1. The exposed low-level circulation of TD 09W (left) and Tropical Storm Dom (right) in its dissipation stage [2605462 August NOAA 7 visual imagery].





TYPHOON ELLEN (10W)

Typhoon Ellen first became apparent on satellite imagery as a tropical disturbance located near 10N 170W on the 26th of August. The disturbance was located in a data-sparse area, making it difficult to estimate its degree of organization or intensity. Satellite intensity estimates using the Dvorak method indicated maximum sustained winds of 30 kt (15 m/s). These estimates were based primarily on the presence of upper-level banding features. Because of its impressive appearance on satellite imagery, the disturbance was mentioned in the Significant Tropical Weather Advisory (ABEH PGTW) on the 27th. At this time, the disturbance was not located in the JTWC area of responsibility (AOR) but it was moving westward and it was becoming a matter of increasing concern to interests in the eastern portion of the JTWC AOR.

The disturbance crossed the dateline and entered the JTWC AOR on the 28th. A TCFA was issued at 281100Z as the system, now associated with a weak upper-level anticyclone, continued moving westward. Satellite imagery indicated that the disturbance was intensifying with maximum sustained winds of 35 kt (18 m/s). This prompted the issuance of the first warning on Ellen at 290000Z which projected continued west-northwestward movement and intensification.

During the next five days, Ellen's intensity fluctuated between 25 and 45 kt (13-23 m/s). Further development during

this period was inhibited by the lack of low-level westerly inflow and the restriction of upper-level outflow channels to the north by a large upper-level anticyclone centered south of Japan. This large upper-level anticyclone was a manifestation of an intense cell of high pressure which extended throughout the troposphere and had a tremendous impact on Ellen. In addition to interferring with Ellen's outflow at upperlevels, it prevented continued westnorthwestward movement and caused Ellen to assume a southwestward track around its southern periphery at speeds of 13 to 23 kt This high speed of movement, (7-12 m/s). combined with outflow restrictions, caused Ellen to weaken to tropical depression intensity briefly on the 1st of September.

After reaching a minimum intensity of 25 kt (13 m/s) at 011200Z, Ellen began to strengthen, reaching typhoon intensity two days later at 031200Z. Upper-level flow patterns during this period were very favorable for the development of outflow channels. A TUTT cell over the South China Sea (Figure 3-10-1) was instrumental in providing the proper environment for the establishment of outflow to the north. Coincident with Ellen's intensification was a change in track from west-southwestward to west-northwestward. This marked Ellen's transit beyond the southernmost point of the massive high previously discussed.



Figure 3-10-1. Favorable upper-level conditions led to Ellen's reintensification after weakening to a tropical depression on 1 September (0212002 September 200 mb analysis).

By 051200z, Ellen was located 200 nm (370 km) east of Luzon with maximum sustained winds of 95 kt (49 m/s). An objective technique for forecasting the onset of explosive deepening (Dunnavan, 1981) indicated that Ellen would deepen rapidly over the next 34 hours. The reliability of this technique was verified when Ellen's central pressure dropped 28 mb to 928 mb over the next 12 hours. Ellen reached maximum intensity of 125 kt (64 m/s) shortly thereafter, at 060600Z (Figure 3-10-2).

This peak in intensity was short-lived due to interaction between the southern part of Ellen's circulation and Luzon. Ellen weakened continuously from this point on as it moved through the Luzon Straits

and headed for southern China.

Fix information on Ellen was exceptionally good. In addition to normal aircraft reconnaissance, three fixes a day from the 3rd to the 7th were provided by an aircraft flying special aircraft stress test penetrations. This aircraft and crew were from the 53rd Weather Reconnaissance Squadron at Keesler AFB, Mississippi. In addition to supplemental aircraft reconnaissance flights, radar coverage of Ellen by land stations was extensive. Radar reports from Aparri, P.I. (WMO 98231), Kaohsiung, China (WMO 46744) and the Royal Observatory, Hong Kong (WMO 45005) provided nearly continuous coverage from the Luzon Straits to landfall near Macao.

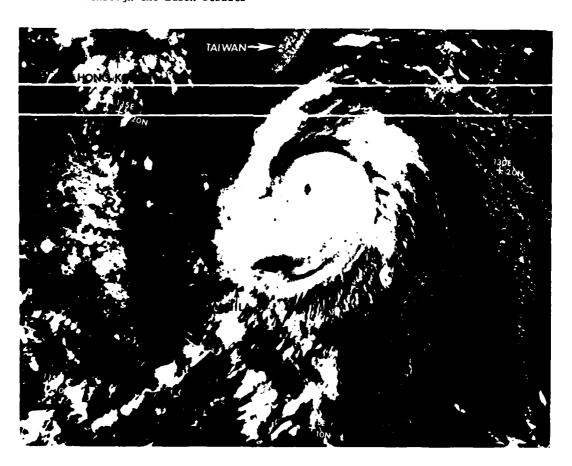


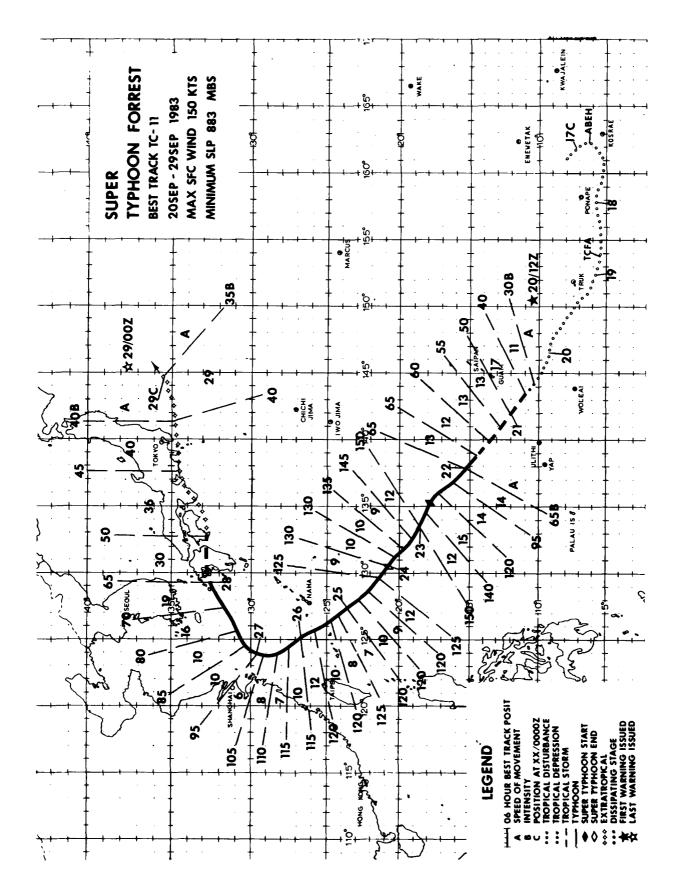
Figure 3-10-2. Typhoon Ellen at maximum intensity (0606532 September NOAA 7 visual imagery).

Ellen made landfall just south of Macao at 0000Z on the 9th of September. Maximum sustained winds at landfall were 65 kt (33 m/s) with gusts to 80 kt (41 m/s). Higher winds due to channelling effects were recorded at the Royal Observatory, Hong Kong, with the highest reported at 90 kt (46 m/s) gusting to 140 kt (72 m/s).

Damages in Hong Kong were extensive. Preliminary reports indicated that six people were killed and 277 were injured, with 120 requiring hospitalization. More

than 1,600 people sought emergency shelter, mostly residents of makeshift hillside dwellings swept away by high winds, flooding, and landslides. Damages to shipping were also extensive. The Hong Kong Marine Department reported that 22 ships ran aground during Ellen's passage.

After moving inland, Ellen dissipated rapidly, becoming a 30 kt (15 m/s) tropical depression within 12 hours after making landfall.



SUPER TYPHOON FORREST (11W)

Forrest was the most intense of all of the tropical cyclones of 1983. After taking a long time to reach tropical storm intensity, it intensified from a tropical storm to a super typhoon in 30 hours and reached a maximum intensity of 150 kt (77 m/s) (Figure 3-11-1).

Forrest developed from a tropical disturbance which originated in a broad area of convective activity located 300 nm (556 km) to the east of Ponape (WMO 91348). This disturbance was first discussed in the Significant Tropical Weather Advisory (ABEH PGTW) on the 17th of September. At this time, the disturbance had a great deal of associated convection but was not well organized. However, a reconnaissance aircraft was dispatched to the area when 24 hour pressure drops of 3 mb at nearby stations were recorded. The aircraft mission con-

firmed the lack of organization in the system and was not able to close off a circulation. This mission was the first of four aircraft reconnaissance flights into Forrest during the period 17-20 September. All four were unable to close off a surface circulation. However, the fourth aircraft did succeed in closing off a circulation at the 700 mb level, thereby lending credence to the theory that Forrest originated from a mid-level circulation which developed downward.

Even though aircraft reconnaissance indicated the lack of a surface circulation, a TCFA was issued for the disturbance at 1818012 when the convection associated with it began to intensify and expand. The alert was reissued 24 hours later, after the second aircraft reconnaissance mission failed to close off a surface circulation.



Figure 3-11-1. Super Typhoon Forrest at maximum intensity with 150 kt (77 m/s) winds and MSLP of 883 mb (2222232 NOAA 8 visual imagery).

The third and fourth aircraft reconnaissance missions were flown on the morning and afternoon of 20 September. Although both flights confirmed the absence of a surface circulation during the day, the first warning was issued later that evening when satellite imagery indicated the formation of a central dense overcast and good outflow to all quadrants. At this time, Forrest was located about 180 nm (330 km) south of Guam. The forecast called for continued gradual intensification and slow northwestward movement. Although this forecast track verified well, the intensity projections were far short of the mark. Reconnaissance aircraft flying a mission on the following morning encountered 50 to 60 kt (21-26 m/s) winds in Forrest's well-defined circulation. Continued intensification after this occurred rapidly. Forrest was upgraded to a typhoon at 2118002 when satellite imagery indicated a developing eye. Aircraft dropsonde data at 2123402 indicated that Forrest's central pressure had dropped to 975 mb. About 11 hours later, at 221057Z, a sea-level pressure of 883 mb was recorded. This represented a drop of 92 mb in a little under 24 hours. This is graph-ically displayed in a plot of Forrest's central sea-level pressure over time (Figure 3-11-2). Note the rapid drop in pressure on

Fortunately, Forrest's rapid intensification occurred after the system had moved well clear of Guam. Even though Forrest was

relatively weak when it passed Guam, the island was subjected to winds gusting in excess of 30 kt (15 m/s) and heavy rains. About 2 inches (5 cm) of badly needed rain fell, causing minor flooding but no serious damage.

As Forrest moved northwestward and intensified, it became apparent that a recurvature scenario was developing. A break in the subtropical ridge between Taiwan and Okinawa was clearly and consistently indicated in the NOGAPS numerical prognoses. Forrest was therefore forecast to continue moving northwestward and recurve in the vicinity of this weakness. This forecast verified well except for the precise time and location of the point of recurvature. Forrest continued moving northwestward longer than expected.

Prior to recurvature, Forrest passed 107 nm (198 km) southwest of Okinawa, subjecting the island to high winds and heavy rain. Maximum sustained winds recorded at Kadena Air Base were 50 kt (26 m/s) with gusts to 74 kt (38 m/s). Rainfall totalling 11.65 inches (30 cm) resulted in flooding which caused minor damage to the installation. Other damages due to high winds were limited to minor personnel injuries and the loss of some antennas. Preliminary reports from Japanese authorities indicated that the civilian population of Okinawa weathered the storm equally well.

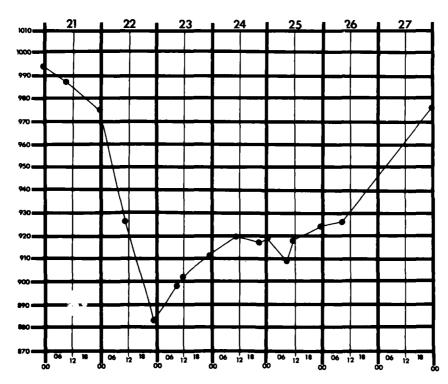


Figure 3-11-2. Intensity trends for Forrest as indicated by a plot of MSLP versus time.

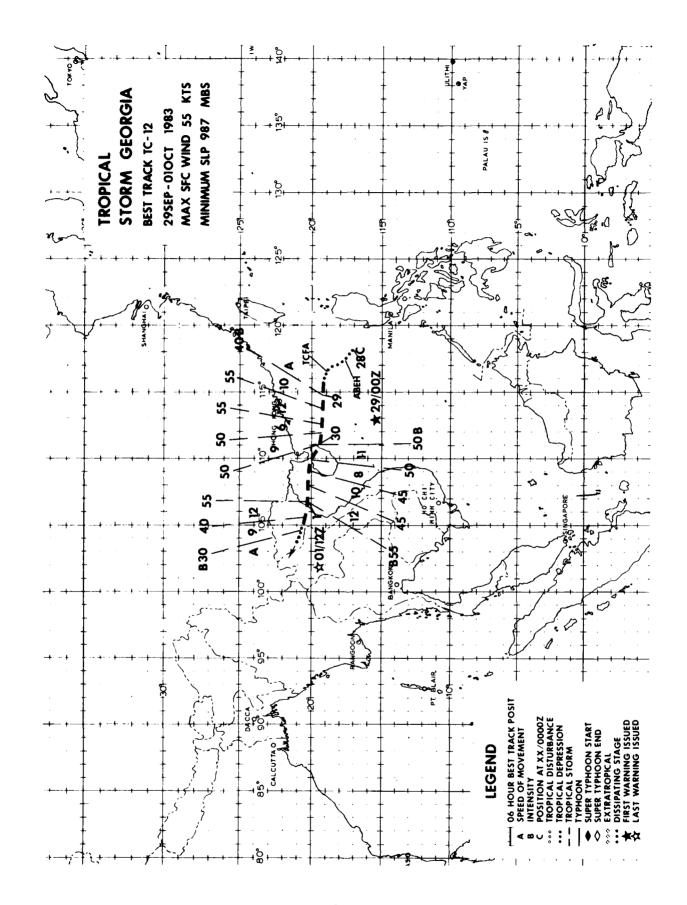
Residents of Inza Island, northwest of Okinawa, were not so fortunate. A tornado, spawned during the passage of Forrest, cleared a swath 300 ft (91 m) wide across the island, destroying seven homes and injuring 26 people, some seriously. There were also reports of tornadoes over Okinawa, however, none of these touched down.

While moving past Okinawa, Forrest began to interact with a frontal system moving off the Asian continent. Within 48 hours of the onset of this interaction, satellite imagery indicated that Forrest had lost its deep convection and had begun to take on extratropical characteristics. Shortly thereafter, Forrest recurved to the east-northeast and accelerated rapidly.

Forrest weakened dramatically while undergoing extratropical transition. This was fortunate since its track during this period carried it into heavily populated areas of southern Japan at speeds up to 40 kt (74 km/hr). While crossing the island of Kyushu, Forrest passed approximately 25 nm (45 km) south of Sasebo. Inport at Sasebo were five U.S. Navy ships and several ships of the Japanese Maritime Self Defense Force.

This harbor had previously been evaluated as a safe typhoon haven due to the sheltering effects of the topography in the area. This evaluation was proven correct when none of the ships in the harbor suffered damages during the passage of Forrest. Other areas in southern Japan suffered extensively from high winds and heavy rains. Initial reports indicated 21 dead, 86 injured and 17 missing. Heavy rains, up to 19 inches (48 cm) in some areas, caused numerous landslides and widespread flooding resulting in damages to 46,000 homes, some of which were total losses. The storm also stranded 28,000 travelers due to the disruption of domestic flights and rail service.

Forrest completed extratropical transition on the 28th at 0600Z while located near the southern tip of Shikoku. From this point on, Forrest continued to weaken and move rapidly toward the east-northeast as an extratropical system. Forrest was continued in warning status for an additional 18 hours until 190000Z when the final warning was issued. At this point, Forrest had cleared Japan and was moving eastward as an extratropical low with maximum sustained winds of 35 kt (18 m/s).



The disturbance that was to become Tropical Storm Georgia originated in a broad area of convective activity located to the west of Luzon in the South China Sea. The southwesterly monsoon was well established in this area at the time, creating an area of high cyclonic vorticity at the intersection of this flow and the easterly tradewind flow at the southern periphery of the subtropical ridge. Georgia was the first of five tropical cyclones to achieve tropical storm intensity in this active monsoon trough.

The weak surface circulation which became Georgia first came to the attention of JTWC forecasters when a upper-level anticyclone formed over it on the 28th of September. This development was accompanied by a rapid increase in the organization and intensity of the circulation. A TCFA was issued at 281459Z when the increase in organization of the system, apparent from satellite imagery, was confirmed by synoptic reports indicating that the MSLP had dropped below 1003 mb.

The circulation continued to intensify rapidly through the night. When a reconnaissance aircraft investigated the area on the following morning, it encountered a tropical storm with maximum sustained winds of 40 kt (21 m/s) and an MSLP of 996 mb. The first warning on Tropical Storm Georgia was issued on receipt of the data from the aircraft at 290000Z.

Georgia tracked westward from this point on with only a slight deviation northward in the vicinity of Hai-Nan island due to topographical effects. This track was accurately predicted by most objective techniques available to JTWC forecasters.

A strong subtropical ridge to the north of Georgia was expected to build westward during the period and keep the storm on a westward track. Daily height change analyses at 500 and 700 mb indicated that the ridge was indeed building as expected, causing Georgia to continue moving westward.

Georgia intensified to a maximum intensity of 55 kt (28 m/s) 12 hours prior to landfall on Hai-Nan island (Figure 3-12-1). The passage over Hai-Nan weakened Georgia slightly causing it to enter the Gulf of Tonkin with an intensity of 45 kt (23 m/s). However, Georgia reintensified while crossing the Gulf and made landfall on the coast of Vietnam with an intensity of 55 kt (28 m/s).

The timing and location of Georgia's arrival in Vietnam amplified the damages wrought by the storm. Georgia struck a low-lying agricultural area, Bac Bo, when the tide was rising and the rice crop was in the earing stage. Preliminary estimates of losses included 26 dead, 7,000 buildings damaged or destroyed and the loss of 247,000 acres (100,000 hectares) of rice. In surrounding areas, the arrival of Georgia proved beneficial. The rainfall associated with the storm, 13 to 14 inches (33 to 36 cm; in Thai Binh and Ha Nam provinces, signalled the end of an extensive drought. Rainfall associated with Georgia provided sufficient water to allow the cultivation of additional acreage for rice and filled lakes and reservoirs which could be used for irrigation of the winter and spring rice crops.

After making landfall, Georgia continued westward and dissipated rapidly in the mountains near the Laos/Vietnam border.

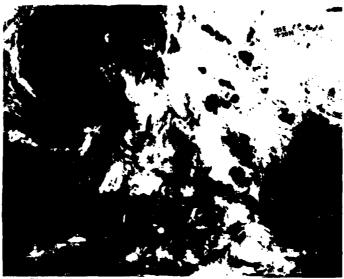
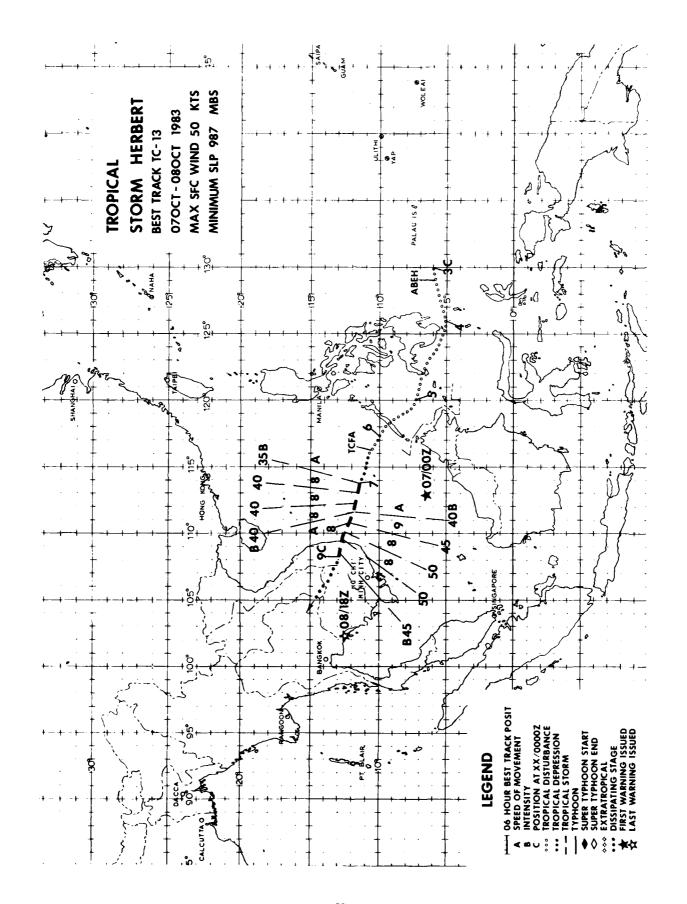


Figure 3-12-1. Tropical Storm Georgia at maximum intensity in the South China Sea (upper left). The disturbance in the lower right was the subject of a TCFA but did not develop (2910267 September DMSP infrared imagery).



TROPICAL STORM HERBERT (13W)

Tropical Storm Herbert formed from a tropical disturbance which was first observed on 3 October as an area of unorganized convective activity located 250 nm (463 km) east of Mindanao. At this time, a weak surface circulation was apparent in the synoptic wind field associated with this convection. Maximum sustained surface winds were 15 kt (8 m/s) and the MSLP was 1010 mb. In spite of the apparent weakness of this disturbance, it was closely monitored by JTWC because a TUTT cell located to the north of the disturbance provided a favorable environment for the establishment of outflow channels.

Convective activity associated with this disturbance remained high over the next three days as the circulation moved westward over the Philippines but there was no increase in the intensity of the system until it emerged in the South China Sea. On the 6th of October, the disturbance entered an area of strong southwesterly monsoon flow and began to intensify. Satellite imagery at the time indicated the

formation of convective banding in spite of the fact that upper-level flow was northeasterly and no longer highly divergent. A TCFA was issued at 0607002 on the basis of the increase in organization apparent from satellite imagery. Figure 3-13-1 shows Herbert at the time the alert was issued.

The system continued to intensify over the next 18 hours. At 0700192, a reconnaissance aircraft was able to locate a well-defined surface circulation with 35 kt (18 m/s) winds, prompting the first warning by JTWC valid for 070000Z. Forecasts for Herbert anticipated continued west-northwestward movement and minimal intensification prior to landfall on the coast of Vietnam. This scenario proved correct as Herbert achieved a maximum intensity of 50 kt (26 m/s) six hours prior to landfall north of Nha Trang, Vietnam at 081200Z. Herbert dissipated rapidly over the mountainous terrain of central Vietnam but persisted as an area of enhanced convection and reduced surface pressures for several days as it moved westward over Indochina.

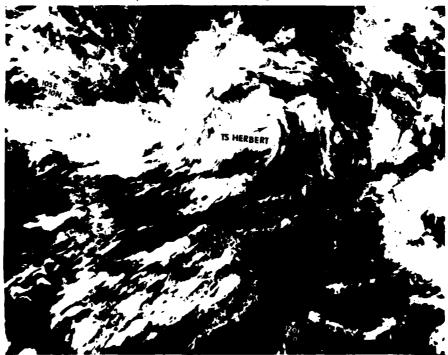
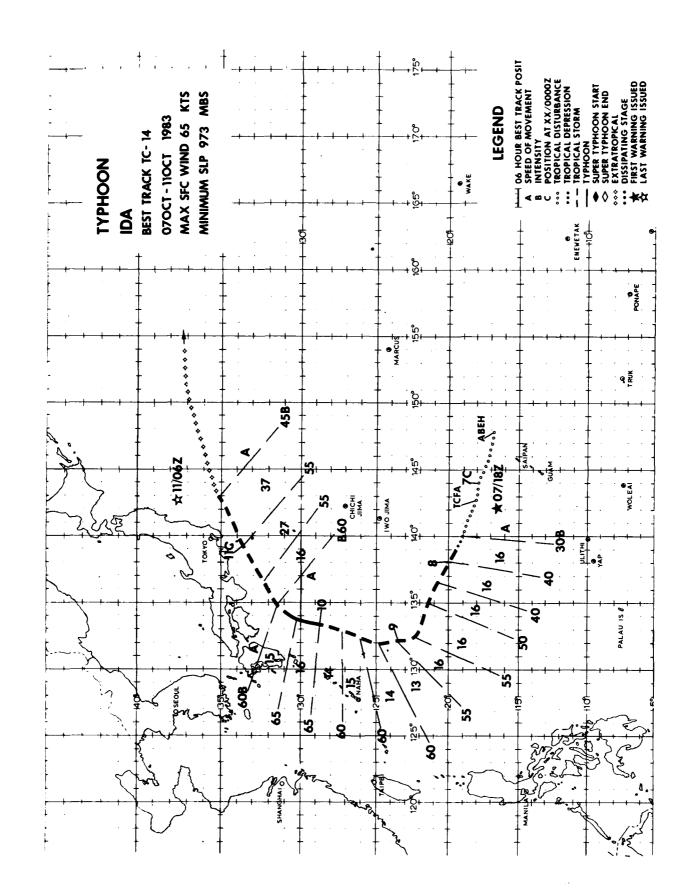


Figure 3-13-1. Herbert as a tropical depression in the South China Sea (060730Z NOAA 7 visual imagery).



The origins of Ida can be traced to an inverted trough which was first detected near Saipan (WMO 91232) using synoptic data on 6 October. Although this is the earliest point at which a reliable track can be established, there appears to be a linkage between the inverted trough and a convective cloud mass which developed approximately one week earlier in the center of a TUTT cell.

After Super Typhoon Forrest underwent extratropical transition in the vicinity of Japan, a TUTT cell located about 270 nm (500 km) west of Johnston Island (WM 91275) appeared to expand and intensify. As the frontal system, containing the extratropical remains of Forrest, passed to the north, the TUTT cell moved westward at about 10 kt (19 km/hr) and intensified. By 3 October, a mass of convective cloudiness had developed in the center of the TUTT cell near Wake Island (WMO 91245).

Over the next three days, the disturbance moved generally westward but fluctuated radically in position and intensity to the extent that it could not be reliably tracked as the same disturbance. During this period, the passage of another frontal system to the north and the formation of another TUTT cell to the southeast contributed to the confused state of the atmosphere in the area.

The inverted trough which was located near Saipan at 0600002 rapidly developed and became a closed circulation with 20 kt (10 m/s) winds by 0612002. Signs of continued development, pressure falls in the

area and increasing winds at nearby stations, led to the issuance of a TCPA at 0707452.

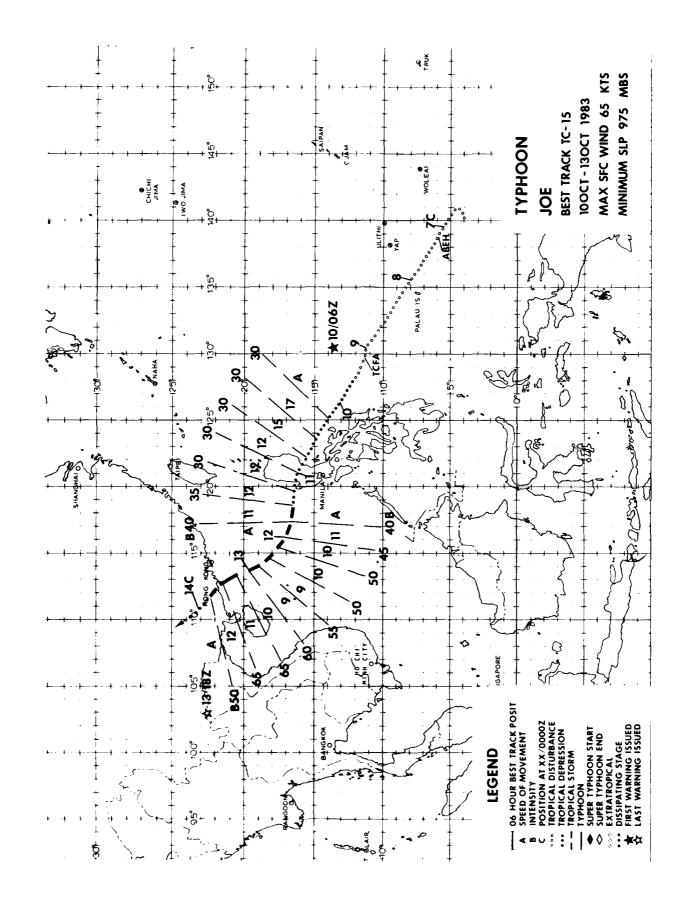
The first warning on Ida as a tropical depression was issued at 071800Z when it became evident from satellite imagery that a central convective feature was forming. Upgrade to tropical storm status followed on the subsequent warning after reconnaissance aircraft revealed that maximum sustained winds associated with Ida had risen to 40 kt (21 m/s) and MSLP had dropped to 1000 mb.

Initial forecasts called for continued northwestward movement and intensification prior to recurvature south of Japan. Ida moved northwestward as expected and intensified, reaching a maximum intensity of 65 kt (33 m/s) on the 10th after turning northnortheastward (Figure 3-14-1). Shortly after reaching maximum intensity, Ida began to interact with a frontal system to the north. This resulted in a weakening and acceleration to the northeast as Ida underwent extratropical transition. Ida's track south of Japan was well documented by timely reports from Japanese radar stations which proved invaluable in positioning the rapidly moving system.

Although Ida passed close to the island of Honshu, approximately 80 nm (148 km) southeast of Tokyo, there were no reports of storm related damage in Japan. The small radius of high winds associated with Ida and the fact that it was weakening as it passed Japan were fortunate circumstances.



Figure 3-14-1. Ida near maximum intensity. Interaction with the frontal system to the north led to the extratropical transition and rapid acceleration of the system (0922582 October NOAA 8 visual imagery).



During the month of October, tropical cyclone activity in the western Pacific was concentrated in the South China Sea. Six tropical cyclones formed between 29 September and 26 October in the western Pacific. Five of the six, formed as tropical depressions in the Philippine Sea and crossed the Philippines prior to intensifying in the South China Sea. All five moved westward without recurving. Typhoon Joe (15W) was the most intense of these and the only one of the five to achieve typhoon intensity.

Joe's origins can be traced back to 6 October when it was detected as a tropical disturbance located well to the south of Guam It was first discussed on the Significant Tropical Weather Advisor (ABEH PGTW) on the following day and was monitored by JTWC as it moved westward. At 090000Z October, synoptic data indicated that the MSLP in the disturbance was near 1006 mb and that a closed surface circulation was developing. Winds of up to 25 kt (13 m/s) were estimated from satellite analysis as convective cloudiness and organization increased. A TCFA was issued at this time in anticipation of continued intensification. The area covered by the alert was later shifted southward when satellite imagery indicated that the predominant circulation center was forming well to the south of the areas that had previously been fixed. Satellite fixes were now scattered over an area that was too large to be accounted for by either storm movement or nominal position error. The presence of multiple circulation centers was considered as a possible explanation for this excessive fix scatter.

An aircraft investigation of the area, completed at 100204Z, revealed a closed circulation center with a central pressure of 1003 mb and 30 kt (15 m/s) winds. The mission ARWO (Aerial Reconnaissance Weather Officer) reported that he suspected the presence of multiple centers, but was unable to locate any other areas of light and variable winds that would be associated with such centers.

The following aircraft reconnaissance mission also encountered perturbations in the wind field which indicated the possibility of multiple circulations. Figure 3-15-1 shows Joe as a tropical depression at the time of this mission. The arrow marks the position of the surface circulation located by aircraft. The position of the dominant circulation is not apparent from this imagery, nor is it possible to confirm the presence of multiple circulations. Synoptic data was also inadequate to afford recognition of multiple centers. Figure 3-15-2 is the surface analysis at 100000Z. Major features, such as Typhoon Ida located south of Japan, and the remains of Tropical Storm Herbert located over Indochina, are well defined. Joe appears as a tropical depression in the Philippine Sea, but data density is not sufficient to prove or disprove the presence of multiple circulations.

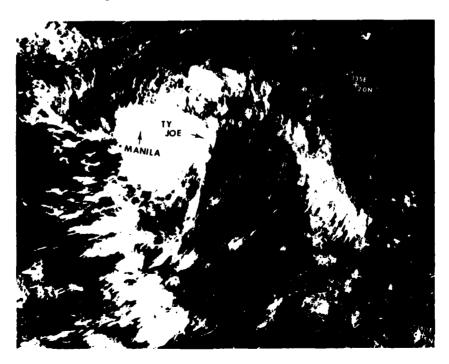


Figure 3-15-1. Satellite imagery at the time of the aircraft reconnaissance mission. {1006507 October NCAA 7 visual imagery}.

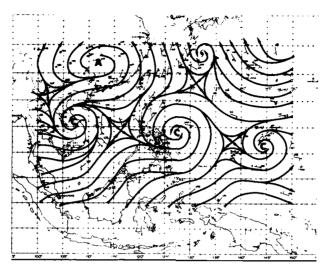


Figure 3-15-2. Surface analysis for 1000002 October showing Typhoon Ida (14W), Tropical Storm Herbert (13W), and Joe (15W) as a tropical depression in the Philippine Sea.

Joe remained poorly organized over the next 24 hours. Figure 3-15-3 illustrates the upper-level conditions which greatly affected Joe's intensity. Strong northeasterly flow to the south of the anticyclone centered near Okinawa created a shearing environment which inhibited Joe's development. This condition, combined with rapid movement over the next 24 hours, resulted in Joe approaching the Philippines as a 30 kt (15 m/s) depression with no increase in organization of intensity. As Joe crossed central Luzon, synoptic data and radar reports indicated that the system was still poorly organized.

After emerging in the South China Sea,

Joe became better organized and intensified as it moved in a wide anticyclonic track around the western periphery of the subtropical ridge. Upper-level flow patterns at this time (Figure 3-15-4) were favorable for Joe's development and allowed the formation of well-defined outflow channels to the northeast and southwest. Figure 3-15-5 shows Joe near maximum intensity. Note the symmetrical and unrestricted outflow pattern.

Joe continued to intensify as it moved northwestward reaching a maximum intensity of 65 kt (33 m/s) six hours prior to landfall. Joe dissipated rapidly after moving inland over southern China approximately 100 nm (185 km) west of Hong Kong.



Figure 3-15-3. 200 mb analysis for 1000007 October. Note the strong northeasterly flow in the vicinity of the Philippines.

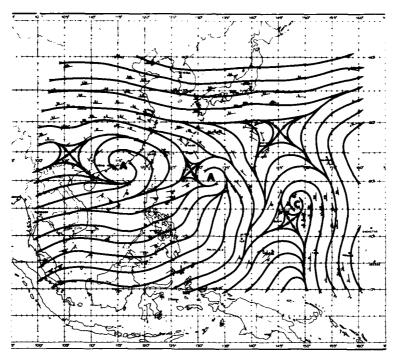


Figure 3-15-4. 200 mb analysis at 1312002 October. Comparison with Figure 3-15-3 shows a displacement of the anticyclone to the north of Joe which allowed the development of outflow channels to the northeast and southwest.

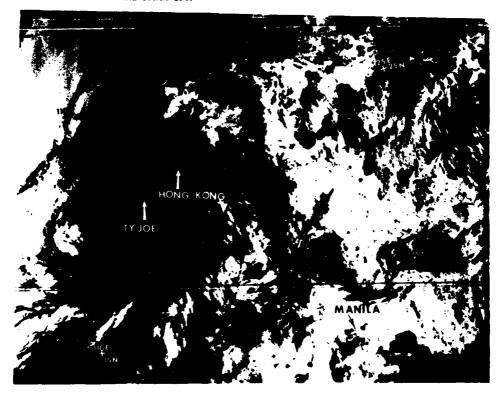
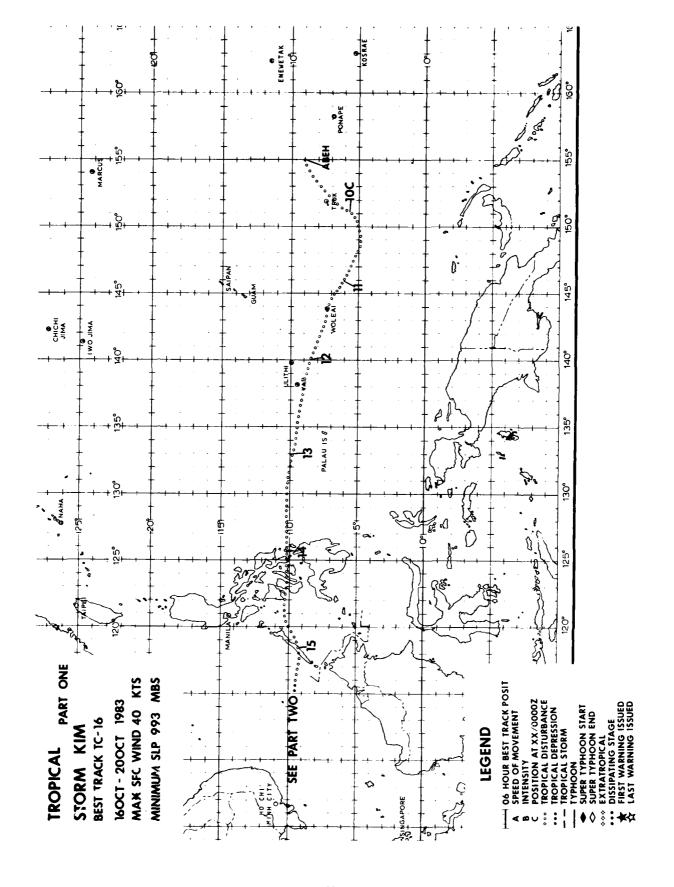
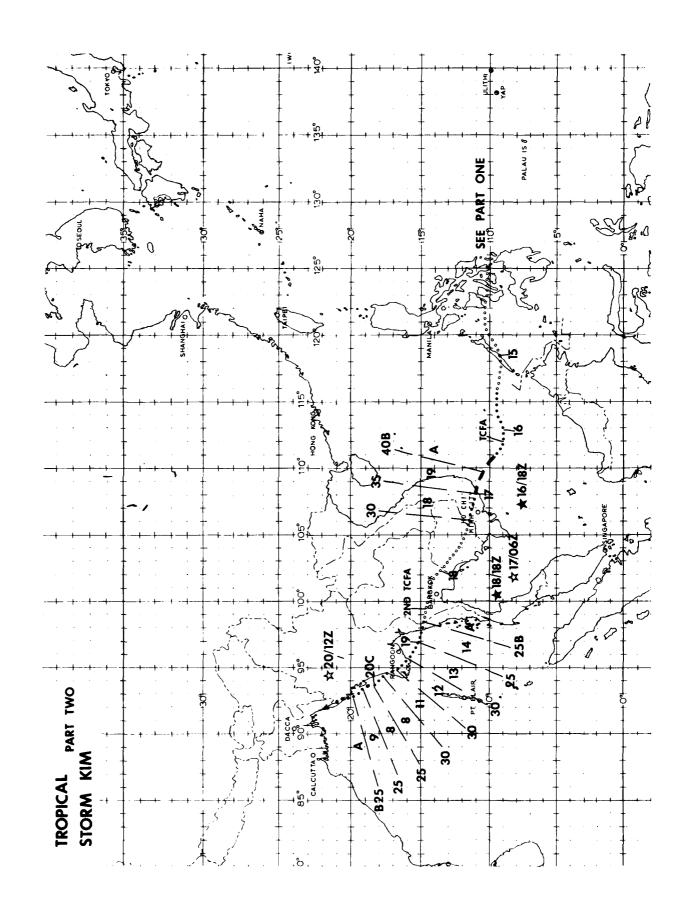


Figure 3-15-5. Typhoon Joe at maximum intensity three hours prior to landfall (1310342 October DMSP infrared imagery).





Tropical Storm Kim was the only tropical cyclone of 1983 to move from the South China Sea, across Indochina, and into the Bay of Bengal. This unusual meteorological event was permitted by the extremely low topographical resistance encountered along the storm's track across Indochina.

Tropical Storm Kim was initially detected on 9 October as a weak tropical disturbance located near 9N 153E. This disturbance was mentioned daily in the Significant Tropical Weather Advisory (ABEH PGTW) as it moved westward over the next four days. Although the disturbance was a persistent feature on satellite imagery, it showed no signs of development and was expected to dissipate over the southern Philippines. On the 14th of October, it appeared that the disturbance was dissipating in the vicinity of the Sulu Sea. At this point, the dis-turbance had lost its convective signature on satellite imagery and was no longer identifiable as a disturbance. However, on the following day, the system emerged in the South China Sea, developed rapidly into a tropical depression, and moved westward at speeds of 11 to 14 kt (6 to 7 m/s). The southwest monsoon was well-developed over the South China Sea at this time, providing an environment favorable for continued development. In view of Kim's position and the fact that several previous depressions had intensified in this environment, a TCFA was issued at 160459Z.

Kim intensified while transitting the South China Sea, reaching tropical storm intensity at 1612002. Figure 3-16-1 shows Rim just prior to achieving tropical storm intensity near the coast of Vietnam. The first warning on Kim was issued at 1618002, five hours prior to landfall on the coast of Vietnam.

Although Kim was a relatively weak

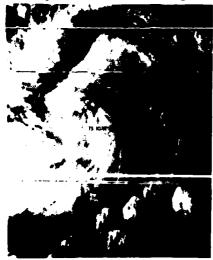


Figure 3-16-1. Kim as a tropical depression just prior to reaching tropical storm intensity off the coast of Vietnam (1607082 October NOAA 7 visual imagery).

tropical storm, its rapid development just prior to landfall resulted in much human suffering. Preliminary reports indicated that more than 200 people, most of them fishermen, died or were lost. Property damage was also unusually high, with 300 boats and ships, 3,000 houses, and 19,750 acres (8,000 hectares) of rice destroyed.

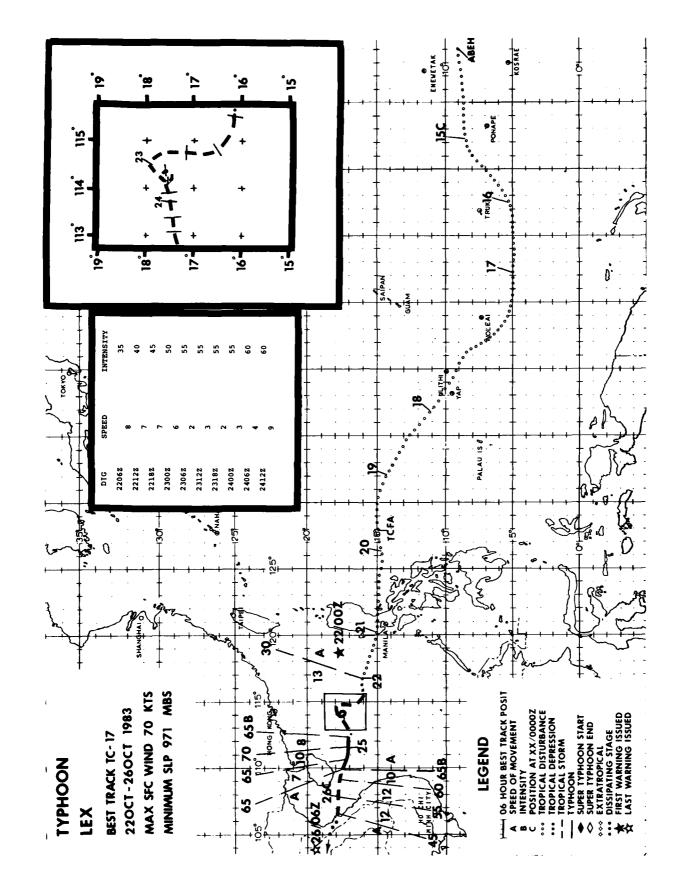
Warnings on Kim were suspended shortly after landfall as the circulation weakened rapidly over land. Kim was downgraded to a tropical depression at 170600Z as it crossed the border from Vietnam into Kampuchea. Six hours later it was classified as a tropical disturbance.

Kim continued tracking across Indochina with a great deal of associated convection and some indications of a middle to lower level circulation apparent in visual satellite imagery. Kim's ability to maintain its intensity during this period may be attributed to the flat terrain encountered along its track and the fact that it was never more than 100 nm (185 km) from water.

A second TCFA was issued for Kim at 181359Z when it became apparent that the disturbance would move into the Andaman Sea where regeneration was considered likely. Warnings for Kim were resumed on the following day as tropical depression intensity was achieved over the Andaman Sea (Figure 3-16-2). At this time, Kim was expected to cross the southern tip of Burma and further intensify in the Bay of Bengal. Kim moved across southern Burma as expected but never actually got out over open water in the Bay of Bengal. Instead, Kim moved northward along the coast of Burma, parallel to the axis of the Arakan Mountain Range, and weakened steadily. The final warning was issued as the system dissipated on the 20th at 1200Z.



Figure 3-16-2. Tropical Cyclone 16W (Kim) after regeneration in the Andaman Sea (1908212 October NOAA 1 visual imagery).



The tropical disturbance which became Lex was extremely slow in developing and achieved Typhoon intensity for a period of only one day. Yet it was one of the most damaging cyclones of the season, responsible for the loss of a ship in the South China Sea and extensive suffering in central Vietnam where it eventually made landfall.

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Lex was monitored as a tropical disturbance for eight days prior to issuance of the first warning on the system as a tropical depression. It was first detected in the vicinity of the Marshall Islands on 14 October when satellite imagery revealed the presence of an area of active convection near 9N 164E. Synoptic data in the area at this time indicated that there was not a surface circulation associated with the disturbance but did indicate a 24-hour drop of one to two millibars in sea-level pressure at nearby stations.

The disturbance underwent diurnal fluctuations in its convection as it moved westward but showed no signs of increasing in intensity until the 16th. On the 16th, while located near Truk (WMO 91334) at 5N 151E, an upper-level anticyclone began to develop over the disturbance and the system became better organized.

Over the next three days, the disturbance continued to intensify slowly as it moved westward across the Philippine Sea. Satellite imagery during this period indicated that the upper-level anticyclone was continuing to develop and that convective activity associated with the disturbance was increasing in size, organization, and intensity. Synoptic data indicated the presence of a weak 10 to 15 kt (5 to 8 m/s) surface circulation with an MSLP of 1008 mb.

A TCFA was issued for this disturbance at 1920002 as it approached the Philippines approximately 180 nm (333 km) northeast of Cataduenas Island. A reconnaissance aircraft was dispatched to the area at this time but was unable to close off a surface circulation. The alert was reissued twice as JTWC monitored the progress of this disturbance while it was crossing the central Philippines. The topography of the Philippine Islands had little effect on the disturbance and it emerged in the South China Sea with no appreciable decrease in its organization.

Lex began to intensify while moving west-northwestward away from Luzon. The first warning on Lex was issued on the 22nd at 0000Z when satellite imagery indicated that the cloud bands associated with the system were taking on a comma-shaped appearance. Although Lex was designated as a tropical depression on the initial warning, upgrade to tropical storm status followed quickly when a reconnaissance aircraft encountered 35 kt (18 m/s) winds while fixing the system at 220535Z.

Lex was expected to continue intensify-

ing slowly and move west-northwestward toward Hai-Nan island along the southern periphery of the subtropical ridge. scenario appeared to be inaccurate when Lex began moving slowly northward after 220600Z. This slow northward movement culminated in a counter-clockwise loop near 17.5N 114.5E, approximately 300 nm (556 km) south of Hong Kong. The movement of Lex during this period was in response to the passage of a developing mid-level trough over China. This trough penetrated farther to the south than was expected, causing a weakness to develop in the subtropical ridge to the north of Lex. It appeared that this trough would cause a complete breakdown of the ridge to the north of Lex, allowing the storm to drift northward toward Hong Kong. Figure 3-17-1 shows the position of this trough as Lex began its cyclonic loop. The interact of Lex with this trough was also apparent in satellite imagery at the time (Figure The interaction 3-17-2). Twelve hours after this scenario was adopted on the 230600Z warning, the subtropical ridge re-established itself to the north of Lex and the storm resumed a westward track.

Lex intensified while moving westward, reaching a maximum intensity of 70 kt (36 m/s) at 0000Z on the 25th. Gradual weakening occurred over the next 24 hours as Lex passed to the south of Hai-Nan island. The interaction of the circulation with the rugged terrain of Hai-Nan had a pronounced effect on the system. The decrease in organization and convection, apparent from satellite imagery, led to the downgrade of Lex to tropical storm status at 251800Z. Lex weakened further while transitting the Gulf of Tonkin, making landfall near Dong Hoi, Vietnam with maximum sustained winds of 50 kt (26 m/s). Lex dissipated rapidly over the rugged terrain of central Vietnam and Laos after causing extensive damage to low-lying areas in its path.

According to preliminary reports from Vietnam, areas near the point of landfall were devastated by the high winds and torrential rains associated with Lex. Damage was extensive as rivers rose six feet (2 m), resulting in widespread flooding. Hundreds of people were killed or injured, 17,000 homes were destroyed, and six hospitals were seriously damaged. In addition, an estimated 100,000 tons of starch food may have been lost due to the flooding.

Other damage caused by Lex came to light after the dissipation of the storm. The oil drilling ship, Glomar Java Sea, was operating in the vicinity of Hai-Nan island during the passage of Lex. A search was conducted for the ship after radio contact was lost during the storm. The 5,926 ton vessel was finally located using sonar under 300 ft (91 m) of water about 60 nm (111 km) south of Hai-Nan island. There have been no reports of survivors from the crew of 81.

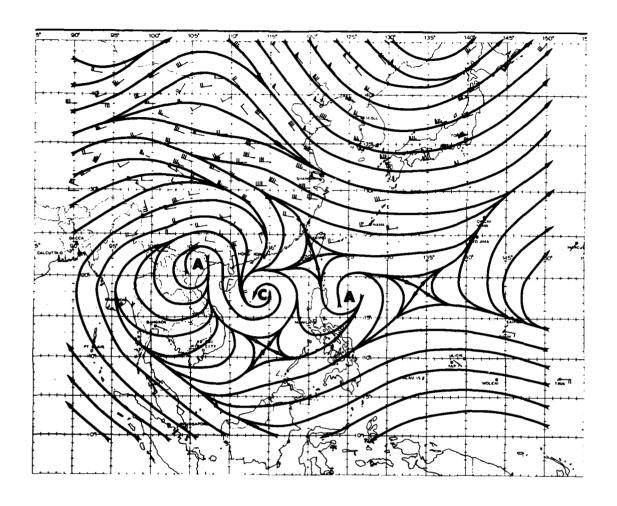
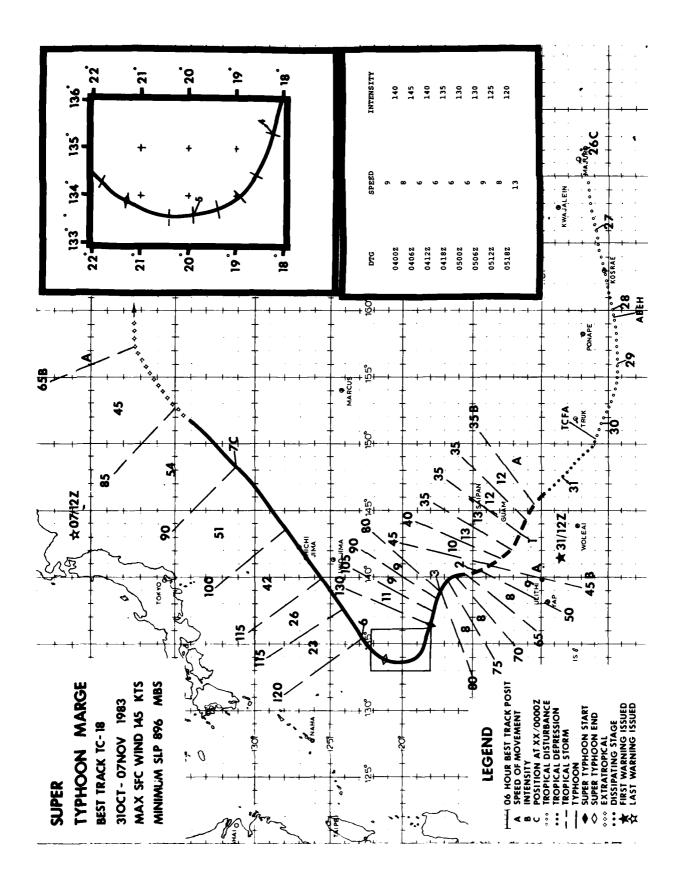


Figure 3-17-1. Orientation of the mid-level trough which briefly interacted with Lex (2300002 October 500 mb analysis).



Figure 3-17-2. Lex as a tropical storm while undergoing a cyclonic loop (2310262 October DMSP infrared imagery).



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The tropical disturbance which developed into the fourth super typhoon of the season was initially detected on 26 October as an area of unorganized convection associated with a weak surface circulation near 7N 1.72E. Synoptic data at the time indicated that surface winds associated with the disturbance were weak, 5-10 kt (3-5 m/s) and MSLP was 1012 mb. This disturbance organized slowly over the next four days as it moved westward along the monsoon trough axis. During this period, an upper-level anticyclone formed in close proximity to the low-level circulation. This development was accompanied by a drop in MSLP to 1008 mb and a concurrent increase in the convective activity associated with the circulation. This led to the issuance of a TCFA on the 30th at 1035Z.

During the 24 hour period following the issuance of the TCFA, satellite imagery showed that the convective activity associated with the circulation was undergoing further consolidation and that outflow channels were developing to the northeast and southwest. Synoptic data and Dvorak satellite analysis indicated maximum sustained winds of 25 to 35 kt (13-18 m/s), prompting the issuance of the first warning at 3112002.

At this point, Marge was located 180 nm (333 km) south of Guam. The subtropical ridge in this area was expected to weaken in response to the passage of an intense midlatitude trough. Forecasts issued during this period projected that Marge would react to the passage of this trough, moving slowly

northwestward, then recurving to the northeast. Marge moved northwestward as expected, but did not recurve. By the time Marge arrived in a position to recurve in advance of the trough, the trough had already passed to the north and Marge came under the influence of low-level easterly flow associated with a high upstream of the trough. This resulted in Marge resuming a northwestward track prior to subsequent recurvature in advance of another mid-latitude trough.

Premature adoption of the recurvature scenario greatly affected the accuracy of the intensity forecasts. Marge achieved typhoon intensity on 2 October at 0600Z. This was not far from the forecast intensity for this time. However, two days later, on the 4th, Marge was a 145 kt (75 m/s) super typhoon. Since, by the 4th, Marge was initially expected to be weakening after recurvature, unusually large intensity errors occurred.

Shorter range intensity forecasts met with greater success. Use of an objective aid for the prediction of explosive deepening (Dunnavan, 1981) resulted in fairly accurate 24 hour intensity forecasts verifying at maximum intensity. At 06002 on the 3rd, this technique predicted that Marge would undergo explosive deepening. Within 24 hours of this prediction, Marge's intensity increased from 90 kt (46 m/s) to 145 kt (75 m/s). Marge did not recurve initially as forecast and, when recurvature did occur, moved at speeds much higher than anticipated while rapidly



Figure 3-18-1. Marge in the early stages of recurvature. At this point, maximum sustained winds were 115 kt (59 m/s) and speed of movement was 25 kt (46 km/hr) (06061!? November NOAA 7 visual imagery).

evolving into an extratropical system. This resulted in large position errors. Figure 3-18-1 and 3-18-2 give some indication of the rapidity with which Marge underwent extratropical transition. Although there is only 17 hours elapsed time between the two pictures, there is a striking difference in Marge's appearance. In Figure 3-18-1, Marge appears as a well developed typhoon with a circular eye and maximum sustained winds of 115 kt (59 m/s). In Figure 3-18-2, Marge is nearing the end of its transition to an extratropical system while moving northeastward at a speed of 51 kt (95 km/hr).

Marge's high speed of movement during recurvature was phenomenal. At 0512002, the forecast called for recurvature with acceleration to a maximum speed of 35 knots. This forecast predicted that Marge would more than quadruple its speed of forward motion since the storm was only moving at 8 kt (15 km/hr) at the time. However, this forecast fell far short of the 54 kt (100 km/hr) speed actually attained by Marge.

Marge's high speed of movement following recurvature contributed to the deformation of the wind field associated with the storm. Marge became very asymmetric, with winds in its southeast semicircle much higher than winds in the northwest semicircle. This was due to the addition of its speed of translation to the circulation wind field on the southeastern side and the corresponding decrease in winds on the northwestern side. This made it appear that Marge's circulation weakened more slowly than it actually did since the measure of the intensity of a system is the maximum surface wind, without regard to symmetry.

The asymmetric nature of Marge's wind field proved beneficial to the crew of the Colombian Navy Sailing Ship ARC Gloria. Gloria was fortunate enough to encounter the weak northwestern portion of Marge's circulation. Even so, Gloria reported seas to 30 ft (9 m) and winds gusting to 90 kt (46 m/s) as Marge passed to the southeast. The high winds and heavy seas encountered by Gloria resulted in the injury of three crewmen, the loss of a motor boat and five sails, and minor structural damage.

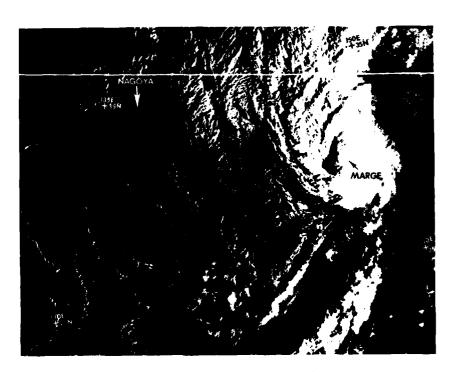
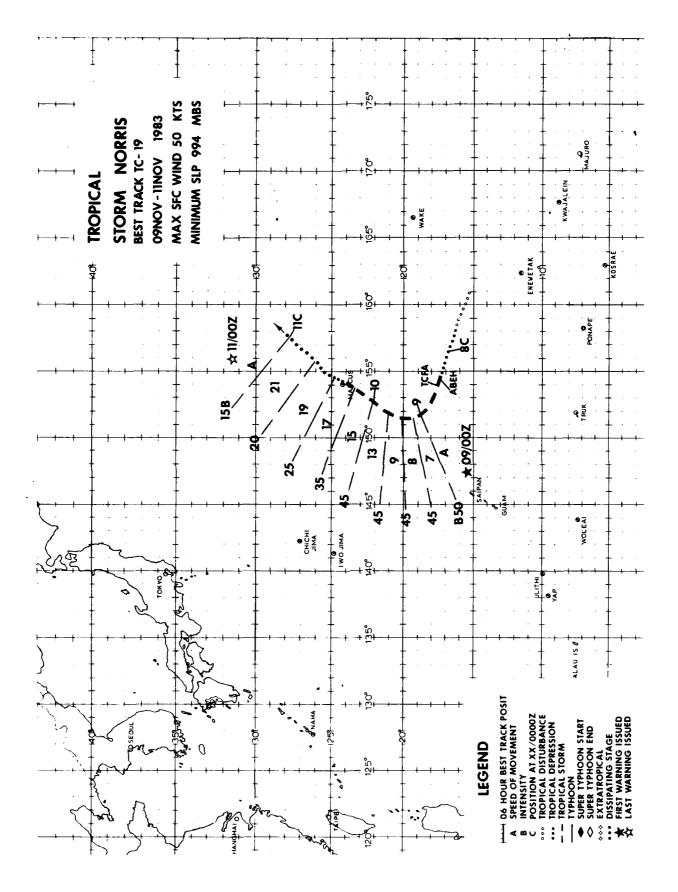


Figure 3-18-2. Marge just prior to completing transition to an extratropical system. Maximum sustained winds were 90 kt (46 m/s) and speed of movement was 51 kt (95 km/hr) (0622542 November NOAA 8 visual imagery).



TROPICAL STORM NORRIS (19W)

On the day following the final warning on Super Typhoon Marge, a surface circulation appeared on visual satellite imagery to the east of the front associated with the remants of Marge. This circulation was located in a data sparse area and had very little associated convective activity. Although depicted as small and unimpressive on the satellite imagery, the circulation quickly evolved into a midget tropical storm. A TCFA was issued at 0808492 when the deformation of the low-level cloud-lines on satellite imagery indicated that the circulation was well organized. A reconnaissance aircraft was dispatched on the following morning to investigate. When the aircraft arrived at the expected position of the circulation, it encountered light and

variable winds with no indication of the presence of a surface circulation. Upon receipt of this report from the aircraft, the expected position was revised on the basis of updated satellite imagery and the aircraft was vectored eastward to a new position. Only 130 nm (241 km) to the east-southeast of its previous position, the aircraft encountered a well-developed tropical storm with 50 kt (26 m/s) winds and a circular eye 15 nm (28 km) in diameter. The first warning on Tropical Storm Norris was issued upon receipt of this report. Figure 3-19-1 shows Norris at the time of the reconnaissance mission. Although an eye is not apparent on satellite imagery, Norris does appear as a highly organized (though extremely small) tropical storm.



Figure 3-19-1. Tropical Storm Norris at maximum intensity just prior to recurvature. Less than 48 hours later, Norris was completely absorbed by the front which appears to the left in the picture (082211Z November NOAA 8 visual imagery).

The position of Norris, to the east of an advancing front, led to a straightforward forecast of recurvature and dissipation which verified well. Less than three days after its initial detection, Norris had been completely absorbed by the advancing front and was no longer identifiable as a distinct entity.

Post-analysis revealed that Norris developed rapidly from a pre-existing disturbance of small proportions. Figure 3-19-2 shows Norris at 080931Z, near the time of issuance of the TCFA. Although there is little convective activity associated with the circulation, the organization of the low-level wind field is evident in the alignment of the cloud lines. This

low-level banding is also evident in visual satellite imagery 12 nours prior to the TCFA. However, imagery prior to that shows only a small unorganized disturbance moving rapidly northwestward. Norris' rapid development was, in part, due to favorable upper-level conditions which existed at that time. Figure 3-19-3 shows that Norris developed in an area of light but highly divergent upper-level flow.

Norris never posed a threat to any major land mass but was a subject of great concern to shipping in the area. Fortunately, Norris' movements were accurately forecasted and the ships involved were able to avoid the tiny but powerful circulation.

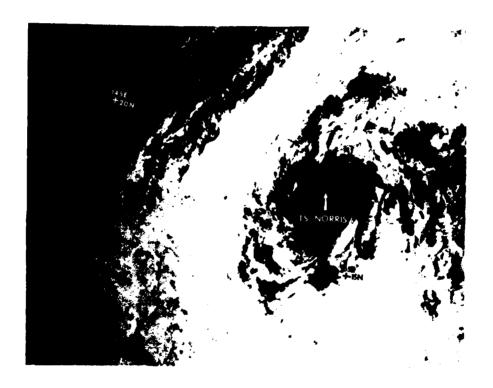


Figure 3-19-2. Norris at the time of issuance of the TCFA (080931Z November NOAA 8 infrared imagery).

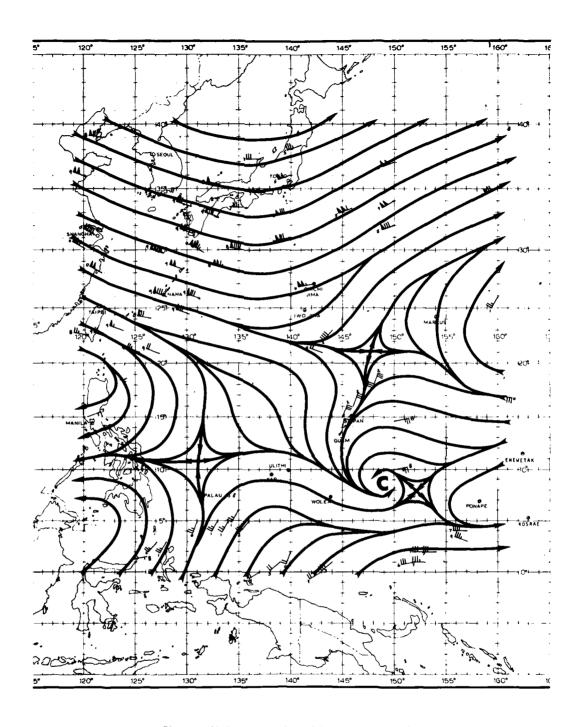
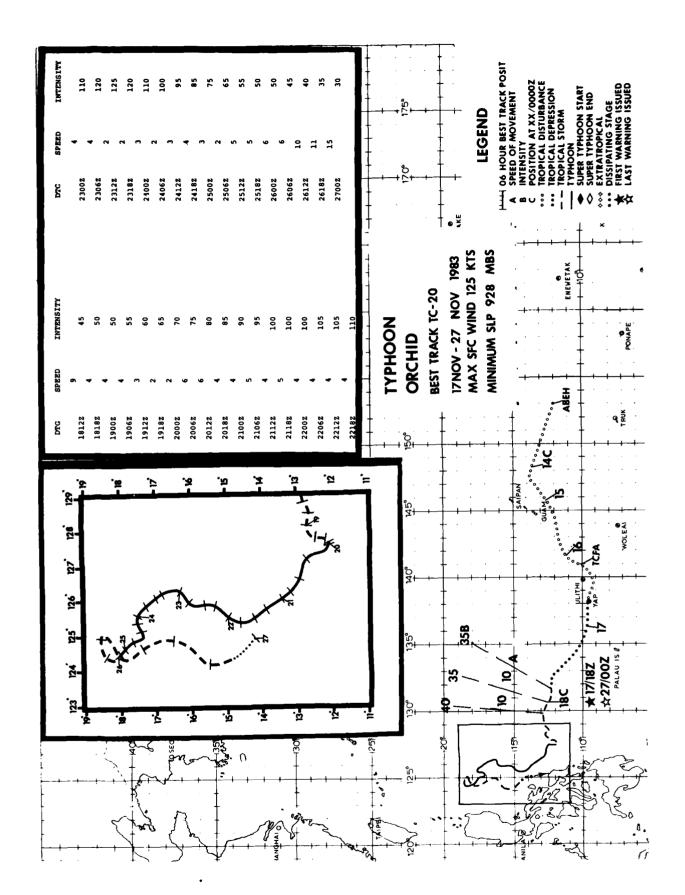


Figure 3-19-3. Norris formed in an area of light but highly divergent upper-level flow to the northeast of a TUTT cell (0812002 November 200 mb analysis).



Typhoon Orchid was the first of three tropical cyclones to develop in the western North Pacific during mid-November. This flurry of activity in the northern hemisphere was accompanied by the development of two tropical cyclones in the southern hemisphere, Tropical Cyclone 04S and Tropical Cyclone 05S (Quenton). The establishment of strong low-level westerlies at low latitudes on both sides of the equator preceded the onset of activity.

Orchid developed from a tropical disturbance which was first detected on the 12th of November as an area of convective activity located 300 nm (556 km) north of Truk (WMO 91334). The disturbance moved southwestward over the next three days as its convection increased in intensity and size. The first aircraft reconnaissance mission to investigate the disturbance was conducted on 15 November while the disturbance was located 170 nm (315 km) southwest of Guam (WMO 91212). This mission did not succeed in closing off a circulation and indicated that the disturbance was a broad area of low pressure (MSLP of 1004 mb) with maximum sustained surface winds of 25 kt (13 m/s). Later satellite imagery indicated that the disturbance was becoming better organized. An increase in convective activity, accompanied by the development of an upper-level anticyclone led to the issuance of a TCFA at 0300Z on the 16th. Α second aircraft reconnaissance mission, on the 17th, was also not able to close off a circulation and provided data indicating that there was little change in intensity from the previous mission. This information did not correlate with observations from satellite imagery which continued to show a marked increase in the organization of the system. Post-analysis revealed that the aircraft was investigating features not

associated with the dominant circulation to the northwest. The first warning on Orchid as a tropical storm was issued at 1800Z on the 17th when intensity estimation by satellite indicated that maximum sustained winds were in the 40-45 kt (21-23 m/s) range.

Orchid's movement from this point on was highly erratic. Strong low-level northeasterlies were opposed at higher levels by southwesterly flow which resulted in a continual conflict in steering. This complex environment was further complicated by the development of Typhoon Percy in the South China Sea (Figure 3-20-1). The separation distance between Orchid and Percy remained constant at 850 nm (1574 km) throughout the period of their coexistence. Although there was not a Fujiwhara interaction observed in this case, the possibility of interaction was under constant consideration by JTWC forecasters.

In spite of the effects of vertical shear experienced by Orchid and Percy, both systems achieved typhoon intensity. maximum intensity of 125 kt (64 m/s) was accompanied by an MSLP of 928 mb measured by aircraft on the 23rd. However. both systems eventually succumbed to the effects of vertical shear. Two days after reaching maximum intensity, Orchid had weakened significantly. Although maximum sustained winds were 55 kt (28 m/s), MSLP was up to 995 mb. Winds associated with Orchid were higher than might be expected for a circulation with such a high central pressure because ambient lowlevel flow was particularly strong. Goforce northeasterlies on the northwest Gale side of Orchid's circulation augmented the winds on that side, resulting in a band of high winds which were much stronger than the winds on the southeast side of the circulation.

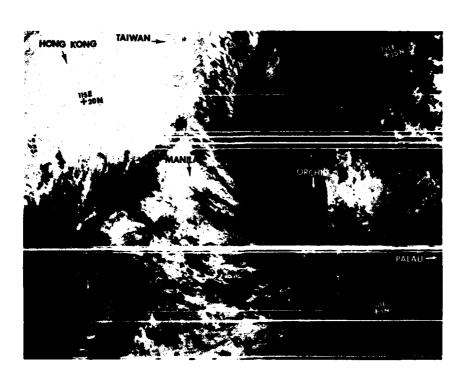


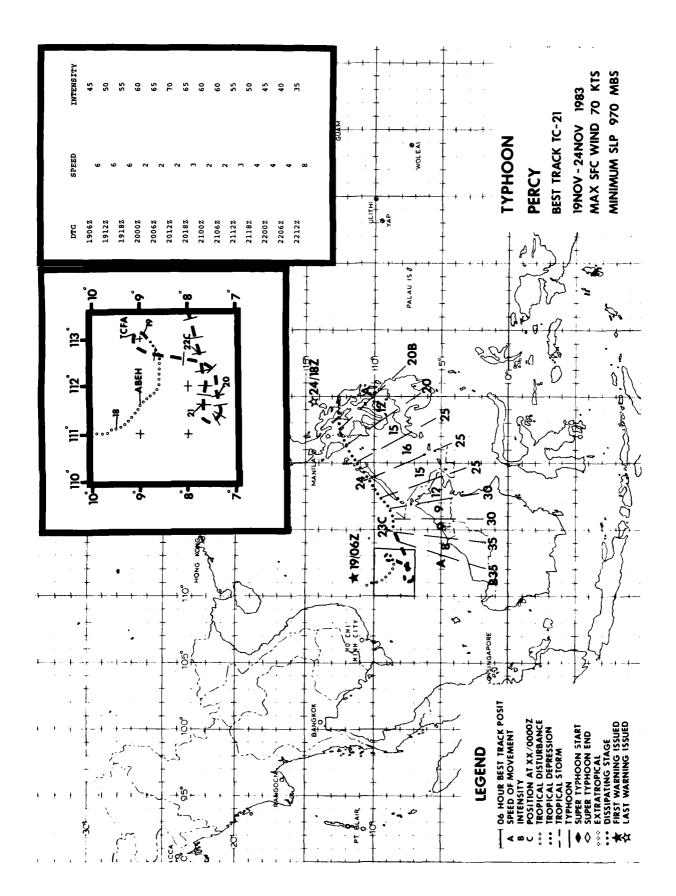
Figure 3-20-1. Orchid as a tropical storm (right) and the disturbance which developed into Typhoon Percy (left) (182336Z November NOAA 8 infrared imagery).

As Orchid weakened, the influence of low-level steering became greater and the circulation moved southward. By the time of the final warning, Orchid was located 40 nm (74 km) west of the position it had occupied five and a half days earlier.

Although Orchid posed a threat to the Philippine Islands for several days, landfall was not made on any of the islands. However, high winds and seas associated with Orchid posed a hazard to maritime interests at great distances from the center. An inter-island ferry, MV Dona Cassandra (487 tons) capsized and sank in the Suriago Strait during a transit between Butuan,

Mindanao and Cebu. Of the 387 passengers and crew onboard, 167 were killed.

In addition to the loss of the Dona Cassandra, Orchid was responsible for damages to the SS Mallory Lykes. Mallory Lykes was headed west across the Philippine Sea when she passed close to Orchid's center. The 60 kt (31 m/s) winds and 24 ft (7 m) seas encountered by the ship caused two engines carried as cargo to break free of their lashings. These eight ton engines caused considerable damage to hull frames and plating as they clattered about but fortunately did not injure any personnel.



TYPHOON PERCY (21W)

From genesis to dissipation, every aspect of Percy's life was affected in some manner by its proximity to Typhoon Orchid (20W). As Orchid neared the Philippines on 17 November, an area of upper-level divergence was created over the South China Sea where Orchid's outflow split into southerly and easterly components. Beneath this upper-level divergence, the confluence of the north-asterly monsoon and the south-westerly inflow into Orchid created an area of high positive vorticity. Typhoon Percy formed in this fertile environment.

A tropical disturbance quickly formed but showed no signs of further development until 1600Z on the 18th. In the eight hour period between 181600Z and 190000Z, the disturbance intensified rapidly, forming convective bands and an upper-level anticyclone. A TCFA was issued at this time and was followed rapilly by a warning when continued intensification became apparent from satellite imagery (Figure 3-21-1). A reconnaissance aircraft investigated the area shortly after issuance of the first warning and found a well-developed tropical storm with a circular eye and maximum sustained winds of 50 kt (26 m/s).

Percy moved very erratically for the first four days in warning status. After completing a series of loops and feints, Percy's position at 230600Z was only 90 nm (170 km) from its position at 190600Z. The

proximity of Orchid to the northeast of Percy and the complicated steering environment in which both systems were embedded made forecasting especially difficult. The possibilities were endless; Fujiwhara interactions or the entrainment of one system into the other were two of the scenarios considered at the time by JTWC forecasters.

Percy eventually sheared and became embedded in Orchid's inflow, but not before achieving typhoon status and a maximum intensity of 70 kt (36 m/s). The reports of reconnaissance aircraft throughout Percy's life best tell the story. On 19 November, the first aircraft encountered a welldeveloped tropical storm with 50 kt (26 m/s) winds and a circular eye. The next mission at 200905Z encountered a 70 kt (36 m/s) typhoon with an MSLP of 971 mb. By 202344Z, Percy was beginning to shear and the aircraft reported a ragged elliptical eye with a poor radar presentation. The 210950Z reconnaissance flight reported that Percy no longer had an eye and that all clouds were below the 700 mb flight level. By the time of the 230241Z mission, Percy was an exposed lowlevel circulation with maximum sustained winds of 35 kt (18 m/s). The final aircraft reconnaissance mission, at 240200Z, was unable to fix Percy. The final warning on Percy was issued at 241800Z when it became impossible to identify the circulation.

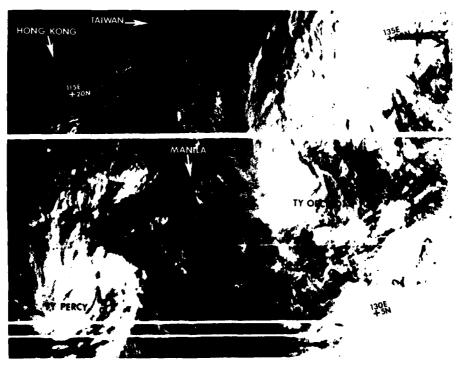
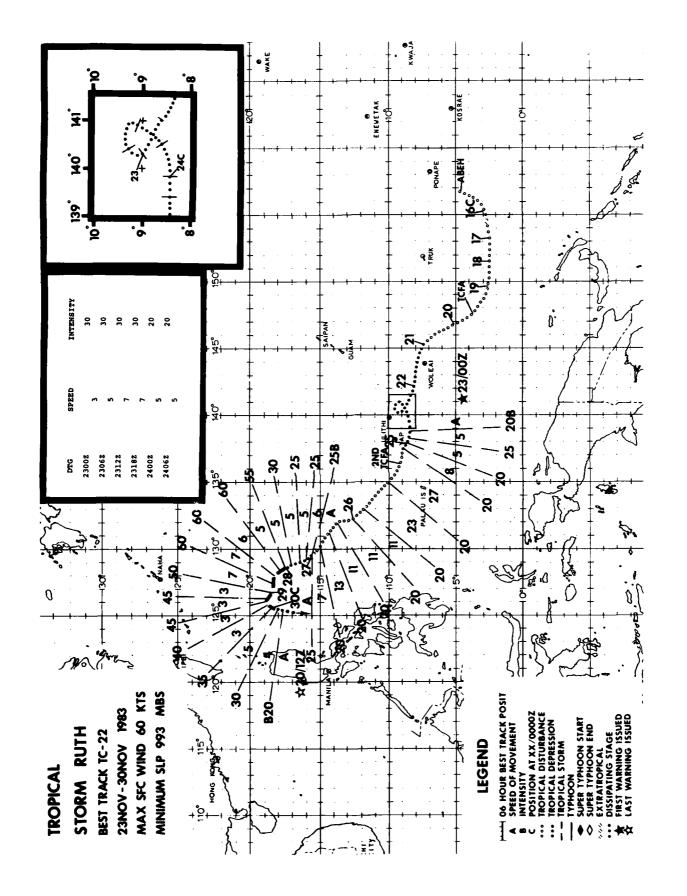


Figure 3-21-1. Percy (left) and Orchid (right), both at tropical storm intensity (1823362 November NOAA 8 visual imagery).



SECTION PRODUCTION DESCRIPTION DESCRIPTION PRODUCTION ASSESSED.

Ruth was one of the more erratic storms of 1983. It dissipated, regenerated, looped, moved at speeds varying from 3 to 25 kt (6-46 km/hr), and was the subject of four TCFA's and two final warnings.

Ruth was first detected as a tropical disturbance embedded in the near-equatorial trough southeast of Guam. The disturbance was discussed in the Significant Tropical Weather Advisory (ABEH PGTW) on 15 November and was monitored closely for the next four days as it moved westward along the trough axis. Little change in organization or intensity was observed during this period. MSLP was fairly constant at 1008 mb and surface winds in the area were 5-10 kt (3-5 m/s).

On the 19th of November, the disturbance showed signs of development. Associated convective activity expanded to cover a large area approximately 1200 nm (2222 km) east and west by 900 nm (1667 km) north and south. Convection was intense and weakly banded into a center near 5N 147E. A TCFA was issued for the disturbance at 1916002 when surface winds picked up to 15-25 kt (8-13 m/s).

The disturbance was continued in alert status for four days as it moved slowly northwestward without any further development. Aircraft reconnaissance flights into the area on the 20th and 21st were unable to close off a surface center and provided data indicating the presence of a surface trough or circulation of synoptic scale. Ruth's arrested development at this stage was due to the presence of Orchid to the west and the passage of a frontal system to the northwest. Although inflow on the north side of Ruth was provided in abundance by the Trade Winds, inflow on the south side was very weak. Most of the low latitude westerly flow was drawn into Orchid leaving an area of weak westerlies to the east of Orchid flowing into Ruth. The frontal system to the northwest of Ruth interacted with the subtropical ridge to create an area

of enhanced mid-level flow inhibiting the development of a circulation at the mid-levels.

In spite of these factors, Ruth was able to maintain convective organization and even intensified slightly with maximum sustained winds reaching 30 kt (15 m/s). A reconnaissance aircraft on an investigative mission at 222345Z was able to close off a surface circulation with MSLP of 1004 mb. The first warning on Ruth as a tropical depression was issued on receipt of this report and projected continued slow intensification and north-northwestward movement.

Ruth maintained 30 kt (15 m/s) intensity for the next 24 hours as it completed an anticyclonic loop but appeared on satellite imagery to be shearing in the process. Warnings were terminated at 240000Z after data from reconnaissance aircraft indicated that maximum sustained winds associated with the circulation were 20 kt (10 m/s).

Over the next four days, Ruth moved quite erratically while exhibiting wide ranging fluctuations in its convective signature on satellite imagery. A TCFA was issued at 250820Z when reconnaissance aircraft located a broad circulation with maximum surface winds of 25 kt (13 m/s) and MSLP of 1004 mb. Ruth remained in alert status until satellite imagery on the 26th indicated that the circulation was shearing. Ruth was placed in alert status again at 2703432 when it appeared from satellite imagery that the circulation was regaining vertical alignment. Synoptic conditions at this time were favorable for further development. Typhoon Orchid had weakened to a tropical depression and no longer competed with Ruth for inflow. At the same time, the destructive interaction between Ruth and the frontal system previously discussed was broken as the front propagated eastward.

Ruth flourished in this environment and intensified rapidly. A reconnaissance aircraft reported surface winds of 55 kt

(28 m/s) and MSLP of 997 mb at 2723402 just prior to the resumption of warnings on Ruth at 2800002. Maximum winds associated with Ruth were higher than would be expected from the MSLP due to the enhancement of Ruth's circulation by an intense northeasterly monsoon gale area on its northwest side.

Ruth peaked at a maximum intensity of 60 kt (31 m/s) briefly on the 28th before the shearing effects of its environment

caused it to weaken for the final time. Ruth was able to intensify to near typhoon intensity in spite of its location in an area of moderate vertical shear. However, when the northeasterly monsoon flow was enhanced further by a cold outbreak from the continent, the resultant increase in vertical shear proved to be too much for the plucky little system. Ruth weakened rapidly after shearing and dissipated as an exposed low-level circulation on the 30th.

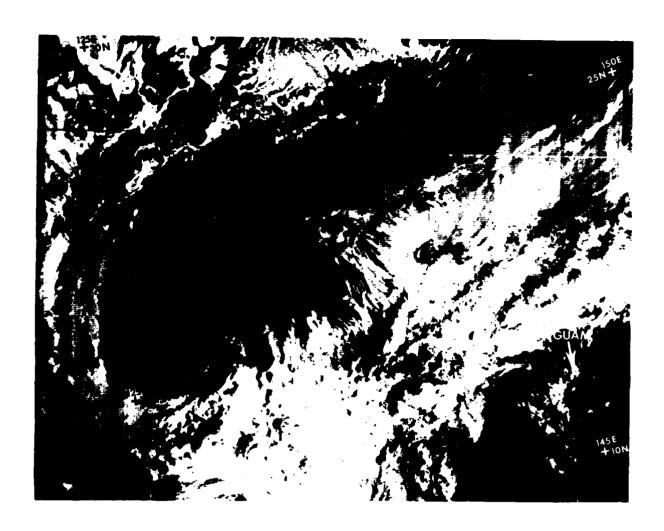
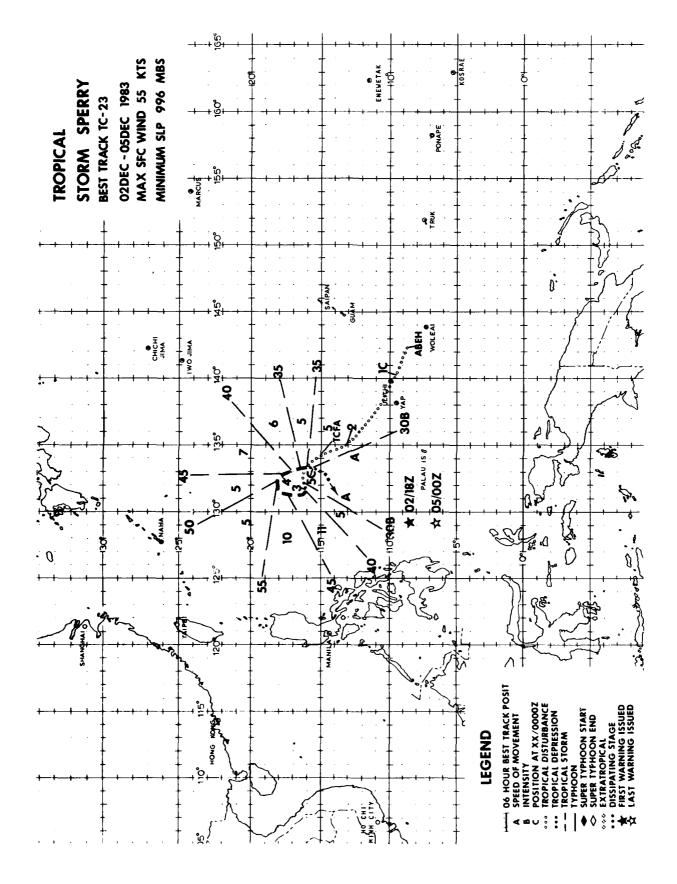
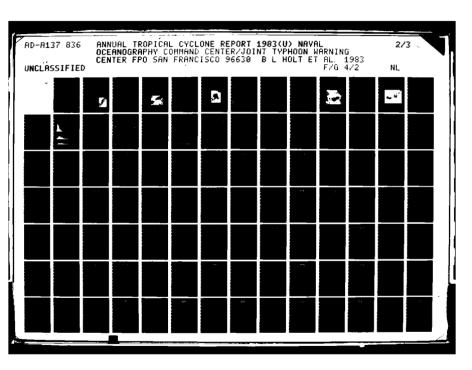
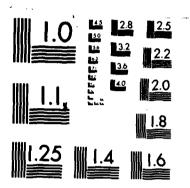


Figure 3-22-1. Tropical Storm Ruth near maximum intensity. Interaction with the frontal boundary to the north and the cold air outbreak south of Japan led to Ruth's destruction two days later (2809352 November DMSP infrared imagery).







MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

The disturbance which became the 23rd tropical cyclone of the year originated in an elongated band of unorganized convection associated with a near-equatorial trough. This cyclone, eventually called Sperry, was to be a short-lived system, lasting about two and one-half days before dissipating in a manner similar to that of two of its predecessors - Typhoon Orchid and Tropical Storm Ruth.

As the remnants of Tropical Storm Ruth faded away, the monsoon trough became active again and reestablished itself, stretching from the south Philippine Sea eastward to the Marshall Islands. The convective activity covered a broad area between 4-10N and 130-150 E. On the 30th of November, a surface circulation embedded in the trough about 400 nm (740 km) south of Guam appeared to be gaining in organization and intensity. MSLP at this time was 1009 mb and associated winds were 10 to 15 ft (5-8 m/s). Over the following 24 hours, MSLP in the circulation dropped to 1006 mb and convective activity increased significantly.

At this point, it appeared that the circulation was well organized and on its way to becoming a significant tropical cyclone with a few more days of development. However, between 0100002 and 0112002 December, the center of convective activity shifted to a point 500 nm (926 km) to the northwest. This radical shift was accompanied by the development of an upper-level anticyclone over the new location. Continued intensification of the center led to the issuance of a TCFA at 03002 on the 2nd. Shortly after the issuance of this alert, a reconnaissance aircraft investigated the area and found an elongated surface trough with pressures around 1006 mb and winds of 15-30 kt (8-15 m/s).

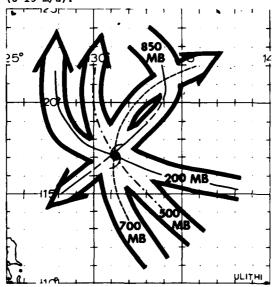


Figure 3-23-1. Diagram illustrating the direction of steering flow at various levels in the vicinity of Sperry.

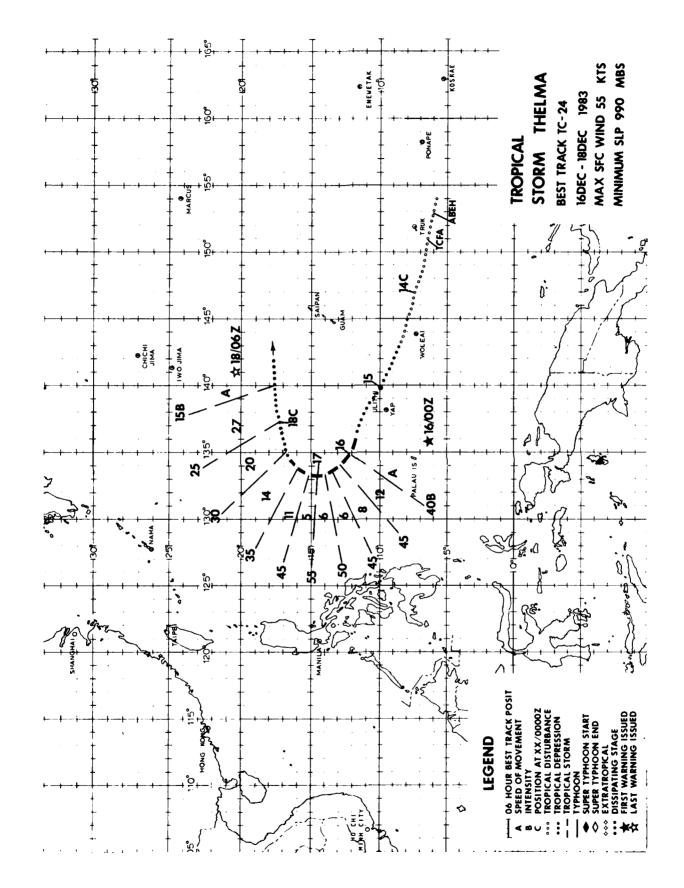
The first warning on Sperry was issued at 021800Z when analysis of satellite imagery resulted in a Dvorak T-number of 2.5 or 35 kt (18 m/s). The accuracy of this analysis was confirmed a few hours later by reconnaissance aircraft. Data collected by reconnaissance aircraft indicated that Sperry exhibited considerable tilt. The surface center was displaced 30-60 nm (56-111 km) to the south of the 700 mb center. This was not unexpected since the circulation was located in an area of strong vertical Figure 3-23-1 illustrates the shear. steering influences acting on Sperry at the Tilting of the system prior to shearing away of the upper portion of the circulation is a common occurrence in this situation. Therefore, it came as a surprise when Sperry regained vertical alignment and intensified. Maximum intensity of 55 kt (28 m/s) was achieved as Sperry turned eastward at 0312002. Figure 3-23-2 shows Sperry near maximum intensity.

The forecast at this point called for Sperry to complete an anticyclonic loop and dissipate over water as an exposed low-level circulation. This forecast was a radical departure from persistence. Over the previous 18 hours, Sperry had intensified from a tropical depression to an intense tropical storm. At the same time, Sperry's speed of motion doubled as it turned northward, then northeastward. Persistence in this case called for continued northeastward movement and intensification.

Sperry sheared as expected and moved southward while weakening over the next 36 hours. The final warning was issued at 050000Z when data from reconnaissance aircraft indicated that Sperry's MSLP had risen to 1010 mb and maximum sustained winds had dropped to 20 kt (10 m/s).



Figure 3-23-2. Tropical Storm Sperry at maximum intensity while undergoing an anticyclonic loop [0313357 December DMSP infrared imagery].



TROPICAL STORM THELMA (24W)

Thelma, the final tropical cyclone of the 1983 season, formed to the east of the Caroline Islands during mid-December. It was the only late-season cyclone to recurve in the western Philippine Sea.

Thelma was initially detected on 11 December as a weak surface circulation embedded in the near-equatorial trough near 4N 170E. Upper-level flow in the area was highly divergent due to the presence of a TUTT cell to the north of the low-level trough. A broad area of convective activity existed below the divergent upper-level flow, and was not confined to the proximity of the low-level circulation.

Over the next two days, the TUTT cell moved westward into a position to the northwest of the low-level circulation. An anticyclone formed over the low-level circulation in the lee of the TUTT, prompting the issuance of a TCFA at 1312002.

Thelma remained in alert status for two and one-half days while moving rapidly westward. Repeated investigative flights by reconnaissance aircraft during this period provided data indicating that the circulation remained poorly defined. Concurrently, Thelma's appearance on satellite imagery indicated that the system was becoming better organized with well-developed outflow.

The first warning on Thelma, as a tropical storm, was issued when reconnais-

sance aircraft located a tight circulation center at 160100Z. MSLP was 996 mb and maximum surface winds observed were 40 kt (21 m/s). The forecast called for Thelma to continue moving west-northwestward for the first 24 hours, then shear and assume a westward track as an exposed low-level circulation. Three previous storms (Orchid, Ruth, and Sperry) had reacted in a like manner under similar circumstances. These storms had reacted to the passage of a mid-latitude frontal system by shearing under the pressure of enhanced but opposing flows at lower and middle-levels. As the frontal system approached to the northwest of Thelma, a repeat of these performances was expected.

Thelma's classic recurvature in advance of the front proved the fallacity of JTWC's forecast reasoning. Thelma's environment differed from its predecessors in that it was not embedded in strong northeasterly flow at the low-levels. Although the northeasterly monsoon was well established in close proximity to the Asian Continent, Thelma was beyond its influence in the central Philippine Sea.

Thelma achieved maximum intensity of 55 kt (28 m/s) just prior to recurving on the 17th. After recurvature, Thelma dissipated rapidly under the effects of intense vertical shear (Figure 3-24-1). The strength of the upper-level flow impacting Thelma is reflected in the rapidity with which the system sheared while moving northeastward at speeds up to 27 kt (50 km/hr).

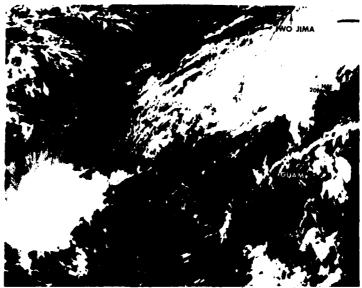
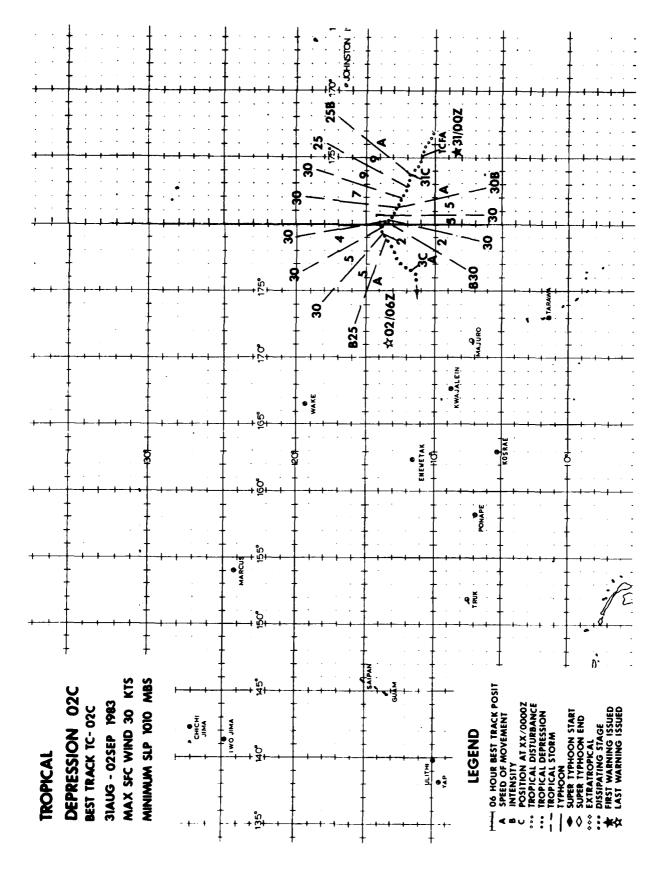


Figure 3-24-1. After recurvature, Thelma quickly dissipated and became absorbed into the frontal system. Only 24 hours after maximum intensity, the remains of Thelma were no longer distinguishable from the frontal system (upper right). The cloud feature at lower left is not associated with Thelma but is a "blow-up" frequently observed at the trailing edge of a front in the western North Pacific (1800562 December DMSP visual imagery).



TROPICAL DEPRESSION 02C

During late August, two tropical disturbances developed in the central North Pacific Ocean, east of the International Dateline, and tracked westward into the JTWC area of responsibility. The first of these disturbances crossed the dateline on 27 August and later became Typhoon Ellen (10W). As this disturbance moved westward toward Enewetak Atoll (WMO 91250), a second disturbance began to develop southwest of Johnston Island (WMO 91275). At 301530Z, the Naval Western Oceanography Center, Pearl Harbor, Hawaii, issued a TCFA for this disturbance, which was followed by the initial warning at 310600Z from the Central Pacific Hurricane Center (CPHC), Honolulu, Hawaii.

During the first 24 hours in warning status, Tropical Depression 02C moved toward the northwest and the dateline. At 312345Z August, satellite fix information from the National Environmental Satellite, Data and

Information Service (NESDIS) office in Honolulu, Hawaii, indicated that Tropical Depression 02C had reached the dateline (see Figure 3-25-1). Based on this information, the CPHC issued their final warning for 010000Z September position and transferred warning responsibility to the JTWC.

After 0100002, satellite fix positions began to oscillate east and west of the dateline. It seems likely that Tropical Depression 02C may have slowed, or moved erratically, near the dateline before resuming a westward track on 2 September. During this period, a break in the subtropical ridge was present northwest of Tropical Depression 02C. Tropical Depression 02C was forecast to respond to this break by moving slowly northwestward. However, that response was never realized, and once the subtropical ridge strengthened, Tropical Depression 02C moved west-southwestward and eventually dissipated over open water.



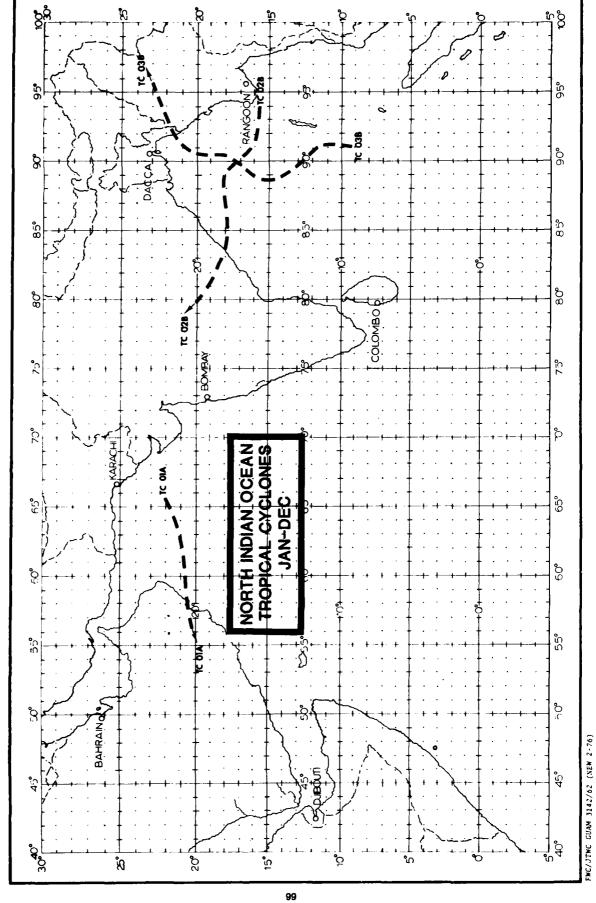
Figure 3-25-1. Tropical Depression 02C at its peak intensity. This imagery provided information to both the CPHC and JTWC that Tropical Depression 02C had reached the dateline. However, it was 24 hours later that satellite fix data indicated a significant movement westward from the dateline (312345Z August COES-West visual imagery, courtesy of the National Environmental Satellite, Data and Information Service, Honolulu, Hawaii).

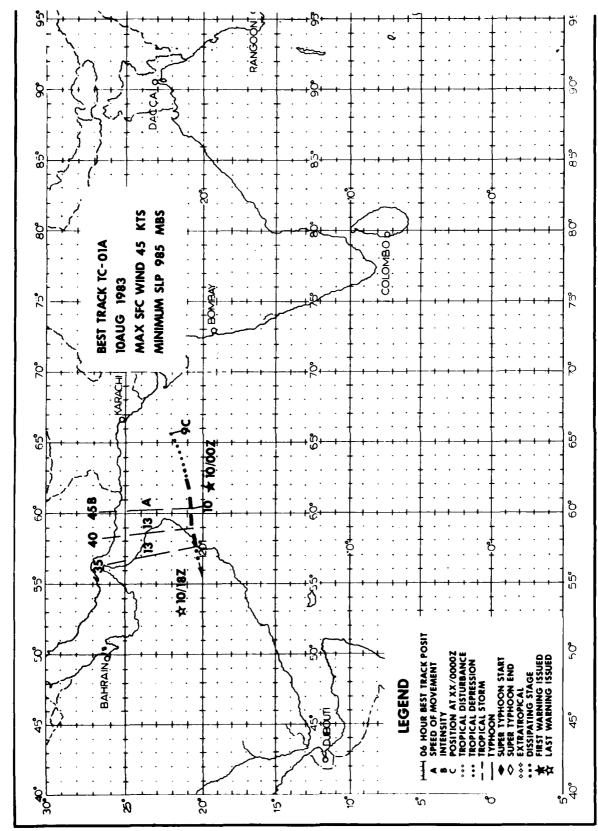
2. NORTH INDIAN OCEAN TROPICAL CYCLONES

Tropical cyclone activity in the North Indian Ocean was below normal during 1983. Only three storms originated in this area as compared to the annual average of 4.6. A fourth system, Tropical Storm Kim, moved into

the area from the western North Pacific. (See Tropical Storm Kim (16W)). Tables 3-6 and 3-7 provide a summary of North Indian Ocean tropical cyclone activity.

TABLE 3-6. NORTH INDIAN OCEAN						
1983 SIGNIFICANT TROPICAL CYCLONES						
TROPICAL CYCLONE PE	RIOD OF WARNIN	CALENDAR DAYS OF G WARNING	NUMBER OF WARNINGS ISSUED	MAXIMUM SURFACE WIND (KT)	ESTIMATED MSLP (MB)	BEST TRACK DISTANCE TRAVELED (NM)
1. TC 01A	10 AUGUST	1	3	45	985	461
	OCT - 4 OCT	2	5	50	990	370
	NOV - 9 NOV	3	10	55	980	900
	1983 TOTALS:	6	18			
TABLE 3-7. 1983 SIGNIFICANT TROPICAL CYCLONES						
NORTH INDIAN OCEAN JAN	FEB MAR AP	R MAY JUN	JUL AUG	SEP OCT NO	V DEC TOTA	. <u>L</u>
ALL TROPICAL			- 1	- 1 1	3	
1975-1982						
AVERAGE .1	1				4 .4 4.6	
CASES 1	1	6 4		3 8 11	. 3 37	
FORMATION ALERTS: Two out of three systems on which Formation Alerts were issued developed into significant tropical cyclones.						
WARNINGS:	Number of wa	rning days:		6		_
	Number of warnings days with two tropical cyclones in region:					
Number of warning days with three or more tropical cyclones in region: 0						





FNC/JTWC GUAM 3142/62 (NEW 2-76)

TROPICAL CYCLONE 01A (AURORA)

Aurora was first detected on 8 August using satellite imagery. It appeared as a loosely organized area of convective activity in the northern Arabian Sea. Synoptic data was sparse in the area and was not useful for intensity estimation. Dvorak intensity estimates indicated that maximum sustained surface winds in the area were approximately 25 kt (13 m/s). This convective area was monitored by satellite for the next 24 hours and continued to appear loosely organized as it moved westward across the Arabian Sea.

On the 9th of August, the system became better organized and appeared to have formed a coherent surface circulation (Figure 3-26-1). Dvorak intensity estimates continued to reflect tropical depression

strength and synoptic data at the time gave no indication of the presence of a surface circulation in the area.

The initial warning was issued at 100000Z after shipboard surface observations indicated the presence of 40 kt (21 m/s) northeasterly winds near Aurora. At the time, Aurora was approximately 90 nm (167 km) east of the coast of Oman with evidence of a strong 35 to 45 kt (18 to 23 m/s) southwesterly monsoon gale area extending to near its latitude. Aurora moved rapidly onshore during the subsequent 12-hour period and dissipated. The final warning was issued at 101800Z, just 18 hours after attaining warning status and less than 42 hours after its initial detection.

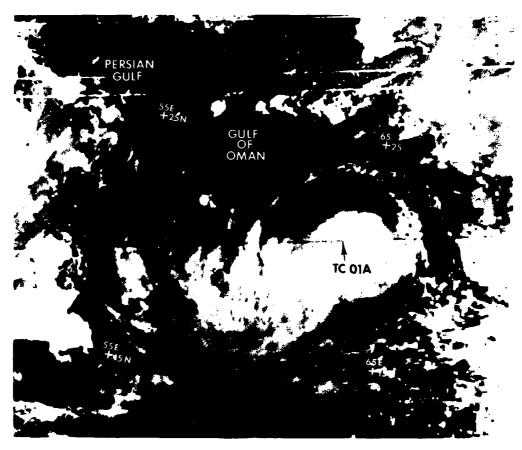
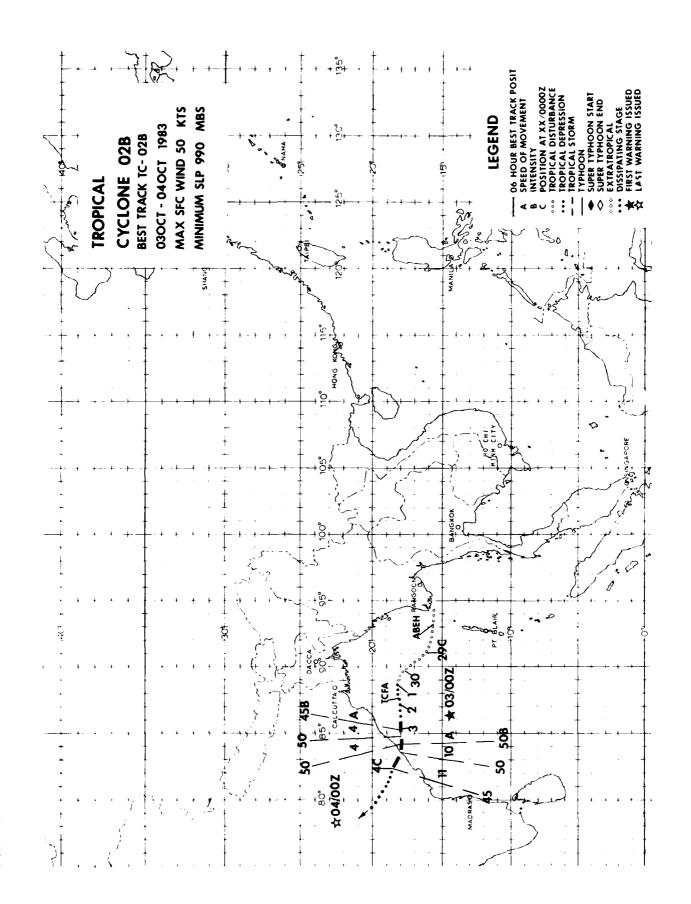


Figure 3-26-1. Tropical Cyclone 01A (Aurora) (0910572 NOAA 1 visual imagery).



TROPICAL CYCLONE 02B

Tropical Cyclone 02B was first detected on 28 September as an area of weakly organized convection located near the southern tip of Burma. Strong upper-level easterly flow over the system inhibitted the formation of outflow channels to the northeast; therefore it moved slowly west-northwestward over the next four days without increasing in organization or intensity. The system eventually moved away from its unfavorable environment and became a significant tropical cyclone.

As Tropical Cyclone 02B continued moving west-northwestward across the Bay of Bengal, its upper-level environment became more favorable for development of the system. Outflow channels became established when the upper-level easterly flow abated over the circulation. A TCFA was issued at 1029Z on

the 1st of October in view of the increased potential for further development. This alert was reissued on the 2nd after 24 hours with no further development. The first warning was finally issued at 030000Z. The initial warning on Tropical Cyclone 02B was prompted by satellite imagery which indicated that the system had intensified significantly over the past 24 hours with estimated winds of 45 kt (23 m/s).

The forecast called for continued west-northwestward movement and slight intensification prior to landfal on the eastern coast of India. Tropical Cyclone 02B behaved as expected, making 20 nm (37 km) northeast of Visconda at 1700Z on the 3rd of (ber. After making landfall, Tropical Cyclone 32B moved inland over India and dissipa

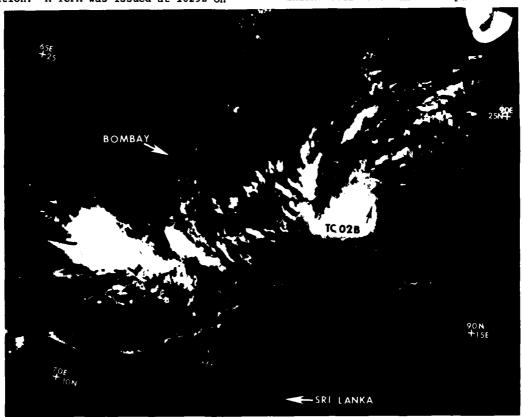
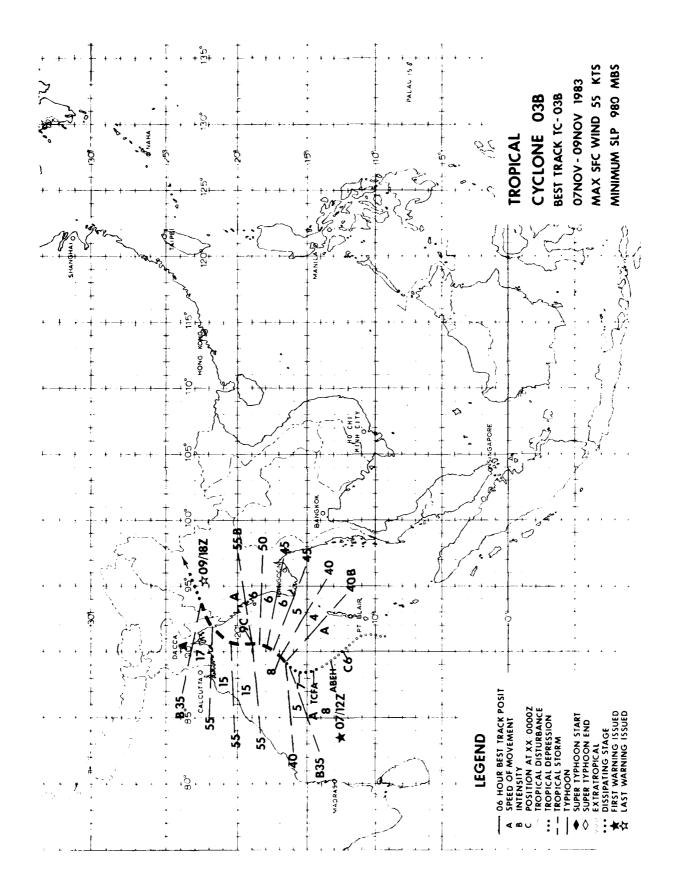


Figure 3-27-1. Tropical Cyclone 02B near maximum intensity seven hours prior to landfall (030948Z October NOAA 7 visual imagery).



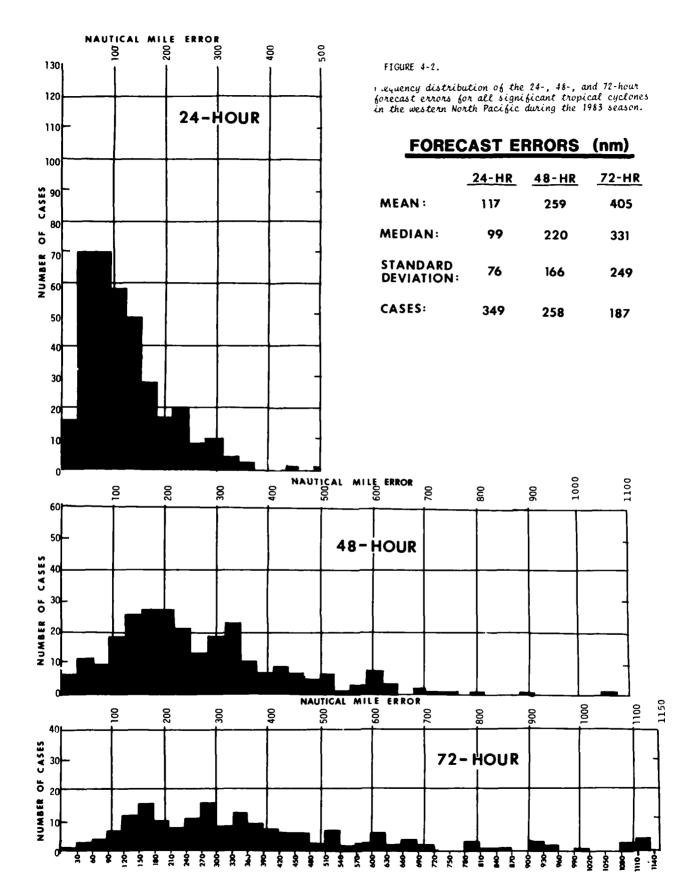
TROPICAL CYCLONE 03B

Tropical Cyclone 03B emerged from the monsoon trough during early November and had a relatively brief and uneventful life. A poorly organized surface circulation in the southern Bay of Bengal had persisted for several days in the monsoon trough. A weak upper-level anticyclone centered over the northern postion of the Bay, placed the low-level circulation in an environment of nondivergent upper-level flow which inhib~ited further development.

The surface circulation remained poorly organized while moving slowly northward until the 5th of November. At this time, it came into superposition with the upper-level anticyclone which had shifted southward. Over the next 24 hours, satellite imagery indicated the development of convective banding features which prompted the issuance of a TCFA at 16002 on the 6th.

The circulation continued to intensify while moving north-northwestward. The first warning on Tropical Cyclone 03B was issued at 1444Z on the 7th when satellite intensity estimates reached 35 kt (18 m/s). The lack of synoptic data in the area prompted JTWC to rely on intensity estimates from satellite imagery throughout the life of the cyclone.

After passing the axis of the subtropical ridge, Tropical Cyclone 03B assumed a north-northeastward track and continued to intensify. Maximum intensity of 55 kt (28 m/s) was reached at 0000Z on the 9th. This intensity was maintained until landfall, 12 hours later, on the coast of Bangladesh between Chittagong (WMO 41941) and Cox's Bazar (WMO 41950). Tropical Cyclone 03B continued moving northeastward after landfall and dissipated over northern Burma.



CHAPTER IV - SUMMARY OF FORECAST VERIFICATION

1. ANNUAL FORECAST VERIFICATION

a. Western North Pacific Ocean

The positions given for warning times and those at the 24-, 48-, and 72-hour fore-cast times were verified against the post-analysis "best-track" positions at the same valid times. The resultant vector and right angle (track) errors (illustrated in Figure 4-1) were then calculated for each tropical cyclone and are presented in Table 4-1. Figure 4-2 provides the frequency distributions of vector errors for 24-, 48- and 72-hour forecasts of all 1983 tropical cyclones in the western North Pacific. A summation of the mean errors, as calculated

for all tropical cyclones in each year, is shown in Table 4-2 for comparative purposes. The data used in this table are not to be confused with that presented in earlier years where the sample was restricted to tropical cyclones that reached typhoon intensity and then had the forecast errors calculated only for that portion of the life-cycle when the intensity was greater than 34 knots (last published as Table 5-1, 1977 Annual Typhoon Report). A comparison of the results using the truncated data set and those obtained for all tropical cyclones can be seen directly in Table 4-3. The annual mean vector errors are graphed in Figure 4-3.

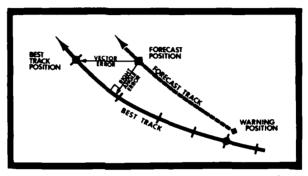


FIGURE 4-1. Illustration of the method to determine vector error and right angle error.

					RY FOR THE CYCLONES (
		WARNING			24-HOUR			48-HOUR			72-HOUR	
	VECTOR ERROR	RT ANGLE ERROR	NR OF WRNGS	VECTOR ERROR	RT ANGLE ERROR	NR OF WRNGS	VECTOR	RT ANGLE ERROR	NR OF	VECTOR	RT ANGLE ERROR	NR OF
lw. TS SARAH	27	18	6	94	86	3						
2C. TD 02C	36	17	5	168	117	4	276	205	1			
2W. TY TEP	12	8	14	66	53	10	165	160	6	215	204	2
3W. TY VERA	14	9	25	72	39	21	131	66	17	187	70	13
4W. STY WAYNE	12	10	14	96	63	11	226	92	7	4 54	102	3
SW. STY ABRY	11	8	51	104	84	47	224	199	43	340	307	39
6W. TS CARMEN	20	12	8	199	105	4						
7W. TS BEN	17	12	12	123	41	8	212	46	4			
8W. TS DOM	18	11	23	134	92	19	317	213	13	395	198	1
9W. TD 09W	21	11	4									
IOW. TY ELLEN	15	11	47	101	60	43	223	123	39	339	178	35
IN. STY FORREST	п	8	32	97	64	28	224	79	24	366	118	20
IZW. TS GEORGIA	10	7	11	53	27	7	52	18	3			
I 3₩. TS HERBERT	18	11	8	33	24	5	43	29	1			
14W. TY IDA	10	6	15	144	58	11	298	95	7	516	25	3
SW. TY JOE	15	10	15	86	61	12	177	151	8	246	200	4
IGW. TS KIM	23	11	3	292	55	ı						
17W. TY LEX	18	11	18	116	69	14	259	156	10	316	137	5
ISW. STY MARGE	19	14	27	191	134	23	484	240	19	755	282	15
19W. TS NORRIS	19	15	7	85	53	3						
OW. TY ORCHID	16	10	38	117	54	33	267	160	30	459	34 3	26
IW. TY PERCY	21	11	23	173	86	19	409	184	15	650	361	11
2W. TS RUTH	15	8	16	94	56	11	246	162	7	394	353	4
3W. TS SPERRY	33	19	10	149	91	6	343	237	2			
24W. TS THELMA	32	16	10	268	151	6	5 12	2 3 9	2			

ANNUAL MEAN FORECAST ERRORS (NM) FOR THE WESTERN PACIFIC TABLE 4-2. 24-HOUR 48-HOUR 72-HOUR VECTOR RIGHT ANGLE VECTOR RIGHT_ANGLE RIGHT ANGLE YEAR VECTOR 1981* 1982* 1983*

TABLE 4-3. ANNUAL MEAN FORECAST ERRORS (NM) FOR WESTERN NORTH PACIFIC

	2	4-HOUR	4	8-HOUR	7:	2-HOUR
YEAR	ALL	TYPHOON*	ALL	TYPHOON*	ALL	TYPHOON*
1950-58		170				
1959		117**		267**		
1960		177**		354**		
1961		136		274		
1962		1.44		287		476
1963		127		246		374
1964		133		284		429
1965		151		303		418
1966		136		280		432
1967		125		276		414
1968		105		229		337
1969		111		237		349
1970	104	98	190	181	279	272
1971	111	99	212	203	317	308
1972	117	116	245	245	381	382
1973	108	102	197	193	253	245
1974	120	114	226	218	348	351
1975	138	129	288	279	450	442
1976	117	117	230	232	338	336
1977	148	140	283	266	407	390
1978	127	120	271	241	410	459
1979	124	113	226	219	316	319
1980	126	116	243	221	389	362
1981	123	117	220	215	334	342
1982	113	114	237	229	341	337
1983	117	110	259	247	405	384

^{*} For Typhoons only while winds were over 35 kt (18 m/sec).

^{*} The technique for calculating right angle error was revised in 1981; therefore, a direct correlation in right angle statistics cannot be made for the errors computed before 1981 and the errors computed since 1981.

^{*} Forecast positions north of 35°N were not verified.

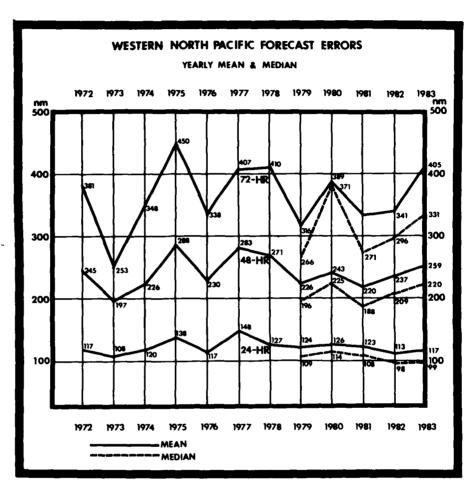


FIGURE 4-3. Annual mean and median vector errors (nm) for all tropical cyclones in the western North Pacific.

b. North Indian Ocean

The positions given for warning times and those at the 24-, 48- and 72-hour valid times were verified for tropical cyclones in the North Indian Ocean by the same methods used for the western North Pacific. It should be noted that due to the low number of North Indian Ocean tropical cyclones,

these error statistics should not be taken as representative of any trend. Table 4-4 is the forecast error summary for the North Indian Ocean and Table 4-5 contains the annual average of forecast errors back through 1971. Vector errors are plotted in Figure 4-4. (Seventy-two hour forecast errors were evaluated for the first time in 1979).

TABI	E 4-4.				_											
						MARY FOR T		INDIAN O								
		WARNING 24-HOUR 48-HOUR 72-HOUR POSIT RT ANGLE NR OF POSIT RT ANGLE NR OF POSIT RT ANGLE NR OF														
		POSIT ERROR		NR OF WRNGS	POSIT		NR OF WRNGS	POSIT		NR OF WRNGS	POSIT ERROR		NR OF WRNGS			
1.	TC OLA	48	35	3	-	-	-	-	-							
2.	TC 02B	23	25	5	162	114	1	-	-	-	-	-	-			
3.	TC 03B	42	21	10	109	35	6	153	67	2	-	-	-			
ALL	FORECASTS:	38	24	18	117	46	7	153	67	2						

TABLE 4-5.

ANNUAL MEAN FORECAST ERRORS FOR THE NORTH INDIAN OCEAN

	24	-HOUR	48	-HOUR	72	-HOUR
YEAR	VECTOR	RIGHT ANGLE	VECTOR	RIGHT ANGLE	VECTOR	RIGHT ANGLE
1971*	232	-	410	-	-	-
1972*	224	101	292	112	-	-
1973*	182	99	299	160	-	-
1974*	137	81	238	146	-	-
1975	145	99	228	144	-	-
1976	138	108	204	159	-	-
1977	122	94	292	214	-	-
1978	133	86	202	128	-	-
1979	151	99	270	202	437	371
1980	115	73	93	87	167	126
1981**	109	65	176	103	197	73
1982**	138	66	368	175	762	404
1983**	117	46	153	67	-	-

The western Bay of Bengal and the Arabian Sea were not included in the JTWC area of responsibility until the 1975 tropical cyclone season.

^{**} The technique for calculating right angle error was revised in 1981; therefore, a direct correlation in right angle statistics cannot be made for the errors computed before 1981 and the errors computed since 1981.

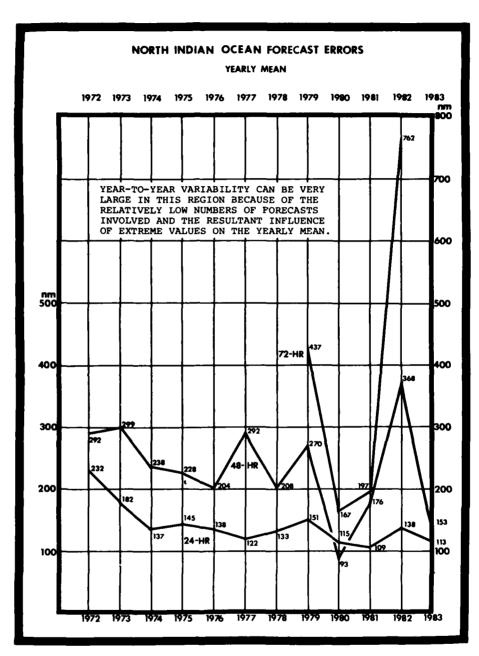


FIGURE 4-4. Annual mean vector errors (nm) for all tropical cyclones in the North Indian Ocean.

2. COMPARISION OF OBJECTIVE TECHNIQUES

a. General

Objective techniques used by JTWC are divided into five main categories:

- climatological and analog techniques;
- (2) extrapolation;
- (3) steering techniques;
- (4) dynamic models;
- (5) empirical and analytical techniques

In September 1981, JTWC began to initialize its array of objective forecast techniques (described below) on the six-hour-old preliminary best track position (an interpolative process) rather than the forecast (partially extrapolated) warning position, e.g. the 0600Z warning is now supported by objective techniques developed from the 0000Z preliminary best track position. This operational change has yielded several advantages:

*techniques can now be requested much earlier in the warning development time line, i.e. as soon as the track can be approximated by one or more fix positions on, or after the valid time of the previous warning;

*receipt of these techniques is virtually assured prior to

development of the next warning
*improved (mean) forecast accuracy.
This latter aspect arises because JTWC now
has a more reliable approximation of the
short-term tropical cyclone movement.
Further, since most of the objective
techniques are biased for persistence, this
new procedure optimizes their performance
and provides more consistent guidance on
short-term movement, indirectly yielding a
more accurate initial position estimate as
well as lowering 24-hour forecast errors.

- b. Description of Objective Techniques
- (1) CLIM -- A climatological aid providing 24-, 48- and 72-hour tropical cyclone forecast positions (and intensity changes in the western North Pacific) based upon the position of the tropical cyclone. The output is based upon data records from 1945 to 1981 for the western North Pacific Ocean and 1900 to 1981 for the North Indian Ocean.
- (2) TYAN78 -- An updated analog program which combines the earlier versions TYFN 75 and INJAH 74. The program scans history tapes for tropical cyclones similar (within a specified acceptance envelope) to the current tropical cyclone. For the western North Pacific Ocean, three forecasts of position and intensity are provided for 24-, 48- and 72-hours: RECR a weighted

mean of all accepted tropical cyclones which were categorized as "recurving" during their best track period; STRA - a weighted mean of all accepted tropical cyclones which were categorized as moving "straight" (westward) during their best track period; and TOTL - a weighted mean of all accepted tropical cyclones, including those used in the RECR and STRA forecasts. For the North Indian Ocean, a single (total) forecast track is provided for 12-hour intervals to 72 hours.

- (3) BPAC -- A program which generates 12- to 72-hour forecast positions based on blending the past motion of the tropical cyclone with the CLIM forecast positions. The blending routine gives less weight to persistence at each succeeding forecast interval.
- (4) XTRP -- Forecast positions for 24- and 48-hours are derived from the extension of a straight line which connects the most-recent and 12-hour-old preliminary best track positions.
- (5) HPAC -- 24- and 48-hour forecast positions are derived by merely connecting the mid-points of straight lines which connect these positions on the XTRP and CLIM tracks, respectively.
- (6) CYCLOPS -- An updated version of the HATTRACK/MOHATT steering program which can provide geostrophic steering forecasts at the 1000-, 850-, 700-, 500-, 400-, and 200-mb levels. The program can be run in a modified (includes a 12-hour persistence bias) or unmodified mode applied to either analysis or prognostic fields. The program advects a point vortex on a preselected analysis and/or smoothed prognostic field at designated levels in six-hour time steps through 72 hours. In 1983, only the modified version, in the prognostic mode for the 500-mb level was verified; however, JTWC routinely uses many of the other levels and modes as operational forecast aids.
- OTCM -- (One-way Tropical (7) Cyclone Model) A coarse-mesh, three-layer in the vertical, primitive equation model with a 205 km grid spacing over a 6400 x 4700 km domain. The model's fields are computed around a bogused, digitized cyclone vortex using FLENUMOCEANCEN Global Bands prognostic fields for the specified valid time. The past motion of the tropical cyclone is compared to initial steering fields and a bias correction is computed and applied to the model. FLENUMOCEANCEN hemispheric prognostic fields are used at 12-hour intervals to update the model's boundaries. The resultant forecast positions are derived by locating the 850 mb vortex at six-hour intervals to 72 hours. In 1983, the OTCM was requested for each warning; and when computer resources were available, the OTCM forecast was normally available to the TDO within one hour of the request hour of the request.

- (8) NTCM -- (Nested Tropical Cyclone Model) A primitive equation model with similar properties as the OTCM. The NTCM differs by containing a finer scale "nested" grid, initializing on Global Bands analysis fields, not containing a (persistence) bias correction, and being a channel model which runs independent of FLENUMOCEANCEN prognostic fields (not requiring updating of its boundaries). The "nested" grid covers a 1200 x 1200 km area with a 41 km grid spacing which moves within the coarse-mesh domain to keep an 850 mb vortex at its center.
- (9) TAPT -- A technique which utilizes upper-tropospheric wind fields to estimate the latitude of initial acceleration associated with the tropical cyclone's interaction with the mid-latitude westerly steering currents. Further, the technique provides speed of movement guidelines for duration and upper-limits, and insight on the probable path of the tropical cyclone, given a prevailing upper-wind pattern during the acceleration process.
- (10) THETA E -- An empirically derived relationship between a tropical cyclone's minimum sea level pressure (MSLP) and (700 mb) equivalent potential temperature ($\theta_{\rm e}$) was developed by Sikora (1976) and Dunnavan (1981). By monitoring MSLP and $\theta_{\rm e}$ trends, the forecaster can evaluate the potential for sudden, rapid deepening of a tropical cyclone.
- (11) WIND RADIUS -- Following an analytic model of the radial profiles of sea level pressures and winds in mature

- tropical cyclones (Holland, 1980), a set of radii for 30-, 50-, and 100-knot winds based on the tropical cyclone's maximum intensity and radius of maximum winds have been produced to aid the forecaster in determining forecast wind radii.
- (12) DVORAK -- An estimation of a tropical cyclone's current and 24-hour forecast intensity is made from interpretation of visual satellite imagery (Dvorak, 1973) and provided to the forecaster. These intensity estimates are used in conjunction with other intensity-related data and trends to forecast tropical cyclone intensity.

c. Testing and Results

A comparison of selected techniques is included in Table 4-6 for all western North Pacific tropical cyclones and in Table 4-7 for all North Indian Ocean tropical cyclones. In these tables, "X-AXIS" refers to techniques listed vertically. The example in Table 4-6 compares CY50 to OTCM, i.e. in the 273 cases available for a (homogeneous) comparison, the average vector error at 24 hours was 114 nm for CY50 and 105 for OTCM. The difference of 8 nm is shown in the lower right. (Differences are not always exact, due to computational round-off which occurs for each of the cases available for comparison).

TABLE 4-6. 1983 ERROR STATISTICS FOR SELECTED OBJECTIVE TECHNIQUES IN THE WESTERN NORTH PACIFIC OCEAN

	24- JTWC RECR ST								24-HC	UR FO	RECAST	ERRO	RS (N	1)								
			R	CR	S1	'RA	TO	TL		50	N1	CM	01	CM	В	PAC	CI	LIM_	XT	RP	HI	AC
JTWC	349 117	117 0																				
RECR	310 126	113 13	310 126	126 0								Γ	NUMBER OF	l	TE	X-AXI CHNIQ						
STRA	317 133	114 18	299 127	121 6	317 133	133 0						<u> </u>	CASES		 	ERROR						
TOTL	328 120	117 4	309 113	126 -11	316 117	133 -15	328 120	120 0				TE	Y-AXIS CHNIQU			ERROR FFERE	NCL					
CY 50	321 114	117 -1	293 111	126 -14	296 111	132 -20	307 113	119 -5	321 114	114 0		_	ERROR			Y - X						
NTCM	274 161	119 42	239 157	122 35	248 154	137 17	257 161	122 39	251 164	109 54	274 161	161 0										
OTCM	288 104	118 -13	258 101	124 +23	260 100	131 -30	271 104	119 -13	273 105	114 -8	232 101	162 -59	289 107	107 0								
BPAC	323 128	117 11	292 124	126 -1	298 122	133 -10	309 126	121 6	301 128	114 14	255 127	161 -33	273 127	103 24	323 128	128 0						
CLIM	341 148	116 32	307 141	126 15	314 144	133 11	325 150	121 29	315 150	114 36	268 152	160 -7	282 147	103 44	323 148	128 20	341 148	148 0				
XTRP	341 112	117 -4	305 111	126 -14	311 108	134 -24	322 111	121 -9	316 112	115 -1	268 109	161 -50	282 113	104 9	321 113	128 -14	337 112	149 -36	341 112	112 0		
HPAC	337 111	117 -4	305 106	126 -18	311 107	134 -25	322 111	121 -8	313 112	114 -1	264 113	160 -46	280 111	103 8	321 111	128 -16	337 111	149 -36	337 111	112	337 111	111
									48-HC	UR FO	RECAS1	ERRO	RS (N	1)								
48-	JT		RE	CR	ST	RA	то	TL	СХ	50	NT	CM	or	CM	ВР	AC	CL	IM_	хт	RP	НР	AC
JTWC	258 259	259		224										1					FORECA	ST		1
RECR	233 235 238	252 -17 259	235 236 228	236 0 230	24.0	204									STRA	- RECT - STRA	AIGHT	(TYAN	78)			
STRA	282	23	274	44	240 284	284	248	252							CY50 NTCM	- CYC	LOPS N	10D I F I ROP I CA	FD 500 L CYCL	ONE M	DOEL	Ì
TOTL	246 252	261 -9	235 236	236	240 250	284 -34	248 253	253							BPAC		NDED F	PERSIS	AL CYC			l
CY 50	237 318	260 59	223 321	239 83	224 321	283 38	232 322	248 74	239 319	319 0	-00				XTRP	- 12-	HOUR, E	EXTRAP	OLATIO ND CLI			
NTCH	200 251	270 -19	179 240	232 7	185 240	292 -50	192 250	258 -7	185 252	326 -73	202 250	250									_	•
OTCH	209 200	262 -60	192 193	234 -40	193 192	276 -83	200 201	245 -44	199 204		166 201	246 -44	211 202	202 0								
BPAC	241 241	261 -19	221 230	236 -5	225 233	286 -52	233 237	251 -13	225 241	326 -83	191 240	248 -7	200 237	200 37	243 241	24 I 0						
CLIM	254 261	261 0	232 249	235 13	237 255	286 -30	245 262	254 9	23 0 263	320 -57	200 274	249 25	207 254	201 53	243 258	241 17	256 262	262 0				
XTRP	252 239	260 -21	230 234	235 0	234 237	286 -47	242 · 238	253 -14	234 242	316 -73	198 232	249 -17	205 240	201 39	241 242	242 0	253 240	261 -20	254 239	23 9 0		
HPAC	251 210	261 -50	230 200	235 -34	234 205	286 79	242 210	253 -42	234 212	316 -102	197 215	250 -33	205 208	201 7	241 210	242 -31	253 211	261 -49	253 211	240 -28	253 211	211 0
									72-H0	UR FOR	ECAST	ERRO	RS (NM	1)								
	JTW 187		KÆ C	R	STR	<u> </u>	TOT	ı.	CY5	0	NTC	<u> </u>	OTC	M	BPA	.c	CLI	M				
	405	0																				
RECR	171 359	388 -28	359	359 0																		
STRA	173 410	393 17	169 404	350 54	177 418	0																
TOTL	180 389	402 -13	176 366	359 7		418 -31	185 389	389 0														
CY 50	171 526	393 132	167 533	364 169		402 117	172 530	368 161	522	522 0												
MICH	149 335	412 -77	137 325	348 -22	139 316		146 338	404 -66	139 336	540 -203	152 336	336 0										
OTCM	145 344	407 -62	139 336	355 -18		412 -90	144 343	381 -37	142 349		123 346	337 9	150 347	347 0								
BPAC	171 354	405 -50	163 334	361 -26		417 -79	171 349	382 -32	163 350		142 359	332 28	140 349	346 3	176 359	359 0						
CLIM		405 -64		357 -37		418 -85	182 337	388 50	173 333		150 356	333 23	146 319	346 -25	175 334	357 -22	188 341	341 0	_			

TABLE 4-7. 1983 ERROR STATISTICS FOR SELECTED OBJTECTIVE TECHNIQUES IN THE NORTH INDIAN OCEAN 24-HOUR FORECAST ERRORS (NM)

24-	JŢ	wc	TO	TL	NTC	1	CY 50	CY	85	01	'CM	BP#	AC .	CL	[M	хт	'RP_	нР	AC
JTWC	10 113	113 0																	
TOTL	9 109	114 -4	9 10 9	109 0						F	Min	MBER	Τ.	X-AXI					
NTCM	0	0 0	0	0	0 0	0				İ	(DF SES	1	ECHNIQI ERROR					
CY 50	8 273	102 171	8 27 3	101 172	0 0	0	8 273 273 0					AXIS NIQUE	ח	ERROR	CE.				
CY85	8 157	102 55	8 157	101 56	0	0	8 273 157 -115	8 157	157			ROR		Y - X					
OTCM	6 165	130 35	6 165	118 47	0 0	0 0	5 266 147 -119	5 147	174 -26	6 165	165 0								
BPAC	9 97	114 -16	9 97	109 -11	0	0 0	8 273 95 -177	8 95	157 -61	6 112	165 -52	9 97	97 0						
CLIM	10 95	113 -18	9 97	109 -11	0	0	8 273 90 -182	8 90	157 -66	6 92	165 -72	9 97	97 0	10 95	95 0				
XTRP	10 135	113 21	9 130	109 20	0 0	0	8 273 120 -152	8 120	157 -37	6 142	165 -23	9 130	97 33	10 135	95 40	10 135	135 0		
HPAC	10 103	113 -9	9 105	109 -3	0	0 0	8 273 96 -176	8 96	157 -60	6 112	165 -52	9 105	97 9	10 103	95 9	10 103	135 -31	10 103	103 0
							4	48-нои	R FOR	ECAST	ERRORS	S (NM)							
48-	JT	WC	TO	TL	NTC	1	CY50	CY	85	TO	CM	BPA	AC	CL	[M	XT	RP	HP	AC
JTWC	2 153	153 0										777	,c	OFFICIA	T 177	IC FOR	ECAST.		_
TOTL	2 84	153 -68	2 84	84 0								TOT NTC	TL - OM -	ANALOG NESTED	TROP:	N 78) ICAL C	YCLONI		L
NTCM	0	0 0	0 0	0 0	0 0	0 0						CY 5	50 ÷	CYCLOPS CYCLOPS ONE-WAY	MOD:	[FIED	500 M	B PROG	EL.
CY50	2 505	153 353	2 505	84 421	0 0	0 0	2 505 505 0					BPA CLI	AC -	BLENDEI CLIMATO	PERS DLOGY	SISTEN	CE AN		
CY85	2 435	153 282	2 435	84 351	0 0	0	2 505 435 - 70	2 435	435 0					12-HOUE MEAN OF					╛
OTCM	2 304	153 152	2 304	84 220	0 0	0	2 505 304 -200	2 304	435 -129	2 304	304 0								
BPAC	2 113	153 -39	2 113	84 29	0 0	0	2 505 113 -391	2 113	435 -321	2 113	304 -191	2 113	113						
CLIM	2 273	153 120	2 273	84 189	0 0	0	2 505 273 -231	2 273	435 -161	2 273	304 -30		113 160	2 273	273 0				
XTRP	2 145	153 -7	2 145	84 61	0 0	0	2 505 145 -360	2 145	435 -289	2 145	304 -159	2 145	113 32	2 145	273 -127	2 145	145		
HPAC	2 205	153 52	2 205	84 120	0	0	2 505 205 - 300	2 205	435 -229	2 205	304 -99	2 205	113 92	2 205	273 -67	2 205	145 60	2 205	205 0

CHAPTER V - APPLIED TROPICAL CYCLONE RESEARCH SUMMARY

1 NAVENVPREDRSCHFAC RESEARCH

TROPICAL CYCLONE HAVEN STUDIES

(Brand, S., NAVENVPREDRSCHFAC)

Tropical cyclone haven studies are being developed for 22 ports and harbors in the Atlantic and Gulf of Mexico, and being published in the Hurricane Havens Handbook for the North Atlantic Ocean (NAVENVPREDRSCHFAC Technical Report 82-03) as available. In addition, Pearl Harbor is presently being evaluated as a hurricane haven.

THE NAVY TWO-WAY INTERACTIVE NESTED TROPICAL CYCLONE MODEL (NTCM)

(Fiorino, M., NAVENVPREDRSCHFAC)

1983 was the first year the CY205 version of the NTCM went into operational evaluation (OPEVAL). Results in WESTPAC were significantly better than for the 1982 OPEVAL version that was run on the CY175. We have further demonstrated that the NTCM, and other dynamic models, are capable of producing better forecasts than climatology-persistence aids, particularily for the long range (48-72 hours) and the general track. However, the model's performance on very large storms, like supertyphoon Abby, has forced us to consider expanding the fine mesh so that the tropical cyclone circulation is always contained within the high-resolution grid.

We will experiment with the biascorrector technique that forces initial model storm motion to be the same as that observed. We anticipate significant improvements in short term (12-24 hours) skill as well as for the longer term. We will also test timedependent boundary conditions, after the bias corrector has been implemented. Monitoring of the performance of the CY205 NTCM in the southern hemisphere will continue.

TROPICAL CYCLONE OPTIMUM FORECAST AID

(Tsui, T., NAVENVPREDRSCHFAC)

A comprehensive review of the performance of all JTWC objective tropical cyclone forecast aids shows that during 1979-82 the "one-way tropical cyclone" model (OTCM) has the best overall performance. The "nested tropical cyclone" model (NTCM) has the

superior track prediction ability, while the OTCM has the best speed of tropical cyclone movement forecast. The blend of climatology (CLIM) and persistence (XTRP) is still a good objective aid.

Through experiments, two alternate objective aids are suggested. One; JTWC forecasters are recommended to use NTCM as a track forecaster and to use one statistical aid's output as the guide of the speed forecast. This statistical aid's forecast track should be closest to the NTCM track. Two; the blending of the CLIM and the XTRP is recommended to be 1:3, 2:2, 3:1 for the 24-, 48-, and 72-hr forecast respectively.

TROPICAL CYCLONE OBJECTIVE FORECAST CONFIDENCE AND DISPLAY SYSTEM

(Nuttall, K., System and Applied Sciences Corp., Tsui, T., NAVENVPREDRSCHFAC)

The system has been installed on FNOC operational computers at the end of 1983. Forecasters at JTWC now can issue one single ARQ command to activate up to 12 objective tropical cyclone forecast aids. The results of the activated objective aids will return to the system for coordination for dissemination of the forecast guidance and the display graphics; and for archival of all objective aid forecasts. The system is also capable of processing JTWC's official forecasts and best track information; and can be applied to western North Pacific, Indian Ocean, and Southern Hemisphere regions.

A weighted combined tropical cyclone forecast composed from all available objective aids is issued upon each combined ARQ request. The weights of the combination are reduced from the past (1979-82) performance of the aids.

SATELLITE BASED TROPICAL CYCLONE INTENSITY FORECASTS

(Cook, J. and T. Tsui, NAVENVPREDRSCHFAC

Results from a recently completed study show the usefulness of a newly developed objective spiral analysis technique as a forecasting aid. Algorithms using persistence and derived spiral parameters show significant skill at estimating current intensity and in making 12 hour intensity forecasts. The 24 hour intensity forecasting skill is only slightly better than persistence. This nowcasting skill is unique because of the stand-alone nature of the SPADS based method.

Also under investigation is a method of studying the relationship of cyclone intensity and cloud patterns in quasi-Lagrangian coordinates. Satellite images of tropical cyclones are rotated and correlated with various intensity parameters.

SYNOPTIC TROPICAL CYCLONE INTENSITY FORECAST

(Gray, W., Colorado State University)

Extensive investigation on tropical cyclone intensity change characteristics is now underway. The study will include: (1) individual case analysis tropical cyclone intensity change with FGGE year and JTWC hand analysis and (2) rawinsonde composite analysis of groups of cyclones experiencing rapid, moderate, weak and negative intensity change. The goal of this study is to develop practical empirical relationships for cyclone intensity change which can be used in an operational forecast environment such as exists at JTWC.

TROPICAL CYCLONE INTENSITY FORECASTS USING THE VERTICAL WIND SHEAR

(Cook, J., and T. Tsui, NAVENVPRDRSCHFAC)

A study of the relationship of tropical cyclone intensity to the large-scale vertical wind shear is currently underway. The data being used are various combinations of the radially averaged vertical shear of the Global Band zonal-wind component for all the western North Pacific tropical cyclones from 1974-81. The wind shear parameters will be related to cyclone intensity by using linear regression techniques.

TROPICAL CYCLONE STRIKE AND WIND PROBABILITIES

Tropical cyclone strike and wind probability is a method for determining up through 72 hours that a tropical cyclone will affect geographic points of interest to the user. Applications presently being developed, tested and implemented for the western North Pacific, and North Indian Ocean, western North Atlantic, and Gulf of Mexico include: strike/wind probabilities and geographic depictions; optimum track ship routing (OTSR) aids; HP-9845/Tactical Environmental Support System (TESS) software for shipboard environmentalists and decision makers; terrain adjusted probabilities; and condition setting aids.

STATISTICAL TROPICAL CYCLONE FORECASTING AIDS FOR THE SOUTHERN HEMISPHERE

(Keenan, T., Bureau of Meteorology, Australia)

Various statistical techniques are being tested for use by JTMC in the southern hemisphere. Australian schemes using multiple linear regression, eigenvector and discriminant analysis of past track data and

synoptic data, are being run on 82/83 storm data over the JTWC area of responsibility. In addition, a technique incorporating both geographic and track orientated prediction schemes is being developed using the FNOC Global Band fields as the developmental data base.

3. PUBLICATIONS

Allen, R.L., 1984: COSMOS: CYCLOPS Objective Steering Model Output Statistics. Proceedings, 15th Technical Conference on Hurricanes and Tropical Meteorology.

COSMOS, a new objective aid used in forecasting the movement of western North Pacific tropical cyclones, is presented. The aid accepts CYCLOPS forecasts at the 850, 700, and 500 mb levels and produces its own forecast based on a statistical analysis of the past performance of CYCLOPS. The design of COSMOS as well as the results of the statistical analysis are presented. Verification of COSMOS during the first eight months of 1983 indicates that the technique may be an improvement over other techniques currently available at JTWC.

Weir, R.C., 1984: Predicting the Acceleration of Northward-moving Tropical Cyclones Using Upper-Tropospheric Winds. Proceedings, 15th Technical Conference on Hurricanes and Tropical Meteorology.

Inconsistent forecasting of the acceleration of northward-moving tropical cyclones entering the domain of the mid-latitude westerlies has been a long-standing weakness in tropical cyclone forecasting. The tracks of tropical cyclones traversing a relative high-density data area of the western North Pacific have been analyzed to verify the acceleration phenomenon, and to correlate the movement with features of the uppertropospheric wind field. The resultant forecast technique is described and the results obtained with its use during the 1982 tropical cyclone season in the western North Pacific are presented.

Weir, R.C., 1983: Tropical Cyclones Affecting Guam (1671-1980). NAVOCEANCOMCEN/JTWC TECH NOTE 83-1.

An update of a previous paper (Holliday, 1975) which presents a climatology of tropical cyclones passing within 180 nm of Guam for the period 1948 to 1980. A review of all typhoons of the 1600's is included. The survey encompasses the frequency, behavior, meteorological effects and descriptive chronicles of Guam tropical cyclones. The major emphasis is on the period since World War II.

TROPICAL STORM SARAH BEST TRACK DATA

	BEST TRAC	:K		WA	RNING				24 H	IOUR F	ORECA	ST		49 H	OUR FO	DRECA!	ST		72 H	IOUR F	DRECA!	5T
						ER	RORS				ER	RORS				ERI	RORS				ERF	RORS
MD/DA/HR	POSIT	MIND	PO	SIT	MIND	DST	MIND	PC	SIT	WIND	DST	MIND	P09	IT	MIND	DST	WIND	PD	SIT	MIND	DST	WIND
861988Z	5.9 136.3	15	8.8	0.0	0.	-0.	ø.	0.0	9.0	0.	-0.	8.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
861986Z	6.4 135.6	15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	ð.	-0.	8.	0.0	0.0	0.	-0.	0.
861912Z	7.8 134.9	15	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.
861918 Z	7.4 134.1	15	0.0	0.0	0.	-8.	ø.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ø.	-0.	ø.
862888Z	7.8 133.3	15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	~0.	8.	0.0	0.0	8.	-0.	0.	0.0	0.0	6.	-8.	0.
862886Z	7.9 132.3	15	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	Ð.	0.0	0.0	0.	-0.	0.
862812Z	8.1 131.2	15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ø.	-0.	Ø.	0.0	0.0	0.	-0.	0.
062018Z	0.3 130.2	15	0.0	0.8	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Э.	0.0	0.0	0.	-0.	0.
862188Z	0.6 129.0	15	8.0	0.0	0.	-0.	8.	0.0	0.0	ø.	-0.	Ð.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
862186Z	8.8 127.8	20	0.0	0.0	8.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	6.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
862112Z	9.3 126.3	25	0.8	0.0	0.	-0.	0.	8.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Ð.	0.0	0.0	0.	-0.	ø.
862118Z	9.9 125.0	25	0.0	0.0	0.	-8.	0.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	Ø.	-0.	ø.
96229 8 Z	10.4 123.3	20	0.0	0.0	₽.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
9 622 9 62	11.4 121.7	15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
0 62212Z	12.2 120.4	15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	8.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
862218Z	12.7 119.0	20	0.8	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ø.	-0.	0.
86238 8 Z	12.7 117.5	15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
8 623 8 6Z	12.8 116.3	15	0.0	0.0	8.	-0.	0.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0 62312Z	12.8 115.3	20	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0 62318Z	12.8 114.3	25	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.
9 62 400 Z	12.8 113.2	25	9.9	9.8	₽.	-0.	Ð.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
062406Z	12.9 112.2	30	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
0 62412Z	13.6 111.6	30	0.0	8.8	8.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
0 62418Z	14.3 111.1	-		110.8	30.	35.		10.1	108.0		103.	5.	9.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
062500Z	15.0 110.6	36		110.5	30.	13.		17.9	107.7	35.	76.	10.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	ø.
062506 Z	15.7 109.9			169.8	35.	8.		18.2	187.5	45.	195.	30.	8.8	0.0	0.	-0.	₽.	0.0	0.0	0.	-0.	0.
862512Z	16.2 109.2			109.5	30.	18.	-5.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.
062518Z	16.4 108.2		• • • •	109.0	25.	76.	-5.	0.0	0.0	0.	-0.	Ð.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
86268 8 Z	16.7 187.3		16.5	107.3	25.	12.	0.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Ø.
862686Z	16.8 106.4	15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	9.0	ø.	-0.	ø.

	ALL	FORECAS	TS		TYPHO	ONS WHIL	E OVER	35 KTS
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	27.	94.	0.	0.	0.	0.	0.	0.
AVG RIGHT ANGLE ERROR	18.	86.	0.	0.	0.	0.	ø.	0.
AVG INTENSITY MAGNITUDE ERROR	2.	15.	0.	0.	Ð.	0.	0.	0.
AVG INTENSITY BIAS	-2.	15.	0.	0.	0.	0.	ø.	0.
NUMBER OF FORECOSTS	6	3	а	A	A	P	R	Я

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1948. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 11. KNOTS

TROPICAL STORM SARAH
FIX POSITIONS FOR CYCLONE NO. 1

	IX O.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
*	1	170000	6.5N 138.5E	PCN 6	T0.0/0.0	INIT OBS ULCC FIX	PGTW
	2	182025	5.3N 136.5E	PCH 4	T0.5/0.5	INIT OBS	PGTW
	3	190610	6.1N 136.4E	PCN 5	T1.0/1.0		RPMK
*	4	192146	7.8N 135.8E	PCN 6	T0.5/0.5 /S0.0/25HRS		PGTW
	5	200000	7.9N 133.2E	PCN 6			PGTW
	6	200300	7.9N 132.4E	PCN 6			PGTW
*	7	200558	9.5N 132.0E	PCN 5	T1.0/1.0 /D0.5/08HRS		PGTW
*	8	201007	9.5N 131.1E	PCN 5		ULCC FIX	PGTW
*	9	201200	9.4N 131.1E	PCH 6		ULCC FIX	PGTW

* 10	201600	9.6N 130.4E	PCH 6	T1.0/1.0 /D0.5/10HRS	ULCC FIX	PGT₩
* 11	201800	9.4N 130.5E `	PCN 6	•	ULCC FIX	PGTW
* 12	202125	9.5N 130.1E	PCN 5		ULCC FIX	PGTW
* 13	210000	9.9N 128.4E	PCN 5		ULCC FIX	PGTW
14	210300	8.1N 128.8E	PCN 5			PGTW
15	211200	9.9N 125.6E	PCN 6		ULCC FIX	PGTW
16	211600	9.8N 125.1E	PCN 6		ULCC FIX	PGT⊎
17	211800	10.0N 124.6E	PCN 6		ULCC FIX	PGTW
18	212166	10.0N 124.1E	PCN 6		ULCC FIX	PGTW
19	220000	10.5N 123.9E	PCN 6		ULCC FIX	PGTW
* 20	220300	18.6N 124.2E	PCN 6	T0.0/0.0	ULCC FIX	PGTW
21	230000	13.8N 117.5E	PCN 6			PGTW
* 22	230300	14.2N 116.0E	PCN 6	T0.0/0.0 /S0.0/24HRS		PGTW
23	240000	13.3N 113.2E	PCN 6	T1.5/1.5-/D1.5/21HRS	ULCC FIX	PGTW
24	240300	13.2N 112.9E	PCN 6		ULCC FIX	PGTW
25	248688	13.3N 112.4E	PCN 6		ULCC FIX	PGTW
26	248651	13.4N 113.4E	PCN 5	T2.0/2.0	INIT OBS	RPMK
27	240900	13.9N 111.7E	PCN 6		ULCC FIX	PGTW
28	241200	14.3N 111.6E	PCN 6	T1.5/1.5 /S0.8/12HRS	ULCC FIX	PGTW
29	241600	14.6N 111.0E	PCN 6			PGTW
30	241800	14.6N 110.5E	PCN 6			PGTW
31	242188	14.5N 110.3E	PCH 6			PGTW
* 32	242323	15.5N 111.BE	PCN 5	T1.5/2.0-/W0.5/14HRS		RPMK
33	250000	15.1N 110.8E	PCN 6	T1.5/1.5-/S0.0/12HRS	ULCC FIX	PGTW
34	250041	15.6N 111.1E	PCN 5	T1.5/2.0-/W0.5/16HRS	0000 1 1/1	RPMK
35	250300	15.2N 110.0E	PCN 6	1110, 210 . 4010, 1011110	ULCC FIX	PGTW
36	250600	15.6N 109.9E	PCN 6		ULCC FIX	PGTW
37	250820	16.0N 109.8E	PCN 3	T1.5/2.0-/W0.5/25HRS	0000 / 1/1	RPMK
38	250900	15.5N 109.6E	PCN 6	1110-210 - 4010-201110	ULCC FIX	PGTW
39	251148	16.4N 109.3E	PCN 3		OLCC TIN	RPMK
40	251148	16.3N 109.5E	PCN 6			RODN
41	251200	16.4N 108.7E	PCN 6			PGTW
42	251600	16.7N 108.0E	PCH 6	T1.5/1.5-/S8.0/16HRS		PGTW
* 43	251800	16.8N 107.2E	PCN 6			PGTW
44	252100	17.3N 107.4E	PCN 6			PGTW
45	252302	16.5N 107.2E	PCN 3	T1.0/1.0	INIT OBS EXP LLCC	ROCH
46	260000	16.6N 107.2E	PCH 4		EXP LLCC	PGTW
	200000	10.00 10/.22	1011		LA LLUC	, G.I.W

AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL			MAX-FLT-LVL-UND ACCRY DIR/VEL/BRG/RNG NAV/MET	EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	
1	210025	8.4N 129.0E	1500FT	1889	15 230 80	130 16 878 38 18 18			+26 +25 +24 29	1

TYPHOON TIP BEST TRACK DATA

	BEST TRE	CK		LUE	RN ING				24	HOUR F	OREC	AST		48 H	OUR F	ORECA	IST		72 H	IOUR I	FORECA	ST
						ER	RORS				E	RRORS				EF	RORS				ER	RORS
HD/DA/HR	POSIT	WIND	Pi	DSIT	WIND	DST		Pf	SIT	MIND) Pi	SIT	UIND			PC	SIT	UIN		WIND
878912Z	11.4 127.4		0.0	0.0	0.	-0.	8.	0.0	8.8		-8.	0.	0.0	0.0	0.	-0.	0.		8.0	0.	-0.	В.
																	٥.	0.0		۵.	7.7	Ι.
878918Z	12.4 125.3		0.0	0.0	ø.	-0.	ø.	0.0	0.0	-	-0.		0.0	0.0	0.	-B.	٠.	0.0	0.0	٠.	-0.	₽.
871 888 2	12.8 123.3	25	9.0	0.0	0.	-0.	ø.	8.0	9.0	9.	-0.	Ø.	0.0	0.8	ø.	-0.	0.	0.0	0.0	0.	-0.	8.
871886Z	13.3 121.6	30	9.0	0.0	Θ.	-0.	0.	0.0	8.0	9.	-0.	0.	0.0	8.8	0.	-0.	8.	0.0	0.0	0.	-0.	8.
071012Z	13.6 120.2	2 30	13.9	119.6	35.	39.	5.	15.8	114.9	45.	53.	-20.	17.6	110.3	45.	133.	-10.	18.9	107.7	35.	204.	5.
871818Z	13.6 118.9	58	13.9	118.9	45.	6.	-5.	15.5	113.5	60.	91.	0.	17.3	109.2	45.	178.	-5.	19.3	106.9	35.	226.	10.
871186Z	14.4 117.7	60	14.3	117.6	60.	8.	ø.	16.8	113.2	90.	40.	20.	18.3	168.6	65.	177.	30.	0.8	0.0	0.	-0.	0.
871186Z	15.1 116.7	60	15.1	116.5	60.	12.	ø.	17.4	111.9	60.	75.	5.	18.7	107.9	50.	207.	20.	0.0	0.0	Ð.	-0.	0.
671112Z	15.6 115.6	65	15.6	115.9	65.	6.	8.	17.6	112.2	70.	29.	15.	19.0	109.2	50.	137.	20.	0.0	0.0	0.	-0.	0.
871118Z	16.2 114.9	60	16.3	114.8	65.	8.	5.	18.2	111.2	70.	51.	20.	19.7	108.1	50.	157.	25.	0.0	0.0	Ø.	-0.	0.
871286Z	16.8 113.9	60	16.7	114.0	60.	Θ.	0.	18.7	110.3	50.	80.	15.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
8712 86 Z	17.3 113.2	2 55	17.3	113.2	60.	0.	5.	19.6	109.7	50.	92.	20.	0.0	0.0	₽.	-0.	0.	8.8	0.0	0.	-0.	0.
071212Z	17.9 112.6	5 55	18.3	112.1	55.	37.	0. :	20.7	189.2	40.	84.	10.	0.0	0.0	Ø.	-0.	ø.	0.0	0.0	0.	-0.	0.
871218Z	18.6 112.6	50	18.7	112.0	45.	6.	-5.	21.9	111.3	25.	66.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
871388Z	19.4 111.5	35	19.5	111.5	40.	6.	5.	0.8	0.0	0.	-0.	0.	0.0	0.0	0.	-8.	Ø.	0.0	0.0	Ø.	-0.	0.
071306Z	20.2 111.2	2 30	20.2	111.0	35.	11.	5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-8.	ø.	0.0	0.0	ø.	-0.	0.
071312Z	20.8 110.7	30	21.0	110.0	30.	13.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
871318Z	21.3 110.3	25	21.3	110.3	25.	ø.	ø.	0.0	0.0	ø.	-0.	Ð.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS					
	WRNG	24-HR	48-HR	72-HR	URNG	24-HR	48-HR	72-HR		
AVG FORECAST POSIT ERROR	12.	66.	165.	215.	10.	60.	163.	8.		
AVG RIGHT ANGLE ERROR	8.	53.	160.	204.	6.	48.	156.	0.		
AVG INTENSITY MAGNITUDE ERROR	3.	13.	18.	8.	3.	14.	15.	0.		
AVG INTENSITY BIAS	1.	9.	13.	8.	1.	8.	5.	0.		
NUMBER OF FORECASTS	14	18	6	2	18	7	3	8		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1286. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 12. KNOTS

TYPHOON TIP FIX POSITIONS FOR CYCLONE NO. 2

FIX	TIME	FIX				
NO.	(2)	POS1T10N	ACCRY	DVORAK CODE	COMMENTS	SITE
1	080911	9.5N 132.4E	PCN 6			PGTW
2	0 81200	9.3N 131.9E	PCN 6			PGTW
3	082151	11.BN 130.0E	PCN 5			PGTW
4	09000 0	10.7N 129.5E	PCN 6			PGT₩
5	090300	10.0N 129.2E	PCN 6	T0.0/0.0	INIT OBS	PGTW
6	090600	10.9N 129.1E	PCN 6			PGTW
7	0 90900	11.0N 128.3E	PCN 6		ULCC FIX	PGTW
8	0 91200	11.1N 127.6E	PCN 6		ULCC FIX	PGTW
9	091600	11.8N 126.2E	PCN 6	T1.5/1.5-	INIT OBS	PGT⊎
10	091800	12.3N 125.6E	PCN 6			PGTW
11	0 921 00	12.5N 125.0E	PCN 6			PGTW
12	092130	12.8N 122.6E	PCH 5	T1.5/1.5	INIT OBS	RPMK
13	100000	12.9N 122.7E	PCN 4			PGTW
14	100300	12.9N 122.5E	PCN 4	T2.5/2.5+/D1.0/11HRS		PGTW
15	100600	13.3N 121.4E	PCH 4			PGTW
16	100900	13.IN 121.1E	PCN 6			PGTW
17	101010	13.4N 120.9E	PCN 3			PGTW
18	101200	13.5N 120.0E	PCH 4			PGTW
19	101600	13.8N 119.4E	PCN 6	T4.0/4.0 /D1.5/13HRS		PGTW
20	101800	13.8N 119.1E	PCN 6			PGTW
21	101942	13.7N 118.1E	PCH 6			RODN
22	102100	13.8N 118.3E	PCH 6			PĞT₩
23	102250	14.2N 118.0E	PCN 5	T3.0/3.0 /D1.5/25HRS		RPMK
24	102357	14.0N 117.6E	PCN 3	T3.5/3.5	INIT OBS	RODN
25	102357	14.4H 117.3E	PCN 3			RPMK
26	110000	14.6N 117.5E	PCN 4			PGTW
27	110300	14.8N 117.3E	PCN 4	T3.5/3.5-/D1.0/11HRS		PGT₩
28	110644	15.4N 116.6E	PCN 3		EXP LLCC	PGTW
29	110900	15.5N 116.4E	PCH 4		EXP LLCC	PGTW
30	111056	15.6N 115.9E	PCN 4		EXP LLCC	PGTW

31	111600	16.1N 115.2E	PCH 4	T4.0/4.0-/S0.0/13HRS		PGTW
32	111800	16.5N 114.6E	PCN 6			PGT₩
33	111929	16.0N 113.8E	PCN 5		ULCC FIX	RODN
34	112100	16.9N 114.2E	PCN 6			₽GTW
35	112229	16.7N 114.4E	PCN 3	T3.0/3.5 /W0.5/23HRS		RPMK
36	112315	16.6N 114.0E	PCN 3	T4.8/4.8 /D8.5/24HRS	EXP LLCC	RODN
37	112335	16.8N 114.1E	PCN 3	T3.0/3.5 /W0.5/24HRS	EXP LLCC	RPMK
38	120000	16.8N 113.9E	PCN 4		EXP LLCC	PGTU
39	120300	17.3N 113.3E	PCN 4	T4.8/4.8-/58.8/11HRS		PGT⊍
40	128688	17.2N 113.0E	PCN 6			PGTU
41	120632	17.6N 112.8E	PCH 3		EXP LLCC	PGTU
42	120632	18.0N 112.7E	PCN 3	T3.0/3.5 /S0.0/08HRS	EXP LLCC	RPMK
43	120900	17.9N 112.6E	PCH 4		EXP LLCC	PGTU
44	121200	18.2N 112.2E	PCN 4		271 2200	PGTW
45	121209	17.3N 111.3E	PCN 5			RODN
46	121215	17.9N 112.3E	PCN 5			RPMK
47	121600	18.5N 112.1E	PCH 4	T2.5/3.5 /W1.5/13HRS	EXP LLCC	PGTW
48	121800	18.7N 112.1E	PCN 4	12.3/3.3 /WI.3/13/R3	EXP LLCC	PGTU
49	121917	19.1N 111.5E	PCN 3		EXP LLCC	PGTU
50	122100	19.3N 111.8E	PCH 4		EXP LLCC	PGTU
51	122208	19.4N 111.5E	PCN 3	T2.5/3.0-/W0.5/24HRS	EXP LLCC	RPMK
52	130000	19.5N 111.5E	PCN 4		EXP LLCC	PGTU
53	130300	19.7N 111.4E	PCN 4	T1.5/2.5-	INIT OBS	PGTW
54	138600	20.0N 111.3E	PCH 4		EXP LLCC	PGT₩

AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT		MAX-SFC-UND VEL/BRG/RNG					EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
1	110030	14.5N 117.7E	788MB	2977	984	78 890 25	178	69 118	30	10 5	CIRCULAR	20	+14 +17 + 9	2
2	110638	15.4H 116.4E	700MB	2938		60 030 74	120	78 828	21	55			+15 +17	3
3	111105	15.5N 116.1E	700MB	2921	977	78 898 4	989	54 360	30	5 5	CIRCULAR	30	+14 +20	3
4	112152	16.5N 114.2E	700MB	2934	981	50 020 30	130	65 020	28	15 5	CIRCULAR	20	+13 +18 +13	4
5	120044	17.8N 113.8E	788MB	2931		80 170 13	050	64 270	20	10 15			+14 +18 +11	4

RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB-CODE ASUAR TODEF	CONTENTS	RADAR POSITION	SITE WMD NO.
1	110000	14.1N 117.5E	LAND				1888/ ////	EYE 78 PCT CIR OPEN NU	16.3H 120.6E	98321
ž		14.2N 117.2E					1891/ 52983	EYE 68 PCT CIR OPEN NU	16.3N 120.6E	98321
3	110200	14.4H 116.9E	LAND				1893 / 53812	EYE 68 PCT CIR OPEN N	16.3N 120.6E	98321
4	130350	19.9N 110.0E	LAND				2//// 53188		28.8N 118.3E	59758

SYNOPTIC FIXES

FIX	TIME	FIX	INTENSITY	MERREST	CONTENTS
NO.	(Z)	POSITION	ESTIMATE	DATA (NPI)	
	138908	13.4N 118.5E 28.6N 118.8E	845 838	825 838	SHIP DESERVATION PRESSURE EST. 995 NB

TYPHOON VERA BEST TRACK DATA

	BEST TRAC	ж		u	arn ing		0000		24	HOUR F		AST RRORS		48 H	IOUR F		RST		72	HOUR F		RST
	*****		. ~				RORS	~						AC 1 T			CKUKS F WIND	~~		MIND		KKUKS F WIND
MD/DA/HR		MIND		DSIT	MIND	DST	MIND		DSIT	MINE				DSIT	MIND		MIKD		SIT		-B.	
0709062	9.5 146.2	20	8.0	8.8	0.	~0.	IJ.	9.0	0.6		-0.	0.	8.0	0.0	0.	-0.	٥.	0.0 0.0	8.8	8.	-0. -0.	8. 8.
676912Z	9.8 145.4	20	8.0	8.0	8.	-6.	ø.	0.0	0.6		-0.	0.	0.0	8.0	0.	-0.	ь.			e.		
878918Z	8.5 144.6	20	8.8	0.0	0.	-6.	Ð.	0.0	8.6		-0.	8.	8.0	0.0	0.	-0.	8.	0.0	8.6	0.	-0.	8.
871888Z	8.4 143.3	28	0.0	0.0	0.	-0.	0.	0.0	0.0		-0.	0.	0.0	8.8	0.	-0.	8.	0.0	0.0	0.	~0.	0.
871886Z	9.8 142.8	25	9.9	9.9	8.	-0.	0.	9.9	9.6		-0.	Ð.	0.0	0.0	0.	-Ø.	Ð.	0.0	0.0	Ð.	-0.	Ð.
871812Z	9.3 140.0	25	0.8	0.0	ø.	-0.	0.	0.0	0.8		-0.	ø.	0.0	0.0	0.	-0.	ø.	0.8	0.0	0.	-0.	0.
971818Z	9.4 138.1	25	0.0	0.0	Ð.	-0.	0.	0.0	0.6		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.
871188Z	9.7 136.6	25	6.0	0.0	0.	-0.	0.	0.0	0.6		- 0 .	₽.	0.0	0.0	0.	-0.	0.	0.0	0.0	₽.	-8.	0.
8711862	10.1 135.4	25	0.0	0.0	ø.	-8.	ø.	0.0	0.6		-0.	0.	0.0	0.0	ø.	~₫.	0.	0.0	0.0	0.	-0.	0.
071112Z	10.6 134.4	38	0.0	0.0	ø.	-0.	0.	0.0	0.0		-0.	Ø.	0.0	0.0	0.	-0.	ð.	0.0	0.0	ø.	-0.	ø.
871118Z	10.0 133.4	30	0.0	0.0	0.	-0.	ø.	0.0	8.6		-0.	0.	0.0	0.8	0.	-0.	Ð.	0.0	0.0	0.	-ð.	0.
871298Z	11.0 132.3	30	9.0	0.0	0.	-0.	0.	0.0	0.0		-0.	0.	0.0	0.0	0.	-0.	8.	0.0	0.0	0.	-0.	0.
871286Z	11.4 131.1		11.7	136.7	38.	38.		13.1	127.1		118.		14.4			117.			119.8		136.	-5.
8 71212Z	11.6 129.9		11.7		30.	36.		14.0	124.		223.		15.8	120.4		230.			117.3		202.	-5.
6 71216Z	11.4 129.2		12.8	120.4	40.	59.		14.8	124.3		163.		16.0	120.0		188.			117.0		168.	-10.
871388Z	11.3 120.6		11.2		45.	В.			124.6		82.			119.3		124.			114.5		163.	-15.
871386Z	11.3 127.9	55	11.3	127.9	55.	₽.	ø.	12.8	123.2	2 65.	77.	-15.	14.3	119.7	55.	47.			116.7	60.	83.	-15.
0 71312Z	11.7 127.1	68	11.7	127.0	60.	6.	8.	13.1	122.5	5 55.	54.	-25.	15.2	110.6	60.	31.			115.5	70.	70.	-16.
071318Z	12.1 126.3	65	12.2	126.0	65.	19.	0.	13.4	121.7	7 55.	42.	-20.	15.6	117.8	60.	30.			114.6		194.	-15.
871488Z	12.5 125.4	75	12.4	125.4	70.	6.	-5.	13.6	121.5	5 55.	36.	-15.	15.1	117.8	65.	115.	-5.	17.3	115.3	75.	199.	-15.
871486Z	13.8 124.5	66	12.9	124.4	65.	8.	-15.	14.2	119.7	7 55.	51.	-5.	16.3	116.4	75.	71.	8.	18.4	113.7		169.	-15.
871412Z	13.3 123.4	80	13.4	123.3	60.	8.	-20.	14.7	118.6	60.	51.	0.	17.1	115.3	70.	50.	-10.	18.9	112.7	60.	185.	-10.
0714102	13.8 122.3	75	13.9	122.3	60.	6.	-15.	15.5	118.6	60.	59.	~5.	17.8	115.7	65.	136.	-20.	19.9	113.1	50.	277.	-15.
871588Z	14.2 121.4	70	14.3	121.1	60.	18.	-10.	16.7	116.9	70.	11.	Ø.	19.2	114.4	55.	120.	-35. 2	21.4	112.5	45.	309.	-10.
071506Z	14.7 128.4	60	14.8	120.1	55.	10.		17.0	116.5	75.	53.	e.	19.4	114.2	55.	181.	-25.	21.8	112.3	40.	370.	0.
871512Z	15.4 119.1	60	15.5	119.2	55.	Θ.	-5.	18.4	115.5	70.	63.	-18.	21.2	112.8	50.	196.	-20.	0.0	0.0	ø.	-0.	0.
0715182	16.1 117.8			117.7	60.	13.			114.6		42.		21.9	111.9		228.	-15.	0.0	0.0	0.	-0.	0.
0716002	16.7 116.7	70	17.0	116.6	65.	19.			112.6		41.	-25.	21.8	110.4	40.	198.	-15.	0.0	0.0	0.	-0.	0.
071606Z	17.2 115.6	75	17.3	115.4	78.	13.			111.2		21.	-28.	22.6	188.2	35.	159.	-5.	8.8	9.8	9.	-0.	0.
0716122	17.8 114.6			114.6	70.			19.8	110.9		74.	-15.	0.0	0.0	0.	-Ø.	ø.	0.0	0.0		-0.	ø.
0716182	18.4 113.4			113.2	80.	17.			109.0		58.	0.	0.0	0.0	ě.	-0.	ø.	0.0	0.0	e.	-0.	0.
071700Z	19.0 112.3			112.1	90.	13.		21.7	100.0		74.	10.	0.0	0.0	ě.	-0.	ø.	0.0	0.0	ø.	-0.	ø.
071706Z	19.6 111.0		19.8	111.1	85.	13.		21.8	107.6		110.	20.	9.0	0.0	0.	-0.	В.	0.0	0.0		-A.	ø.
0717122	19.9 109.6		19.8	109.7	65.	8.	-5.	0.0	0.8		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
871718Z	20.3 169.2		20.3		65.	17.	-5. 0.	0.0	0.0		-0.	8.	0.0	0.0	0.	-0. -0.	0.	0.0	0.0	ð. ð.	-0.	0.
071900Z	20.9 107.0			100.5	55.	6.	ø. Ø.	0.0	0.0		-0.	0.	0.0	0.0	Ø.	-0. -0.	Ð.	6.0	0.0		-8.	8.
0710002 0710067	20.3 107.0			185 8	33. 45	٠.	٥. 5	0.0 a a	0.6		-0.	ο.	9.0 9.9	0.0 a a	Ø.	-8.	9.	9 B	9.9	ο.	-0. -0	a.

	ALL FORECASTS				TYPHOONS WHILE OVER 35 KTS					
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR		
AVG FORECAST POSIT ERROR	14.	72.	131.	187.	14.	72.	131.	187.		
AVG RIGHT ANGLE ERROR	9.	39.	66.	70.	9.	39.	66.	70.		
AVG INTENSITY MAGNITUDE ERROR	5.	13.	16.	11.	5.	13.	16.	11.		
AVG INTENSITY BIAS	-4.	-10.	-16.	-11.	-5.	-10.	-16.	-11.		
NUMBER OF FORECASTS	25	21	17	13	24	21	17	13		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2546. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 12. KNOTS

TYPHOON VERA FIX POSITIONS FOR CYCLONE NO. 3

Φ

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	COMPENTS	SITE
1	090600	9.6N 145.6E	PCN 6	T0.5/0.5	INIT OBS ULCC FIX	PGTW PGTW
* 2	<i>0</i> 9 0 850	9. IN 144. IE	PCH 5			
* 3	092238	9.5N 142.5E	PCN 5		ULCC FIX	PGTW
* 4	100300	9.3N 141.4E	PCN 6	T1.5/1.5 /D1.0/21HRS	ULCC FIX	PGT₩
5	100600	9.1N 142.1E	PCN 4			PGTW
6	100829	9.2N 141.5E	PCN 5			PGTW
7	100936	9. IN 141.0E	PCN 6			PGTW
á	101200	8.9N 140.8E	PCN 6			PGTW
-						
9	101600	9.4N 138.4E	PCN 6	T2.0/2.0 /D0.5/13HRS		PGTW
10	101600	9.7N 137.6E	PCN 6			PGTW
11	102109	10.2N 137.2E	PCN 5		ULCC FIX	PGTW

12	102109		137.4E	PCN 5	T2.0/2.0	INIT OBS	RPMK
13	110000		136.7E	PCN 6			PGTW
14	110300		135.8E	PCN 4	T2.0/2.0 /D0.5/11HRS	IN CC CTV	PGTU
15	110644		135.2E	PCN 6		ULCC FIX	PGTW PGTW
	110949		134.5E	PCN 6 PCN 6		ULCC FIX ULCC FIX	PGTW
17 18	111056 111600		134.1E 133.4E	PCN 6	TO 8/2 8-/58 8/17495	OLCC PIX	PGTW
19	111747		132.8E	PCN 6	T2.0/2.0-/S0.0/13HRS		PGTW
20	112048		132.2E	PCN 6			PGTW
21	112335		131.9E	PCN 5	T2.5/2.5 /D0.5/26HRS		RPMK
22	120000		132.5E	PCN 6	12.3/2.3 / DO:3/201K3		PGTW
23	120300		131.2E	PCN 6	T2.5/2.5 /D0.5/11HRS		PGTW
	120600	11.8N		PCN 6	12.072.3 19010 11.110		PGTW
25	120632	11.9N		PCN 5			PGTW
26	120632		132.0E	PCN 5			RPMK
27	120928		129.7E	PCN 6			PGTW
28	121208		129.2E	PCN 6			PGTW
29	121600		128.8E	PCN 6	T3.8/3.8 /D1.8/13HRS		PGTW
30	121800	11.3N	129.0E	PCN 6			PGTW
31	121917	11.5N	129.0E	PCN 6			PGTW
32	122100	11.5N	129.2E	PCN 6			PGTW
33	122313	10.9N	128.7E	PCN 5	T3.0/3.0 /D0.5/24HRS		RPMK
34	122314	11.5N	128.9E	PCN 6			PGTW
35	130000		128.3E	PCN 4			PGTW
36	130300		127.8E	PCN 4	T3.5/3.5 /D1.0/11HRS		PGTW
37	130620		127.9E	PCN 3			PGTU
	130907		127.3E	PCN 3			PGTW
39	131200		127.0E	PCN 2	T4 0 44 0 40 0 4 7 100		PGTW
40	131600		126.2E	PCN 2	T4.0/4.8-/D1.0/13HRS		PGTW PGTW
41	131800		126.0E	PCN 4			PGTW
42 43	131905 132100		125.9E 125.5E	PCN 5 PCN 5			PGTW
44	132147		125.5E	PCN 5		ULCC FIX	PGTW
45	132251		125.5E	PCN 5		OLCC PIA	PGTW
46	132351		125.6E	PCN 5	T4.5/4.5-/D1.5/24HRS		RPMK
47	140000		125.5E	PCN 2	14.07 410 7 D 110 E 4 ING		PGTW
48	140300		124.9E	PCN 2	T4.5/4.5-/D1.0/11HRS	EYE DIA 18NM	PGTW
49	140600		124.4E	PCN 2			PGTW
50	140607		124.4E	PCN 1	T4.5/4.5	INIT OBS	RODN
51	140900	13.1N	123.8E	PCN 4			PGTW
52	141027		123.7E	PCN 4			PGTW
53	141131		123.7E	PCN 1			RODN
54	141131		123.6E	PCN 1			RPMK
55	141200		123.2E	PCN 2			PGTW
56	141600		122.7E	PCN 2	T4.5/4.5-/D0.5/13HRS		PGTW
57	141800		122.3E	PCH 2			PGTW
58	141852		122.2E	PCN 2			PGT⊎
	142100		121.BE	PCN 2			PGTW
60	142126		121.6E	PCN 4	T4 0 /4 E 4 D E /22HDC		PGTW RPMK
61 62	142156 150000		121.5E	PCN 1 PCN 4	T4.0/4.5 /W0.5/22HRS		PGTW
	150300		121.1E 120.8E	PCN 4	T3.5/4.5+/W1.0/11HRS		PGTW
	150600		120.4E	PCN 4	13.3/4.3*/WI.0/IINK3		PGTW
65	151006		119.7E	PCN 4			PGTW
66	151110		119.2E	PCN 3			RODN
67	151110		119.3E	PCH 4			PGTW
68	151600		118.1E	PCN 4	T4.0/4.0 /D0.5/13HRS		PGT₩
69	151800	16.2N	117.7E	PCN 4			PGTW
79	152100	16.4N	117.1E	PCN 4			PGTW
71	152349	16.BN	116.8E	PCN 3	T4.0/4.0+/S0.0/22HRS		RPMK
72	168000		116.6E	PCN 4		51.5 ABS. 1:	PGTW
73	160300		115.8E	PCN 2	T4.5/4.5 /D1.0/11HRS	EYE OPEN N	PGTW
74	160600		115.3E	PCN 2		1117 000	PGTW
75 76	160725 160900	17.2N 17.7N	115.3E	PCN 3 PCN 4	T4.5/4.5	INIT OBS	RODN PGTW
76 77	161200		114.8E	PCN 4			PGTW
78	161600		113.5E	PCN 6	T5.8/5.8-/D1.8/13HRS		PGTW
79	161800		113.1E	PCN 6			PGTW
80	162100		112.6E	PCN 6			PGTW
81	162225		112.1E	PCN 3			RODH
82	162327		112.5E	PCN 5	T4.5/4.5-/D0.5/24HRS		RPMK
93	170000		112.1E	PCN 6		ULCC FIX	PGTW
84	170300	19.2N	111.6E	PCN 6	T4.0/4.5-/W1.0/11HRS		PGTW
85	170600		111.0E	PCH 6			PGTW
86	170712		110.7E	PCN 5	T4.8/4.5-/W8.5/88HRS		RPMK
87	170900		110.5E	PCN 6			PGTW
89	171105		109.5E	PCN 1			RODN
89	171105		109.9E	PCN 4			RPMK
90	171200		109.0E	PCN 6	T4 5 /4 5		PGTW
91	171207		109.6E	PCN 2	T4.5/4.5		RODN PGTW
92 93	171600 171800		108.5E 108.1E	PCN 6 PCN 4	T3.5/4.0-/W1.0/13HRS		PGTW
93 94	171957		100.1E	PCN 3			RODN
95	172100		107.3E	PCN 4			PGTW
96	172204		107.0E	PCN 5			RODH
97	172204		106.9E	PCN 5		ULCC FIX	RPMK
98	180000		107.0E	PCN 6			PGTW
93	188300		106.3E	PCN 6	T3.0/3.5-/W1.0/11HRS		PGTW
*100	180600		104.8E	PCN 6			PGTW
*101	188659		104.7E	PCN 5	T2.5/2.5		RODH
102	190900	21.0N	104.0E	PCH 6			PGT₩

PGTW PGTW

AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT	700MB HGT	08S MSLP	MRX-SFC VEL/BRG								EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
1 2 3 4 5 6 7 8	128116 122287 130059 130959 131224 150900 151136 160656 161106 162200	11.1N 132.2E 11.1N 128.4E 11.2N 128.5E 11.5N 127.7E 11.8N 126.9E 15.2N 119.8E 15.6N 118.8E 17.3N 115.8E 17.5N 114.8E	1588FT 1588FT 1588FT 7881B 7881B 7881B 7881B 7881B 7881B 7881B	2966 2954 2959 2970	1084 992 993 986	30 048 40 160 45 140 50 290 35 230 75 010 40 270 70 070	25 45 35 90 38 30	818	36 51 52 69 55 65 73 68	288	168 68 68 52 52 45 95 38 15	12 5 15 15	8 15 10 8 6	CIRCULAR ELLIPTICAL CIRCULAR CIRCULAR CIRCULAR	30 20 18 360 48 35 40	+25 +24 +14 +12 +13 +12 29 +13 +13 +11 +13 +11 +14 +12 +15 +16 +16 +15	2 3 4 4 5 5 8 8

RADAR FIXES

						RADA	R FIXES			
FIX	TIME	FIX			EYE	EYE	RADOB-CODE		RADAR	SITE
NO.	(Z)	POSITION	RADAR	ACCRY	SHAPE	DIAM	ASWAR TDDFF	COMMENTS	POSITION	WHO NO.
1	131466	11.9N 126.8E					10303 40000	EYE 80 PCT CIR OPEN E EYE 80 PCT CIR OPEN N EYE 80 PCT CIR OPEN W EYE 108 PCT CIR OPEN W	14.0N 124.3E	98447
	131430 131506	11.9N 126.8E 11.9N 126.8E					10513 42905 10513 40000	EYE BO PUT CIR UPEN E	14.0N 124.3E	98447 98447
	131530	11.9N 126.7E					10512 40000	EYE 80 PCT CIR OPEN E	14.0N 124.3E	98447
	131600	11.9N 126.8E					10513 40000	EYE 80 PCT CIR OPEN E	14.0N 124.3E	98447
6	131630	12.1N 126.7E					18422 42988	EYE 80 PCT CIR OPEN N	14.8N 124.3E	98447
7 B	131700 131730	12.2N 126.5E 12.2N 126.3E					10422 43219 10412 42821	EYE BO PCT CIR OPEN N	14.0N 124.3E	98447 98447
	131730	12.2N 126.3E					10513 42712	EYE BO PCT CIR OPEN W	14.8N 124.3E	98447
	131838	12.2N 126.1E					12653 42918	EYE 100 PT ELPTCL AXIS 68/30	14.8N 124.3E	98447
	132330	12.4N 125.5E					10523 42915	EYE DIA 30 KMS	14.0N 124.3E	98447
	140000	12.5N 125.4E					10523 43208	EYE 100 PCT CIR DIA 30 KMS	14.0N 124.3E	98447
13 14	140000 140030	12.5N 124.4E 12.5N 125.4E					11981 //// 18512 43288	EVE DIG TO PMS	10.3N 124.0E	98646 98447
15	148188	12.4N 125.3E					10513 42710	EYE DIA 30 KMS	14.0N 124.3E	98447
16	140100	12.5N 125.2E	LAND				20840 52920		10.3N 124.0E	98646
17	148138	12.6N 125.2E					18512 43216	EYE DIA 38 KMS	14.0N 124.3E	98447
19 19	140200 140300	12.6N 125.1E 12.7N 124.8E					10512 42711 10512 42811	EYE DIR 30 KMS	14.0N 124.3E	98447 98447
28	140300	12.8N 124.8E	LAND				3/// 42818	EYE IN BLIND SECTOR	10.3N 124.0E	98646
21	140310	12.7N 124.8E	LAND				10512 42909	EYE DIA 25 KMS	14.0N 124.3E	98447
22	140400	12.7N 124.7E					10512 42710	EYE DIA 25 KMS	14.0N 124.3E	98447
23 24	146439 146566	12.8N 124.7E 12.8N 124.6E					10512 43216 10512 43205	EYE DIR 38 KMS	14.8N 124.3E	98447 98447
25	140600	12.9N 124.5E					10512 43213	EIE DIN 30 KID	14.0N 124.3E	98447
	140030	13.2N 124.0E					18512 42915	EYE 100 PT ELPTCL AXIS 60/30 EYE DIA 30 KMS EYE 100 PCT CIR DIA 30 KMS EYE 100 PCT CIR DIA 30 KMS EYE DIA 25 KMS EYE IN BLIND SECTOR EYE DIA 25 KMS EYE DIA 25 KMS EYE DIA 25 KMS EYE DIA 30 KMS EYE DIA 30 KMS EYE DIA 30 KMS	14.0N 124.3E	98447
27	140630	13.2N 124.2E					2051/ 43294		14.1N 123.0E	98440
28	140900	13.4N 124.2E					2041/ 43411		14.1N 123.0E	98440 98440
29 38	141838	13.4N 124.0E 13.2N 123.9E					1061/ 43205 1061/ 42211		14.1N 123.0E 14.1N 123.0E	98440
31	141838	13.2N 123.6E					10512 42611		14.0H 124.3E	98447
32	141100	13.3N 123.0E	LAND				1061/ 42987		14.1N 123.0E	98440
33	141110	13.3N 123.7E					1061/ 42705		14.1N 123.0E	98448
34 35	141118 141288	13.4H 123.4E 13.3H 123.6E					10513 42917 1052/ 42707		14.0N 124.3E 14.1N 123.0E	98447 98440
36	141230	13.3N 123.4E					1051/ ////		14.1N 123.0E	98440
37	141238	13.4H 123.3E	LAND				10513 42903		14.0N 124.3E	98447
38	141300	13.3H 123.3E					18518 42786	EVE 944 35 KM	14.1N 123.0E 14.0N 124.3E 14.1N 123.0E	98448 98447
39 40	141330	13.4N 123.2E 13.4N 123.2E					10513 42713 10310 43207	EYE DIA 25 KMS	14.0N 124.3E	98440
41	141400	13.3N 123.0E					10553 42715		14.8N 124.3E	98447
42	141400	13.5N 123.1E					10611 42905		14.1N 123.0E	98440
43	141438	13.4N 123.1E					18611 42984		14.1N 123.0E	98440
44	1416 88 141638	13.5N 122.9E 13.6N 122.8E					1132/ 43205 1031/ 43005		14.1N 123.0E 14.1N 123.0E	98440 98440
46	142200	14.1N 121.6E					10310 52712		14. IN 123.0E	98440
47	142200	14.8N 121.8E					4/// 52016		16.3N 120.6E	98321
48	142300	14.1N 121.5E					21320 52709	EYE 60 PCT CIR DIA 50 KMS	14.1N 123.0E	98449
49 50	142300 150000	13.8N 122.2E 14.2N 121.3E					1074/ 52912 21340 52812	ETE 60 PC CIR DIN 30 KIS	14.1N 123.0E	98321 98448
51	150030	14.3N 121.1E					35/51 52913		14.1N 123.0E	98440
52	150130	14.8N 120.2E	LAND	POOR					15.2H 128.6E	98327
53	158288	14.7N 128.3E		COOD			727 / 4 771 / 4		15.2N 120.6E	98327
54 55	150300 150300	14.4N 120.7E 14.8N 128.7E		FAIR			323// 531//		14.8N 120.2E 15.2N 120.6E	98426 98327
56	150330	14.5N 120.6E					2037/ 331//		14.8N 120.2E	98426
57	150400	14.5N 120.5E					3405/ 631//		14.8N 120.2E	98426
58	158488	14.6N 128.5E		POOR			7155 4 500 44		15.2N 120.6E	98327 98426
59 68	158438 158588	14.6N 120.5E 14.3N 121.1E					3155/ 529// 35/51 52913		14.8N 120.2E 14.1N 123.0E	98426 98440
61	150500	14.8N 120.3E		FAIR					15.2N 120.6E	98327

62	150600	14.8N 120.2E	LAND	FAIR		15.2N 128.6E	98327
		15.1N 120.1E			3434/ 733//	14.8N 120.2E	98426

SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)		CONTENTS
2	171200	19.7N 110.5E 19.8N 109.7E 20.9N 106.4E	08 0 065 050	020 015 010	WMO 59758 WMO 59845 WMO 48826	59758

SUPER TYPHOON WAYNE BEST TRACK DATA

	BEST TRAC	CK		u	arn ing	50	0000		24 1	10UR I	FOREC	AST RRORS		46 H	IOUR F				72 H	IOUR I	FOREC	
							RORS										RORS					RRORS
HO/DA/HR	POSIT	GHID	P	DSIT	MIHD	DST	CHIM.	P	3S I T	MIH	d de	מאוש ד	P	DSIT	WINI	DST	L MIND	PC	DSIT	WIN	D DS	T WIND
8728182	8.5 138.9	20	0.0	0.0	8.	-0.	0.	0.0	8.0	0.	-0.	0.	0.0	8.8	0.	-0.	0.	0.0	0.0	Ð.	-0.	0.
8721 98 Z	9.4 137.8	25	8.8	0.0	8.	-0.	0.	0.0	0.8	0.	-0.	0.	8.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	8.
872186Z	10.6 136.8	25	0.0	0.0	ø.	-0.	ø.	0.0	0.0	Đ.	-0.	0.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	Ð.
872112Z	11.8 136.2	25	0.0	0.0	ø.	-D.	ø.	0.0	0.0	ø.	-0.	ø.	9.0	0.0	ø.	-Ø.		0.0	0.0	ø.	~8.	ø.
072118Z	13.0 135.0	25	0.0	0.0	a.	-Ð.	0.	0.8	0.0	0.	-0.	8.	0.0	0.0	ø.	-8.	٥.	0.0	0.0	0.	= -	0.
872298Z					Ξ-			= - =		٥.							٥.				-0.	
		25	0.0	0.0	0.	-0.	Ø.	0.0	8.0	٠.	-0.	0.	0.0	0.0	. 0.	-0.	٥.	0.0	0.0	0.	-0.	0.
8722 8 6Z	14.7 133.9		14.6	134.1	25.	13.		16.2	129.9	40.	96.		18.2			205.	-80.	20.0	123.7	65.	371.	-15.
0 72212Z	15.4 132.8	40	15.2	132.6	30.	17.	-10.	17.3	129.2	40.	106.	-40.	19.4	126.7	55.	283.	-65.	21.5	124.7	65.	476.	20.
872218Z	16.1 131.6	50	16.1	131.8	45.	12.	-5.	18.4	128.7	65.	150.	-35.	20.4	126.1	75.	319.	-35.	22.4	124.0	88.	513.	50.
072300Z	16.8 138.2	55	16.8	130.2	50.	0.	-5.	19.9	125.8	70.	72.	-50.	22.9	122.7	80.	185.	-15.	0.0	0.0	ø.	-0.	ø.
872386Z	17.4 128.8	65	17.4	128.8	65.	ø.	Ð.	20.4	124.3	85.	72.		23.5	121.1	70.	160.	-10.	0.0	0.0	ø.	-0.	0.
072312Z	18.2 127.6	80	18.2	127.5	65.	6.	-15.	21.6	123.1	85.	102.		24.2	120.5		284.	20.	0.0	0.0	ø.	-0.	0.
072318Z	18.8 126.1		18.8	126.3	75.			21.9	122.0	90.	91.		24.6	119.4		229.	30.	0.0	0.0	ø.	-0.	ø.
872488Z	19.3 124.7		19.3		125.	11.	-23.	21.8	118.9	115.	45.	20.	0.0	8.0	0.	-0.	30.	0.0	0.0		-0.	0.
072486Z						11.	J.										٥.			0.		
	19.8 123.2		19.9	123.2	130.	ъ.		22.8	118.2	105.	42.	25.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	~0.	0.
0724122			20.5	121.2	120.	34.	•	22.5	116.3	100.	135.	55.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.
072418 Z		110	21.1	120.2	115.	21.	5.	23.4	115.2	90.	144.	60.	0.0	0.0	ð.	-0.	0.	0.0	0.0	0.	-0.	0.
872588Z	22.4 119.4	95	22.3	119.3	95.	8.	0.	0.0	0.0	9.	-0.	₽.	0.0	0.6	0.	-0.	0.	0.0	0.0	8.	-0.	0.
8725862	23.5 118.2	88	23.5	118.1	85.	6.	5.	0.0	0.0	0.	-0.	0.	8.0	0.0	0.	-0.	Ø.	0.0	0.0	ø.	-0.	Θ.
072512Z	24.7 116.8	45	24.8	117.2	45.	23.	ø.	8.0	0.0	ø.	-0.	ē.	0.0	0.0	ø.	-0.	Ř.	0.0	0.0	e.	-0.	
										ä.					= -		ă.					
0725182	25.8 115.4	30	0.0	0.0	0.	-8.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-8.	ē.	0.0	0.0	ø.	-0.	ø.

	ALL	FURECAS	ITS .		TYPHOONS WHILE OVER 35 KTS						
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HF	₹ 48-HR	72-HR			
AVG FORECAST POSIT ERROR	12.	96.	226.	454.	12.	91.	226.	424.			
AVG RIGHT ANGLE ERROR	18.	63.	92.	102.	18.	38.	92.	73.			
AVG INTENSITY MAGNITUDE ERROR	6.	38.	36.	28.	6.	36.	38.	18.			
AVG INTENSITY BIAS	-4.	-9.	~22.	18.	-4.	-16.	-31.	3.			
NUMBER OF FORECASTS	14	11	7	3	13	10	6	2			

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1739. HM

AVERAGE SPEED OF TROPICAL CYCLONE IS 14. KNOTS

SUPER TYPHOON WA'NE
FIX POSITIONS FOR CYCLONE NO. 4

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
* 1	218888	12.5N 138.5E	PCN 6	T1.0/1.0	INIT DBS	PGTW
~ ż	211600	12.6N 135.8E	PCN 6	T1.5/1.5 /DØ.5/16HRS	11111 000	PGTW
7	211900	12.7N 135.1E	PCN 6	11.3/1.3 /De.3/16HR3		PGTW
	212848	13.0N 135.5E	PCN 5			PGTW
- :	220000	14.6N 135.2E	PCN 6	T2.0/2.0 /D1.0/08HRS	ULCC FIX	PGTU
6	228688	15.0N 133.3E	PCN 6	12.0/2.0 /DI.0/00HK3	ULCC FIX	PGTW
7	220900	14.9N 132.BE	PCN 6		ULCC FIX	PGTW
á	221200	15.5N 132.2E	PCN 6		OLCC FIX	PGTW
Š	221600	16.0N 132.0E	PCN 6	T3.5/3.5 /D2.0/16HRS		PGTW
10	221800	16.4N 131.5E	PCN 6	13.3/3.3 /DZ.0/ IONKS		PGTW
11	221855	16.1N 131.5E	PCN 5			PGTW
12	222100	16.3N 131.0E	PCN 6			PGTW
13	222258	16.6N 130.5E	PCN 3	T3.5/3.5		RODN
14	230000	16.9N 130.2E	PCN 4	10.5/5.5		PGTW
15	230300	17.1N 129.3E	PCN 4	T4.8/4.8 /D2.8/11HRS		PGTW
16	230600	17.4H 128.7E	PCH 4	1410/410/2210/111110		PGTW
17	238988	18.0H 128.2E	PCN 4			PGTU
18	230956	17.6N 127.8E	PCN 3			RODN
19	231137	18.2N 127.5E	PCN 3			RODN
28	231200	18.4N 127.5E	PCN 4			PGTW
21	231600	18.6N 126.6E	PCH 4	T4.5/4.5 /D1.8/13HRS		PGTW
22	231800	18.9N 126.1E	PCN 4			PGTW
23	231842	18.9N 126.1E	PCN 4			RODN
24	231843	19.8N 125.7E	PCN 4			PGTU
25	232100	19.0N 125.4E	PCN 2			PGTW
26	232139	19.1N 125.1E	PCN 1			PGTW
27	240000	19.3N 124.6E	PCN 2			PGTW
28	240017	19.2N 124.8E	PCN 1	T5.0/5.0 /D1.5/25HRS		RODN
29	248388	19.6N 123.BE	PCN 2	T6.5/6.5	INIT OBS	PGTW
30	240600	19.9N 123.8E	PCN 2			PGT⊎
31	240727	20.0N 122.6E	PCN 1	T5.5/5.5	INIT OBS	RODN
	5, _,				*****	

32	241819	20.3N 121.9E	PCN 3			PGTW
33	241116	20.0N 122.0E	PCN 6			RODN
34	241116	20.3N 122.0E	PCN 3			RPMK
35	241200	20.6N 121.7E	PCN 4			PGTЫ
36	241688	21.0N 120.8E	PCH 4	T6.0/6.0~/D1.5/13HRS		PGTW
37	241800	21.3N 120.4E	PCN 4			PGTW
38	242100	21.7N 119.9E	PCH 4			PGT₩
39	242356	22.2N 119.1E	PCH 5			RODN
40	250000	22.4N 119.2E	PCN 4			PGTW
41	250300	23.0N 118.7E	PCN 2	T4.0/5.0-/W2.5/11HRS		PGT⊎
42	250600	23.6N 118.2E	PCN 4			PGTW
43	250715	24.0N 118.1E	PCN 3	T4.5/5.5-/J1.0/24HRS		RODN
44	250715	23.7N 110.1E	PCN 1	T4.8/4.8-	INIT OBS	RPMK
45	250900	24.3N 117.8E	PCN 4			PGTW
46	251054	24.6N 117.0E	PCN 6			PGTW
47	251054	24.2N 116.8E	PCN 5			RPMK
48	251200	24.5N 116.5E	PCN 6		ULCC FIX	PGTW
49	251600	25.5N 115.8E	PCN 6	T2.8/3.6-	INIT OBS ULCC FIX	PGTW
50	261200	30.0N 112.0E	PCN 6			PGT⊎

AIRCRAFT FIXES

FIX NO.	TIME (Z)	F1X POSITION	FLT LVL	788118 HGT	DBS MSLP			-WND RNG			-LVL- ⁄BRG/				EYE SHAPE		ORIEN- /TATION	EY OUT/		MP (DP/		MSN NO.
1 2	220457 222053	14.5N 134.2E 16.3N 131.2E	1500FT 700MB	2985	1005 988	25	360	45	969 219		360 130	45 29	16 10		ELL IPTICAL ELL IPTICAL			+12		+23	28	1 2
3 4	222352 238558	16.0N 130.1E 17.3N 128.8E	700MB 700MB	2994 2939	989		090 030	9 15	130 150		020 020	20 20	15 10	_				+12 +15		+12		2 3
5 6	230040 231130	17.6N 128.3E 18.8N 127.7E	700MB 700MB	2891 2838	976	65	350	15	888 288		330 190	30 35	5 10	2 3	CIRCULAR	20		+15 +12	+15	+12		3 3
7	232 030 232325	19.0N 125.7E 19.2N 124.6E	700MB 700MB	2548 2412	921		140 080	120 7		112	130 000	28 20	12 8	5 2	ELL. IPTICAL		0 030	+12	+20	+11		5 5
9 18	241 058 241315	20.3N 122.0E 20.6N 121.5E	700MB 700MB	2419 2522	922				140 050	100		30 30	10 5	1	C IRCULAR C IRCULAR	12 50		+11				6
11	242032	21.8N 120.0E	700MB	2633	946				130	84	959	4	3	1	CIRCULAR	25			+22	+16		8

RADAR FIXES

	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB-CODE ASWAR TDDFF	COMMENTS	RADAR POSITION	SITE WMO NO.
1 2 3 4 5 6 7	248488 242188 258488 258488 258588	19.9N 123.5E 19.9N 123.4E 21.9N 119.8E 23.6N 118.5E 23.1N 118.2E 23.2N 118.4E 23.3N 118.1E	LAND LAND LAND LAND				10412 43412 10412 42700 6/// 53113 6/// 53022 6/// 53012 6/// 53409 6/// 53114	EYE DIA 28 KMS EYE DIA 28 KMS	16.3N 120.6E 16.3N 120.6E 25.1N 121.6E 22.6N 120.3E 23.6N 119.6E 22.6N 120.3E 23.6N 119.6E	98321 98321 46696 46744 46734 46734

SYNOPTIC FIXES

NO.	TIME (Z)	FIX POSITION	ESTIMATE	DATA (NM)		COMMENTS
1 2		24.4H 117.9E 24.8H 117.3E	968 958	020 820	WMO 59134 WMO 58927	

SUPER TYPHOON ABBY BEST TRACK DATA

	BEST	TRACK		u	ARN ING	FE	RORS		24	HOUR F		AST RRORS		40 1	OUR F		AST RRORS		72	HOUR		AST RRORS
MD/DA/HR	POSIT	WIN	n 0	DSIT	WIND		CHIM	Pf	DSIT	WIND		T WIND	Pf	DSIT	WIND		T WIND		POSIT	HIM		T WIND
888588Z	9.1 14			148.8	30.	8.			137.2		101.			133.5		139.			120.6			
989596Z		0.5 38			48.	27.		18.9	136.6		89.		12.4			132.			128.0			
888512Z	9.6 13			139.9	35.	e.	•		137.4		72.		11.9			153.		13.0				
080518Z	9.9 13				35.	8.		10.9	136.6	50.	91.		12.4			156.			129.			-55.
888688Z	10.2 13			138.8	48.	0.		12.2	135.7	60.	36.		14.2		80.	184.		16.				
888686Z		8.1 45			45.	19.		12.9	134.4	60.			14.8					16.1				-48
080612Z	11.8 13			137.5	55.	13.			134.5	75.	35.	-15.	16.7		90.	57.		18.			159.	-25.
080618Z	12.4 13			136.3	65.	В.		14.4	133.1	90.	43.	-25.	16.5			112.	-	18.			246.	5.
690796Z	12.8 13			135.8	78.	8.		14.8	132.6	98.	61.		16.2		115.			17.0		125.		10.
080706Z	13.6 13			134.9	88.	13.		15.3	131.7	95.	72.		16.9			130.		18.			219.	5.
8887122		3.9 90			90.	A.		16.5	138.6		88.		18.7			148.		21.			296.	5.
688718Z	15.0 13					8.			130.4		59.		19.7			171.		22.1				10.
0808002	15.8 13			132.8	125.	ø.		18.2	129.7		67.		20.3			198.		22.			352	0.
080806Z	16.3 13					19.		19.2	129.7		87.		21.5			216.		23.9				-20.
989912Z	17.1 13			131.9		В.			129.6		87.		22.8			254.		25.				
080018Z	17.4 13				140.	25.		20.7	129.2		127.					298.		26.				
0809002	17.8 13			130.9	135.	6.		19.7			64.		22.3			220.		24.				-25.
000906Z	18.1 13					0.		19.7	129.4		58.					189.		24.6				
8809122	18.7 13			130.2		ě.		20.5	128.8		102.		22.2			187.		24.			327.	-30.
080918Z	18.9 13			130.2		11.			129.0		90.		23.1			215.		25.				
681996Z	19.2 13					13.		28.4	129.1		91.			127.6	100.	173.	-20.	24.	126.6	90.	318.	-25.
0010062	19.5 13			130.0	115.	26.		21.3	128.6							210.		25.1	125.3	90.	375.	-20.
081012Z	19.9 13				115.	0.			130.4		18.		23.3			105.		25.			384.	-30.
881818Z	20.1 13					8.		21.3	138.3	100.	45.				85.	128.	-35.	25.6	127.6	75.	331.	-30.
081100Z	20.6 13					11.		22.5	129.9	90.	44.		23.9		80.	201.	-35.	25.4	4 126.5		374.	-35.
081106Z	21.2 13				128.	13.			129.5	105.			25.1		98.	272.		27.2			443.	-20.
8811122	21.6 13					6.		23.5	129.3					127.0		304.		27.7		75.	441.	-25.
6811182	22.0 13					11.	8.	24.0	129.8	105.	137.	-15.	25.6	126.6	90.	347.	-15.	27.5	124.4	75.	484.	-20.
681296Z	22.5 13					13.	ø.	24.4	129.4	100.	132.	-15.	25.9	127.3	98.	326.	-15.	27.7	125.3	80.	442.	-18.
881286Z	22.9 13	0.8 120	23.0	130.6	115.	13.	-5.	24.9	129.7	95.	136.	-15.	26.3	127.3	90.	337.	-10.	27.6	125.6	88.	486.	-5.
0812122	23.4 13	1.2 125	23.5	131.0	115.	13.	-10.	25.3	130.0	95.	141.	-15.	26.5	127.8	90.	312.	-10.	28.	1 125.7	80.	468.	-5.
081218Z	23.9 13					23.	-10.	25.5	130.0	95.	166.	-10.	26.0	127.8	90.	313.	-5.	29.3	125.7	. 88	487.	0.
08 1 3 0 8 Z	24.6 13	1.8 115	24.6	131.7	110.	5.	-5.	27.6	131.3	90.	123.	-15.	30.3	129.7	80.	231.	-10.	33.	1 128.5	70.	356.	-5.
001306Z	24.9 13					25.	-5.	28.1	131.2	90.	134.	-10.	30.7	129.6	80.	253.	-5.	33.3	128.5	65.	390.	-5.
0013122	25.4 13	2.6 110	25.5	132.4	100.	12.	-10.	27.8	132.4	90.	60.	-10.	30.4	131.4	80.	160.	-5.	33.	1 130.3	60.	313.	-10.
881318Z	26.1 13	3.0 105	26.2	132.9	190.	8.	-5.	29.8	132.7	90.	69.	-5.	31.7	132.1	75.	172.	-5.	34.4	4 131.3	55.	285.	-15.
681466Z	26.6 13				105.	Θ.			133.4	85.	85.	-5.	32.5	131.8	70.	188.	-5.	35.2	129.6	50.	371.	-10.
081406Z	27.2 13	3.5 100	27.3	133.4	100.	8.	0.	30.1	133.4	80.	70.	-5.	32.6	131.8	65.	209.	-5.	35.3	129.6	45.	487.	-10.
081412Z	27.6 13	3.5 100	27.6	133.5	95.	ø.	-5.	30.0	133.4	80.	56.	-5.	32.2	132.1	65.	225.	-5.	35.6	130.8	45.	462.	0.
981418Z	28.1 13	3.5 95	28.2	137.5	90.	6.	-5.	31.0	132.9	. 66	115.	В.	38.0	131.2	55.	378.	-15.	0.0	9.8	0.	-0.	0.
001500Z	28.5 13	3.6 90	28.5	133.5	90.	5.	Ð.	32.5	132.3	75.	166.	0.	41.8	132.7	45.	483.	-15.	0.6	9.6	0.	-0.	0.
991596Z	29.1 13	4.1 85	29.0	133.7	85.	22.	ø.	33.3	132.9	65.	172.	-5.	43.1	133.9	35.	518.	-20.	0.6	9.6	0.	-0.	0.
0015122	29.5 13	4.3 85	29.6	134.3	95.	6.	0.	35.7	132.9	55.	254.	-15.	42.6	134.6	35.	476.	-10.	0.6	9.6	0.	-0.	0.
0915192	30.0 13			134.7	80.	13.	ø.	36.3	132.8	45.	255.	-25.	0.0	0.0	ø.	-0.	Ø.	0.6	9.6	0.	-0.	9.
081600Z	31.1 13				75.	8.		38.0	135.7		218.		0.0	0.0	0.	-0.	ø.	0.6	9.6	0.	-0.	0.
00 1606Z	31.0 13		31.9		70.	6.	ø.	39.3	139.7	45.	263.	-10.	0.0	0.0	0.	-0.	ø.	0.6	0.0	ø.	-0.	0.
881612Z	32.7 13		32.6		70.	θ.		37.9	139.2		138.	-5.	0.0	0.0	0.	-0.	0.	0.6	0.6	ø.	-0.	ø.
001618Z	33.8 13		33.7	137.2	70.	12.	ø.	0.0	0.0	ø.	-0.	0.	0.0	0.0	Ð.	-0.	ø.	0.6	9.6	0.	-0.	0.
8817902	34.6 13			137.4	60.	5.	ø.	0.0	0.8	ø.	-0.	0.	0.0	0.0	0.	-0.	ø.	0.6	9.0	0.	-0.	8.
001706Z	35.1 13			138.2	55.	8.	ø.	0.0	0.0	ø.	-0.	0.	0.0	0.0	ø.	-0.	0.	0.6	9 .0	0.	-0.	0.
081712Z	35.6 13	9.4 45	36.0	140.1	48.	42.	-5.	0.0	0.0	ø.	-0.	Ø.	0.0	0.0	Ø.	-0.	0.	0.6	9.0	0.	-0.	0.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 3					
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72~HR		
AVG FORECAST POSIT ERROR	11.	184.	224.	340.	10.	194.	224.	340		
AVG RIGHT ANGLE ERROR	8.	84.	199.	307.	8.	84.	199.	307.		
AVG INTENSITY MAGNITUDE ERROR	3.	12.	17.	21.	3.	12.	17.	21.		
AVG INTENSITY BIAS	~1.	-11.	-17.	-19.	-2.	-11.	-17.	-19.		
NUMBER OF FORECASTS	51	47	43	39	48	47	43	39		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2831. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 7. KNOTS

SUPER TYPHOON ABBY FIX POSITIONS FOR CYCLONE NO. 5

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
1	012011	7.7N 146.7E	PCN 5	T0.0/0.0	INIT OBS	PGTW

2	829999	7 AN	146.8E	PCN 6			PGTW
3	628388		145.8E	PCN 6			PGTW
4	020600		145.7E	PCH 6			PGTW
5	020908		145.7E	PCN 6			PGTW
6	030300		145.4E	PCN 6	T1.0/1.0 /D1.0/30HRS		PGTW
7	030600		145.1E	PCN 6			PGTW
8	031200		144.5E	PCN 6		ULCC FIX	PGTW
9	032110	8.4N	143.7E	PCN 6			PGTW
10	040000	8.5N	143.1E	PCN 6			PGTW
11	040300	9.1N	143.2E	PCN 6	T2.0/2.0 /D1.0/24HRS		PGTW
12	040512		142.8E	PCN 6			PGTW
13	946869		142.5E	PCN 6		ULCC FIX	PGTW
14	841200		142.3E	PCN 6			PGTU
15	041756		141.7E	PCN 5			PGTW
16 17	042137		141.2E 148.7E	PCN 5			PGTW PGTW
10	050000 050300		148.3E	PCN 6 PCN 6	T3.0/3.0 /D1.0/24HRS		PGTW
19	050459		140.3E	PCN 6	T2.5/2.5	INIT OBS	RODN
20	050600		148.1E	PCN 6	12.5, 2.5	1111 005	PGTW
21	050900		140.5E	PCN 6			PGTW
22	050929		141.0E	PCH 5		ULCC FIX	PGTW
23	051017	9.3N	140.3E	PCN 6			₽GTW
24	051200	10.BN	140.0E	PCN 6			PGTW
25	051600	10.1N	140.1E	PCN 6	T3.0/3.0	INIT 085	PGTW
26	051744		140.2E	PCN 6			PGTW
27	052028		139.5E	PCN 3			PGTW
28	052257		139.8E	PCN 5	T2.5/2.5	INIT OBS	RPMK
29 3 0	052257 052257		139.3E 139.7E	PCN 5 PCN 5			PGTW RODN
31	968988		139.7E	PCN 4			PGTW
32	969399		138.2E	PCH 4	T3.0/3.0 /S0.0/24HRS		PGTW
33	060629		137.9E	PCN 5	1310/310 / 3310/24/83	ULCC FIX	PGTW
34	060629		137.8E	PCN 3	T3.8/3.8	INIT OBS	RPMK
35	060629		138.2E	PCN 5	T3.5/3.5 /D1.8/24HRS		RODN
36	060908	11.6N	137.4E	PCN 4	T3.0/3.0 /D0.5/10HRS		RPMK
37	060900		137.6E	PCN 6			PGTW
38	060955		137.9E	PCN 5			RODN
39	061200		137.1E	PCN 6	74 0 44 0 401 0 417400		PGTW
48 41	061600 061800		136.4E 136.1E	PCN 6 PCN 6	T4.0/4.0 /D1.0/13HRS		PGTW PGTW
42	962100		135.7E	PCN 2			PGTW
43	062235		135.6E	PCH 2			PGTW
44	062235		136.1E	PCN 3	T4.8/4.8 /D1.5/24HRS		RPMK
45	062235		136.1E	PCN 3			RODN
46	879898		135.4E	PCN 4			PGT⊎
47	070300		134.9E	PCN 2	T4.5/4.5 /D1.5/11HRS		PGTW
48	878617		134.5E	PCN 3			PGTU
49	070617		134.6E	PCN 3	T5.8/5.8 /D1.5/24HRS		RODN
50 51	070847		134.3E	PCH 4 PCH 3			PGTW RODN
52	070933 071200		133.9E 134.2E	PCN 2			PGTU
53	871688		133.BE	PCN 2			PGTW
54	871888		133.6E	PCN 2	T6.8/6.8 /D1.5/15HRS		PGTW
55	071901		133.4E	PCN 1			PGTW
56	072100	15.3N	133.0E	PCN 2			PGT⊎
57	872127	15.3N	133.2E	PCN 1		EYE DIA 6NM	PGTW
58	872213		133.0E	PCN 1			PGTW
59	072213		133.0E	PCH 1			RODN
60	868686 868388		133.0E 132.7E	PCH 2 PCH 2	TC 8 /C 8 / / / E / BOUIDE		PGTW PGTW
61 62	989699		132.7E	PCN 2	T6.0/6.0-/D1.5/09HRS		PGTW
63	888684		132.4E	PCH 1			PGTW
64	000004		132.1E	PCN 3	T5.0/5.0	INIT OBS	RKSO
65	696654		132.4E	PCN 1	T6.5/6.5 /D1.5/24HRS	EYE DIA 15NM	RODN
66	080900		132.2E	PCN 2		EYE DIA 18NM	PGTW
67	001007		132.2E	PCN 1		m. m. a.a	PGTU
68	98 1953		132.1E	PCN 1		EYE DIA 12NM	PGTU
69	881288		132.0E	PCN 2 PCN 2	77 8 4 8 401 8 400 Upc		PGTU
78 71	981699 981899		131.5E 131.3E	PCN 2	T7.0/7.0-/01.0/22HRS		PGTW PGTW
72	001000		131.4E	PCN 1			PGTU
73	082196		131.1E	PCN 2			PGTW
74	082106		130.BE	PCN 1	T7.8/7.0-/03.0/26HRS		RPMK
75	982186	17.5N	131.1E	PCN 1			RODH
76	682312	17.7N	131.1E	PCN 1		EYE DIA 20NM	RODN
77	662333		138.8E	PCN 1			PGTW
78	090000		131.0E	PCN 2		PUP PIA 18184	PGTW
79	090300		130.9E	PCN 2	T7.0/7.8-/01.0/11HRS	EYE DIA 18NM	PGTW
88	090552		130.5E	PCN 3	T7.0/7.0 /D2.0/24HRS		RKSO PCTU
81 82	090552 090552		130.7E 130.7E	PCN 1 PCN 1	T7.5/7.5-/01.8/24HRS	EYE DIA 18MM	PGTW RODN
83	898688		130.7E	PCN 2	17.3/1.3-/VI.0/24NK5	EYE DIA 20NM	PGTW
84	898988		130.7E	PCN 2		EYE DIA 20NM	PGTW
85	898946		130.7E	PCN 1		EYE DIA 18MM	PGTU
96	091031		130.5E	PCH 1		EYE DIA 18NM	PGTW
87	091200		130.5E	PCN 2			PGTW
88	091600		130.5E	PCN 2	T6.5/6.5 /UB.5/13HRS		PGTW
89	091800		130.4E	PCN 2			PGTW
98	092045		130.2E	PCN 1			PGTW
91	892311		130. IE	PCN 1	T5.5/6.5 /W1.5/26HRS		RPMK
92	89 2311	13.14	130.4E	PCH 1			RODN

93	100000	18.9N	130.4E	PCN 2			PGTW
94	100300		130.4E	PCN 2			PGTW
95 96	160533 160539		130.2E 130.3E	PCN 1 PCN 1	T7.0/7.5 /W0.5/24HRS T5.5/6.5 /W1.5/14HRS	EYE DIA 20NM	RODN PGTW
97	100539	19.4N	130.0€	PCN 1	T6.8/7.8 /W1.8/24HRS	ULCC FIX	RKSO
98 99	1 00900 101200		138.4E 138.4E	PCN 2 PCN 2			PGTU
188	101600		130.4E	PCN 2	T5.8/6.8 /W1.5/18HRS		PGT⊍ PGT⊍
161	161886		130.4E	PCN 2			PGTW
102 103	161824 162624		130.4E 130.3E	PCN 2 PCN 2			PGTW PGTW
184	102249	20.2N	130.4E	PCN 1			RODN
	110000 110300	28.3N	130.7E 130.8E	PCN 2 PCN 2	T4.5/5.5 /U1.0/11HRS		PGT⊎
	110527		131.0E	PCN 1	T6.8/6.8 /S8.8/23HRS		PGTW RKSO
	110527		130.6E	PCN 2		EYE DIA 30NM	PGT⊎
	110527 110904		130.7E	PCN 1 PCN 2	T5.5/7.0 /W1.5/24HRS	EYE DIA 30NM	RODN PGTW
111	111945	21.4N	130.0E	PCN 2		LIL SIN SOM	RPMK
		21.6N		PCN 1 PCN 2			RODN PGT⊍
	111600		130.6E	PCN 2	T4.5/5.5 /W0.5/13HRS	INIT OBS EYE DIA 30NM EYE DIA 30NM EYE DIA 30NM EYE DIA 40NM INIT OBS	PGTU
	111751		130.4E	PCN 2	** * * *		PGTW
116 117	112141 112144		131.1E 130.9E	PCN 1 PCN 1	T6.5/6.5	INIT OBS EYE DIA 30MM	RPMK PGTW
118	112227	22.3N	130.7E	PCN 1			PGTW
		22.4N 22.6N		PCN 2 PCN 2	T5.5/5.5-/01.0/11HRS	EYE DIA 38NM	PGTW
	120600		130.9E	PCN 2	13.3/3.3-/VI.6/IIAKS	EYE DIA 30NM EYE DIA 40NM	PGT⊎ PGTW
	120657		130.9E	PCN 1	T6.0/6.0	INIT OBS	RPMK
	12 0900 121 02 4	23.2N 23.1N		PCN 2 PCN 1			PGTW RKSD
125	121200	23.4N	131.1E	PCN 2			
	1218 00 121941	23.7N	131.1E 131.2E	PCN 2 PCN 1	T5.5/5.5-/S0.0/13HRS		PGTW RPMK
	122100		131.6E	PCN 2			PSTL
			131.6E	PCN 1		5.5 5.4 5.40	PGTL
	122123 122347	24.3N 24.5N	131.9E	PCN 1 PCN 1	T5.5/5.5	EYE DIA 24NM EYE DIA 30NM	RODN PGTW
132	130300	24.7N	131.9E	PCN 2		EYE DIA 30NM	PGTW
	130502 130900	24.9N	132.1E 132.3E	PCN 2 PCN 2	T5.5/5.5 /S0.0/11HRS		PGTW PGTW
135	131045	25.3N	132.8E	PCN 1			RPMK
	131200 131600		132.4E	PCN 2 PCN 2	TE E & E. & B 417UDC		PGTW
		26.0N 26.2N		PCN 2	T5.5/5.5-/S0.0/13HRS		PGTW PGTW
139	132100	26.7N	133.1E	PCN 2			PGTW
		26.4N 26.5N		PCN 1 PCN 1	T5.5/5.5-/S0.0/24HRS		RODN PGTW
142	140300	26.9N	133.5E	PCN 2			PGT⊎
	140600 140900	27.3N 27.5N	133.4E	PCN 2 PCN 2	T4.5/5.5-/W1.0/14HRS		PGTW PGTW
145	140942	27.3N	133.5E	PCN 1	T6.0/6.0 /S0.0/24HRS		RKSO
146 147	141200 141600	27.8N 28.1N	133.5E	PCN 2 PCN 2	TA E & E - 411 9 / 19490		PGTW
	141800		133.6E	PCN 2	T4.5/5.5-/U1.0/10HRS		PGTW PGTW
	142041		133.3E	PCN 3	74 5 45 5 44 5 47 1150		PGT⊎
150 151	142303 142393	28.3N	133.6E 133.5E	PCN 1 PCN 1-	T4.5/6.0-/W1.5/13HRS		RKSO PGTW
152	150000	28.6N	133.4E	PCN 2			PGT⊌
	150300 150600	28.9N 29.0N	133.6E	PCN 2 PCN 2			PGTW PGTW
155	150620	28.7N		PCN 3	T4.5/4.5-/S0.0/14HRS		PGTW
156	150620		133.7E 134.0E	PCN 1	T5.0/5.5 /W0.5/24HRS		RODN
157 158	150900 151001		133.7E	PCN 4 PCN 2			PGTW RKSD
159	151200	29.5N	134.2E	PCH 4	T4 E 44 E		PGTW
160 161	151600 151800		134.6E 134.8E	PCN 4 PCN 4	T4.5/4.5-/S0.0/10HRS		PGTW PGTW
162	151904	30.2N	135.0E	PCH 3			PGTW
163 164	152020 152241		134.8E 135.0E	PCN 1 PCN 3		EXP LLCC	PGTW RODN
165	152242	31.0N	135.2E	PCN 3			PGTW
166	160000		135.1E 135.6E	PCN 3			PGTW PCTU
167 168	16 0300 16 0600	31.4N		PCN 3 PCN 6			PGTW PGTW
169	160607		135.6E	PCN 6	T3.5/4.5-/W1.0/14HRS	10.00	PGTW
179 171	160900 161200		136.6E 136.5E	PCN 6 PCN 6		ULCC FIX	PGTW PGTW
172	161600	33.2N	136.9E	PCN 4	T3.0/4.0 /W0.5/10HRS		PGTW
173 174	161 900 1619 59		137.5E 137.4E	PCN 4 PCN 4			PGTW PGTW
175	162100	34.2N	137.2E	PCN 6			PGTW
176 177	170000	34.5N		PCN 4 PCN 4			PGTW
178	170300 170600		137.7E 138.1E	PCN 6	T2.5/3.5 /W1.0/14HRS	ULCC FIX	PGTW PGTW
179	170839	35.41	138.6E	PCN 6	•	ULCC FIX	PGTW
188 181	170918 171200		138.7E 139.3E	PCN 3 PCN 6		ULCC FIX ULCC FIX	RKSO PGTW
182	171600	35.5N	1 39.8 E	PCN 6		ULCC FIX	PGTW
103	171000	35.8N	140.5E	PCN 6		ULCC FIX	PGTW

184	172100	36.1N 141.2E	PCN 6		ULCC FIX	PGTW
185	172339	36.6N 142.7E	PCN 5	T2.0/2.0	INIT OBS	RKSO
186	180000	36.7N 141.7E	PCN &	T1.5/2.5 /W1.0/18HRS		PGT⊍
187	180300	37.8N 141.6E	PCH 6			₽GTW
188	188688	38.9N 141.5E	PCN 6			PGTW

AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	780MB HGT	OBS MSLP		-SFC- ⁄BRG				-LVL- ⁄BRG/		ACC NAV		EYE SHAPE			RIEN- ATION	EYE OUT/	TEMP IN/ D		MSN NO.
1 2	050034 058848	9.2N 140.7E 9.4N 140.4E	1500FT 700MB	3074	1004		340	15	979 989		340	19	5	3) 7 17	3 27	2
3	851147	9.6N 140.0E	1500FT	3074	998 1002	26	350	35	230		360 130	70 90	-	18					+11 +			3
4	852054	10.0N 139.2E	700MB	3043	997	70	340	60	060		340	120	10	10					+11 +			4
5	8 52336	10.2N 138.8E	700MB	3043	996		130	45	200		130	45	10	10					+12 +			4
6	060932	11.5N 137.8E	700MB	2980	330		248	70	260		200	38	15	3					712 7		•	5
7	061132	11.8N 137.5E	788MB	2965	985			, 0	150		050	25	10	2	CIRCULAR	30			+14 +	15		5
B	062020	12.6N 136.2E	780MB	2880		29	310	120	140		070	-8	7	7	01.1002.111							6
9	062314	12.8N 135.9E	700MB	2877	973		130	10	250		360	ī	5	5	CIRCULAR	20			+13 +2	22 +	5	6
19	070845	13.9N 134.5E	788M8	2747			240	20	160		060	12	10	2	CIRCULAR	20			+12 +	21 +	9	7
11	071141	14.2N 134.1E	788MB	2653	946				080	110	310	14	12	2	ELL IPTICAL	20	14	360	+19 +2	21 +1	0	7
12	072037	15.3N 133.1E	700MB	2309		50	220	48	140	120	949	10	5	1								8
13	072329	15.7N 132.8E	700MB	2304	908	120	240	6	200	110	110-	15	10	2	CIRCULAR	13			+15 +2	26 +	4	8
14	080035	16.7N 132.2E	700MB	2224	900	80	150	12	110	117	050	10	5	5					+12 +2	25 +1	8	10
15	681112	17.0N 132.IE	700MB	2208	901					105		10	10	5	CIRCULAR	20			+12 +2			10
16	002049	17.6N 131.2E	700MB	2094	888					113		26	10	1	CIRCULAR	15				53 +1		11
17	082342	17.8N 130.8E	700MB	2129	893		970	22		113		15	7	1	CIRCULAR	10			+13 +2			11
18	091034	18.8N 130.1E	700MB	2267	908	130	250	90	210			30	7	2	ELLIPTICAL	10	7	180	+15 +	18 +1	4	13
19	091337	18.8N 130.3E	700MB	2381						112		10									_	13
20	092120	19.0N 130.4E	790MB	2446	927		110	90		111		5	5	5					+14 +			14
21	092344	19.2N 130.3E	700MB	2453	927		050	10		197		. 5	5	5	CIRCULAR	26			+13 +	17 +1	6	14
22	100857	19.7N 130.4E	700MB	2415		70	110	80	310			15	7	4		_						17
23	101109	19.8N 130.5E	700MB	2434	926				350	93		8	10	3	CIRCULAR	7			+14 +		_	17
24	102109	20.3N 130.5E	700MB	2472	929		030	10		102		20	3	3	C 1 D C 1 # A D				+14 +			18
25 26	110011	20.6N 130.8E 21.5N 130.7E	700MB 700MB	2500 2401	934 921		340 310	10		106		33	4	3	CIRCULAR	30			+16 +1			18 19
27	111101	21.5N 130.7E	700MB	2369	917	90	310	6	210			25	5	5	CIRCUI OR	25			+14 +2			19
28	112332	22.5N 130.6E	780MB	2402	921	00	250	10		118		15 18	5 7	5	CIRCULAR CIRCULAR	25 25			+14 +2		4	20
29	120209	22.7N 130.7E	788MB	2393	321		969	15	050	108		13	7	1	CIRCULAR	25			+15 +2			20
30	121117	23.3N 131.1E	788M8	2345		80	000	13	320		230	15	15	2	CIRCULAR	25			+15 +2		7	22
31	121330	23.3N 131.2E	700MB	2357					120		030	20	10	2	CIRCULAR	23			* 1.5 .2		•	22
32	122248	24.4N 131.7E	700MB	2411	922	65	360	12	240		330	45	10	7	CIRCULAR	25			+15 +	7 +1	5	25
33	130102	24.7N 131.8E	700MB	2424	722		240	18	368		278	53	10	5	CIRCULAR	25			+16 +			25
34	131225	25.4N 132.7E	700MB	2471	928	-			330		250	50	10	2	CIRCULAR	20			+17 +			26
35	132046	26.3N 133.2E	700MB	2550	937	60	070	128	260		180	30	12	3	CIRCULAR	20			+16 +			27
36	141035	27.4N 133.5E	700MB	2593	942				238		120	30		10	CONCENTRIC		20		+17 +			28
37	141310	27.7N 133.5E	700MB	2609	944				100		120	120		10	CONCENTRIC				+15 +		_	28
38	142834	28.2N 133.5E	700MB	2681					320		230	90	15	4					+17 +			29
39	142319	28.4N 133.5E	700MB	2695	953	55	120	120	220	79	120	94	10	4					+17 +	18 +1	7	29
48	150930	29.2N 134.2E	700MB	2964		45	010	190	010	62	278	90	10	5	CIRCULAR	40						30
41	151049	29.4N 134.2E	700MB	2703					190	86	090	100	10	5					+15 +1	7		30
42	152032	30.8N 134.8E	700MB	2772		60	290	120	100	67	030	118	10	5					+16 +	17		31
43	152352	31.0N 135.0E	700MB	2795	965			155	230			120	5	4					+15 +1			31
44	160057	32.3N 136.1E	700MB	2828	969	35	250	48	150			174	5	8						6 +1		32
45	161147	32.7N 136.4E	700MB	2840					230			144	5	1						7 +1	-	32
46	162050	34.3N 137.2E	700MB	2881			150	90	220		150	77	5	6	CIRCULAR	28			+17 +1			33
47	162254	34.5N 137.2E	700MB	2016		50	150	90	220	61	160	110	2	3	CIRCULAR	10			+14 +	6 +1	5	33

RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB-CODE ASWAR TDDFF	CONTENTS	RADAR POSITION	SITE WMO NO.
1	160000	31.3N 135.3E	LAND				5//// /////		33.3N 134.2E	47899
2	160100	31.4N 135.5E	LAND				5/// 50614		33.3N 134.2E	47899
3	160300	31.8N 136.8E	LAND				5///: /////		33.3N 134.2E	47899
4	160400	31.7N 135.8E	LAND				5///. /////		33.3N 134.2E	47899
5	160500	31.8N 135.8E	LAND				5//// 50105		33.3N 134.2E	47899
6	160600	31.8N 135.8E	LAND				5/// 50105		33.3N 134.2E	47899
7	161400	33.2N 136.8E	LAND				5//// 50322		33.3N 134.2E	47899
8	161400	33.1N 136.9E	LAND				6//// 5////		34.6N 135.7E	47773
9	161500	33.4N 136.9E	LAND				5//// 50216		33.3N 134.2E	47899
10	161500	33.3N 137.0E	LAND				6//// 5////		34.6N 135.7E	47773
11	161 900	34.8N 137.2E					203/2 50511		35.2N 137.0E	47636
12	161900	33.9N 137.1E					5///4 53511		35.3N 130.7E	47639
13	161 900	34.3N 137.1E					65/// 53611		34.6N 135.7E	47773
14	1622 00	34.4H 137.3E					23711 50408		35.2N 137.0E	47636
15	1622 00	34.4N 137.1E					5///2 53608		35.3N 138.7E	47639
16	1622 00	34.4H 137.4E					65/// 5////		34.6N 135.7E	47773
17	162300	34.5H 137.2E					5///2 50211		35.3N 130.7E	47639
19	162300	34.5H 137.5E					55/// 50300		34.6N 135.7E	47773
19	162300	34.5N 137.3E					23711 53605		35.2N 137.0E	47636
20	178888	34.5H 137.2E					52//3 50400		35.3N 130.7E	47639
21	170000	34.6N 137.5E	LAND				55/// 53600		34.6N 135.7E	47773

22	178188	34.5N 137.3E	LAND				52/13 50000	35.3N 130.7E	47639
								34.6N 135.7E	47773
23	170100	34.9N 137.5E	LAND				55/// 53511		
24	170200	34.8N 137.3E	LAND				51/13 50111	35.3N 130.7E	47639
25	178488	34.9N 137.5E	LAND				52/13 50411	35.3N 138.7E	47639
26	178588	34.9N 138.0E	LAND				353// /////	35.2N 137.0E	47636
27	170500	34.9N 137.9E	LAND				52/43 50919	35.3N 138.7E	47639
28	179500	34.8N 138.1E	LAND				55/// 5////	34.6N 135.7E	47773
29	178688	35.0N 130.3E	LAND				5//// /////	35.2N 137.0E	47636
36	178688	35.0N 138.2E	LAND				51//3 50814	35.3N 130.7E	47639
31	178688	35.0N 138.3E	LAND				55//1 50611	34.6N 135.7E	47773
32	170700	35.1N 138.5E	LAND				5//// /////	35.2N 137.0E	47636
33	170700	35.1N 138.4E	LAND				21//3 50511	35.3N 13B.7E	47639
34	179799	35.1N 138.4E	LAND				55//1 50611	34.6N 135.7E	47773
35	170800	35.2N 138.6E	LAND				7//// /////	35.2N 137.0E	47636
36	170800	35.2N 138.6E	LAND				5///3 50716	35.3N 138.7E	47639
37	170800	35.1N 138.6E	LAND				55//1 50611	34.6N 135.7E	47773
38	170900	35.2N 138.7E	LAND				4///3 50705	35.3N 138.7E	47639
39	170945	35.5N 139.2E	LAND	GOOD	CIRCULAR	60		35.7N 139.3E	47642

SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)		CONTENTS
1	170000	34.6N 137.4E	969	838	WMD 4765	54
2	170900	35.4N 138.3E	050	018	UMO 4763	38
3	171200	35.7N 139.5E	945	020	UMO 4762	26
4	171500	36.4N 139.6E	949	020	W10 4762	24
5	171800	36.6N 140.3E	949	025	WMO 4762	29
6	180000	37.5N 140.6E	035	030	WMO 4759	95

TROPICAL STORM BEN BEST TRACK DATA

BEST TRACK	WARN ING	24	HOUR FORECAST	48 HOUR FORECAST	72 HOUR FORECAST
		ERRORS	ERRORS	ERRORS	ERRORS
MO/DA/HR POSIT WIND	POSIT WIND	DST WIND POSIT	WIND DST WINI	ONIW TER DIND POSIT WIND	POSIT WIND DST WIND
081200Z 24.3 145.1 30 (0.0 0.0 0.	-0. 0. 0.0 0.0	0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
081206Z 24.9 145.8 35 (0.0 0.0 0.	-0. 0. 0.0 0.0	0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0812122 25.7 146.1 40 20	.0 145.6 40.	32. 0. 29.9 144.	1 40. 7210.	32.6 143.2 35. 3210.	0.0 0.0 08. 0.
0812182 27.0 146.0 40 20	6.6 146.2 40.	26. 0. 30.0 145.0	6 40. 1010.	32.7 144.7 35. 17710.	0.0 0.0 00. 0.
081300Z 28.0 145.6 40 20	3.2 145.4 40.	16. 0. 31.6 144.3	3 40. 6210.	35.0 143.8 35. 23310.	0.0 0.0 00. 8.
0813062 28.7 145.4 45 20	3.5 145.3 40.	135. 30.7 144.	7 40. 915.	33.2 144.0 35. 405. 5.	0.0 0.0 00. 0.
081312Z 29.3 145.3 50 29	9.1 145.3 50.	12. 0. 32.0 144.0	0 40. 73. - 5.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0813182 30.0 145.4 50 2	9.9 145.2 45.	125. 32.4 143.3	2 40. 1 30 5.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
081400Z 30.9 145.2 50 30	3.8 145.1 45.	85. 33.9 143.3	3 48. 2125.	0.0 0.0 00. 0.	6.0 6.0 00. 0.
081406Z 32.2 144.5 45 3	1.8 144.8 45.	28. 0. 35.2 143.0	0 40.333. 10.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
081412Z 33.1 143.4 45 3	2.9 143.4 45.	12. 0. 0.0 0.0	0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
081418Z 34.1 141.6 45 3	1.1 141.3 55.	15. 10. 0.0 0.0	9 99. 9.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
081500Z 34.6 139.1 45 34	4.3 139.3 50.	21. 5. 0.0 0.0	0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
081506Z 35.2 136.2 30 3	5.3 136.4 35.	11. 5. 0.0 0.0	00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.

	ALL	FORECAS	TS		TYPHO	E OVER	35 KTS	
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	17.	123.	212.	ð.	0.	ø.	0.	0.
AVG RIGHT ANGLE ERROR	12.	41.	46.	0.	0.	Ø.	0.	0.
AVG INTENSITY MAGNITUDE ERROR	3.	8.	9.	0.	Ð.	0.	0.	0.
AVG INTENSITY BIAS	0.	-5.	-6.	0.	8.	0.	0.	ð.
NUMBER OF FORECASTS	12	8	4	0	0	8	0	0

DISTANCE TRAVELED BY TROPICAL CYCLONE IS , 968. NM
AVERAGE SPEED OF TROPICAL CYCLONE IS 12. KNOTS

TROPICAL STORM BEN
FIX POSITIONS FOR CYCLONE NO. 7

SATELLITE FIXES

FIX	TIME	F1X				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
1	112227	24.8N 145.3E	PCN 5	T2.0/2.0	INIT OBS	PGTW
2	120000	24.4N 144.7E	PCN 6			PGTW
3	120300	24.5N 145.3E	PCN 4			PGTW
4	120600	24.7N 145.9E	PCN 4			PGT₩
5	121290	25.0N 146.7E	PCN 6			PGTW
6	121800	26.7N 145.5E	PCN 6	T2.5/2.5	INIT OBS	PGTW
7	121942	27.3N 145.4E	PCN 6			PGTW
8	122100	28.1N 145.3E	PCN 6			PGTW
9	122206	28.3N 145.4E	PCH 5			PGTW
10	130000	28.0N 145.7E	PCN 6			PGT⊎
11	130502	28.3N 145.4E	PCN 4	T3.8/3.8-/D8.5/11HRS		PGTW
12	130900	28.7N 145.5E	PCN 4		EXP LLCC	PGTW
13	131200	29.8N 145.4E	PCN 6			PGTW
14	131600	29.5N 145.4E	PCN 6	T2.5/2.5-/S0.0/11HRS		PGTW
15	131900	29.9N 145.2E	PCH 6			PGTW
16	132144	38.6N 145.1E	PCN 6			₽GTW
17	140000	30.8N 145.2E	PCN 4			PG™
18	140450	31.8N 144.7E	PCN 4	T2.0/3.0 /W1.0/13HRS		PGT⊎
19	140900	32.5N 144.2E	PCN 6			PGT⊎
28	140942	32.6N 144.0E	PCN 3	T1.5/1.5	INIT OBS	RODH
21	141200	33.1N 143.3E	PCN 6		EXP LLCC	PGTW
22	141600	33.5N 142.3E	PCN 6	T2.8/2.5 /W0.5/11HRS	EXP LLCC	PGTW
23	141888	34.1N 141.2E	PCN 6			PGT⊌
24	142641	34.4H 140.1E	PCH 5		EXP LLCC	PGTW
25	142303	34.3N 139.7E	PCN 3			PGTW
26	150000	34.5N 139.6E	PCN 4		EXP LLCC	PGTW
27	150600	35.0N 136.5E	PCN 6	T1.0/2.0-/W1.0/14HRS		PGT⊍

AIRCRAFT FIXES

FIX HO.	TIME (Z)	FIX POSITION	FLT LVL			MAX-FLT-LVL-UND ACCRY DIR/VEL/BRG/RNG NAV/MET	EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
	126742	25 2N 146 86	150057	997	AB 1AB AS	200 AD 1AD 67 7 7			29	1

3 4 5 6 7 8 9	122312 130842 131134 132357 140254 140833 141182 142113	27.9N 145.7E 28.9N 145.5E 29.9N 145.2E 39.2N 145.2E 30.9N 145.1E 31.3N 144.9E 32.3N 144.2E 32.6N 143.5E 34.2N 140.2E 34.2N 139.4E	1500FT 700MB	2976 2994 2989 3017 3014 2992	994 994 996	35 11	9 10 9 40 9 25 9 36 9 10	060 060 120 230 160 190 170 120	35 120 40 300 34 270 55 040 47 130 62 070 41 110 51 090 52 040 34 130	10 25 21 13 26 30 25 65	18 5 6 19 19 2	5 5 1 2 10	CIRCULAR	28	+25 +26 +28 29 +12 +14 +11 +12 +14 +11 +14 +17 +18 +18 +18 +6 +19 +17 +28 +12 +12 +16 +12 +14 +18 +18	2 3 3 4 4 5 6 6	
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RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB-CODE ASUAR TODFF	CONTENTS	RADAR POSITION	SITE WHO NO.
1 2 3 4 5 6	141790 141900 141900 142000	33.9N 142.2E 33.9N 141.9E 34.1N 141.5E 33.9N 141.0E 34.1N 140.8E 34.5N 138.2E	LAND LAND LAND				5//// ///// 4/// 73019 5//// 73021 5//// 72719 6//// 72818 5//// /////		35.3N 138.7E 35.3N 138.7E 35.3N 138.7E 35.3N 138.7E 35.3N 138.7E 35.2N 137.0E	47639 47639 47639 47639 47639 47636

SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)		COMMENTS
1 2		35.3N 136.4E 37.0N 136.9E	035 030	822 865	WMO 47636, WMO 47600	47899.47600

TROPICAL DEPRESSION 06 BEST TRACK DATA

	BEST TRAC	:K		WA	RNING				24 F	OUR FO	DRECAS	ST		48 H	OUR FO	DRECA			72 H	IDUR FO		
						ER	RORS				ER	RORS				ER	RORS				ERF	RORS
MD/DA/HR	POSIT	WIND	P	DSIT	MIND	DST	MIND	POS	TIE	WIND	DST	MIND	P09	TIE	WIND	DST	MIND	POS	SIT	WIND	DST	MIND
080800Z	16.0 111.3	20	8.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
080806Z	15.1 112.2	20	0.0	0.0	e.	-0.	0.	0.0	0.0	é.	-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	0.
080812Z	14.7 113.1	20	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ø.	-0.	0.
080818Z	14.6 114.0	20	8.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-8.	Ð.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
080900Z	14.4 114.6	20	0.0	0.0	ø.	-0.	ø.	0.0	0.0	Ð.	-0.	8.	0.0	0.0	ø.	-Ø.	ø.	0.0	0.0	Ø.	-0.	0.
989996Z	14.1 115.0	20	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.
0809122	14.2 115.4	20	0.0	0.0	ē.	-0.	ø.	0.0	0.0	Ñ.	-0.	ø.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.
080918Z	14.5 115.5	20	0.0	0.0	ø.	-0.	ø.	0.0	0.0	Ñ.	-0.	ø.	0.0	0.0	ø.	-0.	0.	0.0	0.0	ø.	-0.	0.
081000Z	14.9 115.4	25	0.0	0.0	ě.	-0.	ø.	0.0	0.0	Ñ.	-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	0.
081006Z	15.1 115.3	25	0.0	0.0	ě.	-0.	a.	0.0	0.0	Ñ.	-0.	ø.	0.0	0.0	ø.	-0.	ē.	0.0	0.0	0.	-0.	0.
0810122	15.4 115.3	25	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ē.	0.0	0.0	ē.	-0.	0.
081018Z	15.8 115.4	25	0.0	0.0	ě.	-0.	Ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0		-0.	ø.
0811002	16.0 115.5	25	0.0	0.0	Đ.	-0.	ø.	0.0	0.0		-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0		-0.	0.
081106Z	16.4 115.8	25	0.0	0.0	Ð.	-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	P.	0.0	0.0		-0.	ø.
							•										ø.					
										7.							a.					
																	Ñ.					ø.
																	Ñ.			ø.		ø.
				116.2													Ñ.			ø.		ø.
										= -							я.					
						11											я.			Ñ.		
0811112Z 0811118Z 081200Z 081206Z 081206Z 081212Z 081212Z 081300Z	16.7 116.1 17.0 116.3 17.3 116.5 17.6 116.7 17.8 116.8 18.0 116.9	25 25 30 30 30 30	0.0 0.0 0.0 0.0	0.0 0.0 0.0	0. 0. 0. 30. 30.	-0. -0. -0. -0. 36. 42.	0. 0. 0. 0.	9.0 9.0 9.0 9.0 9.0	0.0 0.0 0.0 0.0 0.0	0. 0. 0. 0.	-0. -0. -0. -0.	0. 0. 0. 0.	0.0 0.0 0.0 0.0 0.0	9.0 0.0 0.0 0.0 0.0		-8. -0. -0. -0. -0.	0. 0. 0. 0.	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0	0. 0. 0.	-0. -0. -0. -0. -0.	0. 0. 0.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS						
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR			
AVG FORECAST POSIT ERROR	30.	Ø.	0.	0.	0.	0.	ø.	0.			
AVG RIGHT ANGLE ERROR	25.	0.	0.	Θ.	0.	0.	ø.	0.			
AVG INTENSITY MAGNITUDE ERROR	0.	0.	0.	0.	0.	0.	0.	8.			
AVG INTENSITY BIAS	0.	0.	0.	0.	0.	8.	0.	0.			
NUMBER OF FORECASTS	3	0	0	0	8	9	0	8			

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 555. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

5. KNOTS

TROPICAL DEPRESSION TD06W-A FIX POSITIONS FOR CYCLONE NO. 6

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
1	898888	14.5N 114.5E	PCN 6	T1.0/1.0	INIT OBS	PGTW
2	990300	14.4H 114.8E	PCN 6			PGTW
3	898688	14.1H 114.9E	PCN 6			PGTW
4	898 734	14.1N 115.5E	PCN 3	T1.5/1.5		RPMK
5	090739	14.6N 114.8E	PCN 5	T1.6/1.8	INIT OBS	RODN
6	898988	14.1N 115.2E	PCN 6			PGTW
7	89 1127	14.1H 115.3E	PCN 6			RPMK
8	0 916 00	14.4H 115.1E	PCN 6	T1.0/1.0-/D1.0/13HRS		PGTW
9	891866	14.6H 115.1E	PCN 6			PGTW
10	692018	14.3H 115.9E	PCN 5			RPMK
11	092100	14.6N 115.2E	PCN 6			PGTW
12	092226	15.1H 114.8E	PCH 5	T0.5/1.5 /W1.8/15HRS		RPMK
13	0 92226	14.8H 115.1E	PCN 5			RODH
14	100000	14.8H 115.8E	PCN 6			PGTW
15	100052	15.0N 115.6E	PCN 5	T1.0/1.5 /W0.5/17HRS		RPMK
16	106306	15.2N 115.0E	PCN 6			PGTW
17	100721	14.9N 115.5E	PCN 5	T1.5/1.5 /S0.0/24HRS		RPMK
* 18	101106	15.3N 115.5E	PCN 5	T1.5/1.5 /S6.8/24HRS		RPMK
19	101200	15.6N 116.1E	PCN 6		ULCC FIX	PGTW
26	101600	15.6N 115.5E	PCN 6		ULCC FIX	PGTW
* 21	162666	15.9N 116.6E	PCN 5	T1.5/1.5 /S0.8/24HRS		RPMK
22	102205	16.0N 116.2E	PCN 5	T1.5/1.5 /D1.0/24HRS		RPMK
23	110000	16.7N 115.7E	PCN 6			PGTW
* 24	110030	15.6N 115.1E	PCN 5	T1.0/1.0	INIT OBS	RODN
25	120300	17.6N 116.6E	PCN 4	T1.0/1.0	INIT OBS EXP LLCC	PGTU
26	120600	17.4N 116.6E	PCN 4		EXP LLCC	PGTU
27	120657	17.7N 116.4E	PCN 3	T2.5/2.5	INIT OBS	RPHK
28	120900	17.6N 116.2E	PCN 6			PGTW
29	121200	17.5H 116.3E	PCN 6			PGTW
30	121886	17.7N 115.9E	PCN 6	T2.5/2.5	INIT OBS	PGTW
* 31	122100	17.7H 115.8E	PCN 6			PGTW

* 32 122384 17.9N 115.8E PCN 5 T2.5/2.5 /S0.8/24HRS

RPMK PGTW

AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB OBS HGT MSLP		D MAX-FLT-LVL-UND ACCRY G DIR/VEL/BRG/RNG NAV/MET	EYE EYE ORIEN- SHAPE DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
1	181821	15.0N 115.4E	1580FT	1999		7 48		+25 +22 27	4
2		15.8N 115.2E		1002	15 210 45	• •		+26 +24 31	5
3	120247	17.5N 116.6E	1500FT	999	40 210 70			+27 +26 +23	6
4	130008	18.7N 116.9E	1500FT	1905	25 120 90	9 060 15 120 90 5 15		+25 +24	7
5	130303	18.5N 117.2E	1500FT	1005	20 230 60	270 24 230 60 5 20		+26 +25 +24	7

TROPICAL STORM CARMEN BEST TRACK DATA

08131: 08140: 08140: 08140: 08141: 08141:	AHR PO 52 19.2 22 19.4 82 19.6 82 19.8 52 19.9 82 20.2 82 21.0	119.4 30 8 120.2 30 19	POSIT .0 0.0 .7 121.3 .0 120.8 .0 121.6 .1 122.4 .8 124.2 .0 126.0 .1 129.2	WIND DS 00. 30. 65. 40. 24. 40. 6. 45. 13. 45. 16. 30. 8.	RRORS F WIND POSIT 8. 0.0 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	WIND DST WIND 8 00. 0. 5 25. 12120. 2 45. 164. 5. 2 45. 238. 15. 8 45. 288. 15. 9 00. 0. 9 00. 0.	0.0 0.0 0.	D DST WIND POS -0. 0. 0.0 -0. 0. 0.0 -0. 0. 0.0 -0. 0. 0.0 -0. 0. 0.0 -0. 0. 0.0 -0. 0. 0.0		ERRORS ST WIND . 0. . 0. . 0. . 0. . 0.
AVG R AVG II AVG II NUMBEI	IGHT ANG NTENSITY NTENSITY R OF FOR NCE TRAV		ROR	20. 199. 12. 105. 2. 14. 2. 4. 8 4	ASTS R 48-HR 72-HR B.	WRNG	0. 0.			
						STORM CARMEN S FOR CYCLONE NO.	6			
					SATE	LLITE FIXES				
FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK (CODE	COPPE	NTS	SITE		
2 3 4 5 6 7 8 9 18 11 12 13 14	130900 131200 131600 131800 132100 132325 140300 140600 140632 140900 141600 141600	19.4H 128.3E 19.4H 120.5E 19.7H 120.6E 19.8H 120.7E 20.0H 121.0E 20.3H 121.2E 19.4H 121.5E 19.8H 121.5E 20.0H 122.7E 20.0H 123.1E 20.3H 123.1E 20.3H 123.4 20.3H 124.4E 20.4H 124.6E	PCN 5 PCN 6 PCN 6 PCN 6 PCN 6 PCN 5 PCN 6 PCN 6 PCN 6 PCN 6 PCN 6	T1.5/1.5	5 /U1.5/13HRS 5 /U1.8/10HRS 5 /S0.8/14HRS 5 /S0.8/10HRS	ULCC FIX		PGTU PGTU PGTU PGTU PGTU PGTU PGTU PGTU		
		21.0N 127.5E 20.4N 129.2E	PCN 6 PCN 5	T1.5/1.5	5	INIT OBS		PGTW RPHK		
					AIRC	RAFT FIXES				
FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	790M9 06 HGT MSI		MAX-FLT-LVL-UNI DIR/VEL/BRG/RNG			EYE TEMP	
	140328 140633 141107 141426	19.8H 128.8E 19.9H 122.1E 19.8H 122.8E 19.8H 124.2E 28.8H 125.2E 28.7H 127.6E	700HB 700HB 700HB 700HB 700HB 700HB	3052 99 3058	37 36 35 310 36 38 198 46 32 38 248 98 35 128 98	218 40 090 68 340 23 280 68	10 0 12 7 5 5 5 5		+12 +12 +13 +15 +16 +13 +16	9 10 10 11 11
					RADA	R FIXES				
FIX NO.	TIME (Z)	FIX POSITION	RADAR I		EYE EYE HAPE DIAM	RADOB-CODE ASWAR TDDFF	CONTEN	\$	RADAR POSITION	SITE WMD NO.
1 2 3	132000 132100 132130	19.6N 128.7E 19.7N 121.1E 19.6N 121.8E	LAND			10011 40401 EY	E 100 PCT CIR E 100 PCT CIR E 100 PCT CIR		18.3N 121.6E 18.3N 121.6E 18.3N 121.6E	98231 98231 98231

4	132200	19.7N 121.3E	LAND	19911 40401	EYE 100 PCT CIR	18.3N 121.6E 982	231
5	132300	19.7N 121.3E	LAND	10011 40401	EYE 100 PCT CIR	10.3N 121.6E 982	
		19.8N 121.4E		18781 48482	EYE 90 PCT CIR	18.3N 121.6E 982	
		19.8N 121.5E		18651 48681	EYE 100 PCT CIR	18.3N 121.6E 982	
		28.8N 124.2E		10341 70927		16.3N 128.6E 983	321
9	141500	20.0N 124.3E	LAND	4///1 50903		18.3N 121.6E 982	231

TROPICAL STORM DOM BEST TRACK DATA

	BEST TRAC	ж	4	arn i NG	==	RORS		24	HOUR I		AST RRORS		48 H	IOUR F		AST RRORS		72 H	HOUR F	FORECA	ST RORS
MD/DA/HR	POSIT	MIND	POSIT	MIND	DST		PO	SIT	MIN			- 101	OSIT	WIN				DSIT	WINI		MIND
881786Z	15.2 140.1		0 0.0	Ð.	-8.	B.	8.6	0.6		-B.	Ø.	0.0	0.0	e.	-0.	2.	0.0	0.0	0.	-Ø.	0.
881712Z	15.4 139.0		8 8.8	٥.	-B.	8.	0.0	0.0		-0.	ø.	0.0	0.0	٥.	-B.	8.	0.0	8.8	ø.	-0.	8.
881718Z	15.4 138.1		0 0.0	Ð.	-0.	Ð.	0.0	8.6	•	-0. -0.	Ð.	8.0	0.0	0.	-8.	0.	0.0	8.8	0.	-0.	e.
88 1888Z	15.2 137.2		0 0.0	ø.	-Ø.	8.	0.0	0.6	0.	-0. -8.	8.	8.0	0.0	8.	-0. -0.	8.	0.0	9.0	9.	-0. -8.	ø.
081806Z	15.0 136.3		9 8.8	Ð.	-0.	Ø.	8.8	0.0		-0. -0.	8.	0.0	0.0	0.	-0.	Ø.	0.0	6.0	ø.	-0.	ð.
6919122	15.2 135.3		0.0	0.	-0.	ð.	0.0	0.0	• • •	-0.	8.	0.0	0.6	0.	-0. -0.	0.	0.0	0.0	0.	-0.	0.
881818Z	15.6 134.5		8 8.8	0.	-0.	ø.	0.0		9.	-0.	8.		0.0	Ø.	-0.		8.8	0.0	0.	-0.	0.
881988Z	15.9 133.8		0.0	0.	-0. -0.	8.	0.0	0.0	9.	-0. -0.	Ø.	9.0	0.0	Ø.	-0. -0.	0. 0.	0.6	9.0	0.	-0. -0.	0.
88 1986Z	16.1 133.2		3 133.2	35.	12.			131.3	45.	99.		20.9	130.7	60.	281.		23.9	130.7	75.	442.	45.
881912Z	16.3 132.8		5 132.7	48.	13.		18.6	131.2		189.		20.9	130.7	65.	314.		23.9 23.0	130.7	90.	520.	45.
881918Z	16.5 132.4		9 132.7	40.	25.		19.6	131.2	68.	149.		21.6	130.7	70.	350.	35. 48.	23.0 23.4	130.7	85.	600.	48.
082000Z	16.9 132.2		8 132.2	45.	6.		18.0	130.9		230.		19.9	130.7	70.	447.		23.4 22.0	130.7	80.	693.	30.
882086Z	17.4 132.5		6 132.2	45. 45.	21.		22.8	134.8		128.		23.8	137.4	78.	80.		25.5	148.2	80.	157.	30.
882812Z	18.0 133.0		B 132.2	45. 48.	17.		19.9	135.1	50.	83.		21.9		55.	171.		23.5	148.8	65.	198.	20.
882018Z	10.0 133.0		6 133.4	40.	18.		20.6	136.6	50. 50.	7B.		22.4		55.	193.	10.	24.1	141.6	65.	155.	25.
882188Z	19.3 134.7		4 134.8	25.	8.			138.6		78. 58.		24.6	142.2	20.	28.	-30.	0.0	0.0	03.	~0.	23. 0.
0021002 0021062	20.0 135.6	35 20.	0 135.8	25. 25.	11.		22.6	139.2	25.	45.	-5. -5.	0.0	0.0	20.	-A.	-30. 0.	0.0	0.0	0.	~0. ~0.	Ø.
BB2112Z	28.7 136.3		7 136.6	25.	17.	-5.	0.0	0.0		45. -0.	-3. Ø.	9.0	0.0	0.	-0.	0.	0.0	0.0	ø.	~0.	0.
082118Z	21.4 137.1		0 0.0	25.	-Ø.	-J.	0.0	0.0		-0.	ø.	9.0	0.0	8.	-0.	ø.	9.0	0.0	0.	~0.	0.
082200Z	22.2 137.9		8 8.8	a.	-0.	8.	0.0	0.0	9.	-0. -0.	0.		8.0	0.	-0.	ø. Ø.	0.0	0.0	0.	-0. -0.	0.
8822 8 6Z	23.2 138.7		0.0	8.	-0. -0.	8.	0.0	0.6		-0. -0.	0.	9.0	0.0	ø.	-0.	ø.	0.0	9.0	0.	-0.	0.
692212Z	23.8 148.1		9 0.0	Ð.	-8.	Ð.	0.0	0.6		-0. -0.	0.	0.0	0.0	Ð.	-0. -0.	Ø.	0.0	0.0	0.	~0.	ø.
082218Z	24.2 141.6	35 D.	0.0	Ð.	-0.	Ð.	0.0	8.6		-0. -0.	Ð.	8.8	0.0	0.	-0.	8.	0.0	0.0	0.	~0. ~0.	Ø.
0022102 002300Z	24.9 142.6		9 142.7	45.	-e. 5.		29.8	147.5		290.		31.7	153.7	35.	623.	-15.	0.0	0.0	0.	-0. -0.	Ø.
002306Z	25.4 143.1		6 143.7	45. 50.	35.		29.0 28.7	148.6	40.	270.		30.3	154.1	30.	625.	-15.	0.0	0.0	0.	-0.	ø.
0023002 002312Z	25.8 143.5	45 25.		45.	17.		20.7 27.9	145.6		127.		29.8	150.0	25.	446.	-15.	0.0	0.0	Ø.	-0. -0.	Ø.
682318Z	25.5 144.0		9 143.9	45.	25.		27.4	144.6		81.		29.8	147.8	25. 25.	341.	-10.	0.0	0.0	0.	-0.	e.
682466Z	25.1 144.3		1 144.2	45. 35.	23. 5.		25.9	141.6		93.	~20.	9.0	0.8	25. R.	-0.		0.0	0.0	0.	-0.	Ð.
082406Z	25.3 144.7	45 25.		35.	24.			141.6		47.	-10.	ט.ט 27.7	142.3	25.	216.	0. 0.	0.0	0.0	0.	-0.	ð. ð.
882412Z	25.8 144.7	50 25.		35.	8.			145.2		186.	-10.	2 r . r	0.0	25. 0.	-0.	0.	0.0	0.0	0.	~0.	0. 0.
882418Z	26.2 144.1			40.	34.									• •			0.0			-0.	D.
	26.5 143.4							144.6		199.	15.	0.0	0.0	0.	-0.	ø.			0.		0. 0.
002500Z 002506Z	27.1 142.8		3 143.7	35.	20.		28.3	142.6		132.	15.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	~8.	
082512Z	27.1 142.0	45 27.	5 143.4 6 142.0	35.	40.		29.4	143.1	48.	143.	15.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	~0.	0.
				30.	21.	-10.	0.0	0.6	9.	-0.	ø.	0.0	0.0	0.	-0.	9.	0.0	0.0	0.	-0.	0.
682518Z	29.1 141.3		2 148.8	30.	27.	-5.	0.0	0.0		-0.	8.	0.0	0.0	0.	-0.	ø.	0.0	9.0	0.	-0.	8.
6 82688Z	30.0 141.2		2 141.1	25.	13.	-5.	0.0	0.0		-0.	0.	0.0	0.0	0.	-8.	Ð.	0.0	0.0	0.	-0.	0.
8826862	31.2 141.3	25 0.	0.8	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.

	ALL	FORECAS	TS		TYPHO	ONS WHIL	e over	35 KTS
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	18.	134.	317.	395.	ð.	0.	€.	0.
AVG RIGHT ANGLE ERROR	11.	92.	213.	198.	0.	Ð.	0.	Ð.
AVG INTENSITY MAGNITUDE ERROR	7.	13.	23.	34.	0.	0.	0.	Θ.
AVG INTENSITY BIAS	-7.	4.	10.	34.	0.	Θ.	0.	0.
NUMBER OF FORECASTS	23	19	13	7	9	8	0	2

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1859. HM

AVERAGE SPEED OF TROPICAL CYCLONE IS

9. KNOTS

TROPICAL STORM DOM
FIX POSITIONS FOR CYCLONE NO. 8

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
1 * 3 * 3 4 5 6 7 8 9	171888 190000 190300 190600 190600 191638 191290 181680 181900 192058	15.1N 137.0E 15.7N 138.6E 15.9N 137.9E 15.1N 136.4E 15.2N 136.2E 15.3N 135.6E 15.4N 135.6E 15.4N 134.5E 15.4N 134.8E	PCN 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	T1.8/1.8 T1.8/1.8 /S8.8/16HRS	ULCC FIX INIT OBS	PGTU PGTU PGTU PGTU PGTU PGTU PGTU PGTU
11 12 13 14 15	182317 198300 198538 198938 191288	15.7N 133.9E 16.2N 133.8E 16.4N 133.5E 16.1N 133.6E 16.4N 132.7E	PCN 5 PCN 4 PCN 3 PCN 4 PCN 6	T2.5/2.5 /D1.5/07HRS T2.5/2.5 /D1.5/12HRS		PGTW PGTW PGTW PGTW PGTW

17 119 20 12 23 24 5 26 7 29 38 3 34 35 6 6 6 7 38 3 34 4 4 24 34 4 4 5 5 5 5 5 5 5 5 6 6 6 6 6 6 6 6 6	212100 212212 212212 228300 228437 221630 221633 221738 221738 221738 221738 221738 221738 221738 221738 231800 231200 231200 231600 241600 241600 241600 241733 242248 24	24.5N 142.2E 24.6N 142.7E 24.9N 143.1E 25.2N 143.4E 25.2N 143.6E 25.5N 143.6E 25.5N 143.9E 25.5N 143.9E 25.5N 144.2E 25.5N 144.2E 25.5N 144.6E 25.2N 144.6E 25.5N 144.6E 25.5N 144.6E 25.5N 144.6E 25.5N 144.6E 25.5N 144.6E 26.6N 144.5E 25.5N 144.6E 26.5N 143.3E 26.5N 143.3E 27.5N 143.5E 27.5N 144.5E 29.5N 141.5E 30.5N 141.5E 30.5N 141.5E 30.5N 141.5E 30.5N 141.5E	######################################	T2.8/2.8 T3.8/3.8 /D8.5 T2.8/2.8 T3.8/3.8 /S0.8 T2.8/2.5 /D8.5 T2.8/2.5 /D8.5 T2.8/2.6 /S8.8 T2.5/2.5 /D8.5 T3.8/3.8 /D8.5 T3.8/3.8 /D8.5 T3.8/3.8 /D8.5 T3.8/3.8 /S8.8	1/24HRS 1/24HRS 1/24HRS 1/24HRS 1/24HRS 1/24HRS 1/24HRS	EXP LLCC		PGPK PGT2 3 2 3 2 3 2 3 2 3 2 3 2 3 2 3 2 3 2 3		
					AIRCR	AFT FIXES				
FIX NO.	TIME (Z)	FIX POSITION	FLT			MAX-FLT-LVL-WND F DIR/VEL/BRG/RNG NA		EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	222351 232659 232316 246641	16.2N 133.0E 16.7N 132.2E 16.8N 132.2E 17.5N 132.8E 17.5N 132.5E 19.1N 134.4E 19.3N 134.4E 20.3N 135.9E 20.5N 135.6E 23.4N 136.5E 24.8N 142.7E 25.4N 144.2E 25.1N 144.2E 25.5N 144.7E	1500FT 700MB 700MB 700MB 700MB 700MB 1500FT 700MB 1500FT 1500FT 1500FT 1500FT 700MB 700MB	1002 58 3112 55 3089 35 3083 3124 1003 35 1002 35 3116 1003 30 995 40 999 35	138 18 140 32 5 228 27 5 190 90 6 150 60 6 020 5 6 150 50 1 160 220 8 360 8 6 330 20 2 210 75	240 33 140 25 920 22 930 60 1 240 37 170 95 1 200 24 950 30 1 210 40 140 150 270 36 220 150 210 33 140 100 340 18 220 120 1 220 38 140 185 360 37 270 20 990 39 360 8 960 40 330 20 240 72 220 90 1	0 2 7 4 8 10 0 10 5 2 2 8 10 5 1 1 5 5 1 7 3 5 3 6 3 0 4		+26 +27	3 4 4 5 5 6 6 7 7 8 9 11 11 12 12

16	242842	26.0N 144.0E	788HB	3094		50 060	25	186	5i 86	50	15	2	+10 +11	13
17	242325	26.5N 143.8E	706MB	3052	998	35 140	135	000	34 35	50	8	5	+11 +12	13
10	251829	27.4N 142.1E	788119	3122	1007			210	36 11	63	8	7	+12 +11	14
19	251381	28.2N 141.8E	786MB	3118				969	27 32	60	10	5		14
28	252832	29.3N 148.8E	700MB	3105		25 090	30	190	26 09	98	5	8	+12 +12 +10	15
21	252340	38.8N 141.2E	7681B	3120	1883	25 270	25	100	20 03	40	5	10	+26 +22 29	9 15

TROPICAL DEPRESSION 89 BEST TRACK DATA

	BEST TRAC	:K		us	RHING	ER	RORS		24 H	OUR F		ST		48 H	OUR FO		ST RORS		72 H	OUR FO		ST RORS
MD/DA/HR	POSIT	UIND	P	SIT	MIND	DST	WIND	PO	SIT	MIND	DST	GHIN	₽O	SIT	MIND	DST	WIND	P09	31T	MIND	DST	WIND
8825862	25.5 128.1	20	0.0	6.6	۵.	-8.	Ø.	0.0	9.0	0.	-8.	0.	0.0	8.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0025 12Z	25.6 128.8	20	0.0	0.0	0.	-0.	0.	0.9	8.0	ø.	-0.	0.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.
8 825182	26.6 128.7	20	0.0	0.0	0.	-0.	0.	Ø.	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
002600 Z	27.6 129.1	25	0.0	0.0	0.	-0.	0.	Ø.1	0.0	ø.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
082606 Z	29.0 129.2	25	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
98 2612Z	30.3 128.9	25 3	30. 3	129.1	25.	10.	ø.	0.0	0.0	0.	-6.	0.	0.0	0.0	Ø.	-0.	Ø.	0.0	0.0	0.	-0.	0.
9 82618Z	31.8 128.4	25 3	31.6	128.6	25.	16.	ð.	0.0	8.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ø.	-0.	0.
08 2700Z	33.3 127.4	30 3	33.9	127.0	30.	41.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0 82796Z	34.9 126.9	25 3	34.9	127.2	25.	15.	0.	0.0	0.9	0.	-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	e.	-0.	0.

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 622. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

13. KNOTS

TROPICAL DEPRESSION TD09W FIX POSITIONS FOR CYCLONE NO. 9

SATELLITE FIXES

FIX NO.	TIPE (Z)	FIX POSITION	ACCRY	BYORAK CODE	CONTENTS	SITE
1	258388	25.4H 128.1E	PCN 6	T1.8/1.8	INIT DOS	PGTW
2	258558	25.5N 120.2E	PCN 5			PGTW
3	250946	25.7N 128.6E	PCN 6			PGT⊌
4	251266	25.2N 129.0E	PCN 6	T1.5/1.5	INIT OBS ULCC FIX	PGTW
5	251600	26.2N 128.4E	PCN 6		ULCC FIX	PGTU
6	260000	27.8N 129.2E	PCN 6	T2.8/2.8 /D1.8/12HRS		PGTW
7	260300	28.7N 129.3E	PCN 6			PGTW
8	260545	20.9N 129.3E	PCN 5			PGTW
9	260600	29.6N 129.2E	PCN 6			PGTW
10	26 0900	29.4N 129.1E	PCN 6			PGTW
11	261033	30.0N 129.2E	PCN 3		EXP LLCC	RPMK
12	261105	30.1N 129.0E	PCN 3			RKSO
13	261200	30.3N 129.8E	PCN 6	T1.5/1.5 /S0.8/12HRS		PGTW
14	261600	31.2N 128.6E	PCN 6			PGTW
15	262132	32.7N 128.8E	PCN 3	T1.5/1.5	EXP LLCC	RPMK
16	262346	33.3N 127.9E	PCN 3	T1.5/1.5	INIT OBS	RKSO
17	278888	33.4N 127.5E	PCN 4	T1.5/2.8 /W8.5/12HRS		PGTW
18	278388	34.2N 127.6E	PCN 6			PGTW
19	278688	34.9N 126.9E	PCN 6			PGTW
20	271844	36.8N 127.4E	PCN 5			RKSO

AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	Fi.T LVL			MAX-FLT-LVL-UND DIR/VEL/BRG/RNG		EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
	262726	77 7N 197 7E	70000	7001	25 170 55	100 75 120 125	5 D			414 414 411	,

SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)		CONTENTS
		33.3N 126.9E	030	626	WHO 47184,	
2	278688	34.9N 127.2F	825	のクラ	LIMO 47156	47 1 6R

TYPHOON ELLEN BEST TRACK DATA

				u	ARN ING	ER	RORS		24	HOUR F		AST RRORS		48 H	HOUR F		AST RRORS		72 (HOUR F		AST RRORS
MD/DA/HR	POSIT	WIND	P	DSIT	WIND	DSI	MIND	PC	DSIT	WIND	DS.	T WIND	P	DSIT	MINI	DS'	T WIND	P	05 I T	WIN	DS DS	T WIND
0827 00 Z	9.8 183.2	20	0.0	0.0	0.	-0.	0.	0.0	0.0		-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.
082706Z	10.2 101.7	20	0.0	6.6	Ð.	-0.	0.	0.0	0.0		-0.	ø.	0.0	0.0	8.	-0.	Ø.	0.0	0.0	ø.	-8.	٥.
082712Z	10.7 180.2	20	0.0	0.0	0.	-0.	ø.	0.0	0.0		~0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
6 82718Z	11.3 178.8	20	0.0	0.0	0.	-0.	0.	0.0	0.0		-0.	0.	0.0	0.0	9.	-0.	0.	0.0	0.0	0.	-0.	0.
082800Z	11.8 177.6	20	0.0	0.0	0.	-0.	ø.	0.0	0.0		-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	8. 0.	-0.	0.
082806Z 882812Z	12.2 176.1	20 25	0.0	0.0 0.0	0. 0.	-0. -0.	0. 0.	0.0	0.0 0.0		-0. -0.	0.	0.0	0.0 0.0	Ð.	-0. -0.	0. 0.	0.0	0.0	ø.	-0. -0.	0. 8.
082818Z	13.1 173.0	30	0.0	0.0	Ø.	-0.	ø. Ø.	0.0	8.8		-0. -0.	0. 0.	0.0	0.0	ø. Ø.	-0. -0.	ø.	0.0	0.0	0.	-0. -0.	Ø.
002010Z	13.1 171.3		13.0	171.3	35.	6.		14.2	164.8		74.				55.	270.	10.	15.5		75.	412.	40.
082906Z	13.2 169.9			178.2	35.	18.		13.9	165.9		154.		14.8	161.8	55.	386.	10.	15.3		75.	569.	40.
082912Z	13.2 168.5			168.8	40.	18.			165.2		226.			161.5	65.	484.			158.2	85.	792.	60.
0 82918Z	13.1 166.8	45	13.4	166.9	45.	19.	0.	14.9	163.0	55.	274.	15.	16.0	160.3	75.	550.	35.	17.3	157.9	95.	909.	65.
083000Z	13.0 165.1	48	13.2	165.2	35.	13,			159.9	50.	195.	5.	15.0	155.9	70.	394.	35.	16.2	151.8	90.	654.	55.
083 00 62	12.5 163.7			163.8	45.	36,		13.3	150.8					154.8		407.			150.9		653.	55.
083012Z	11.9 162.0			162.4	40.	34.			157.9					154.6		508.			151.4		730.	45.
683618Z	11.4 160.0			160.3	45.	40.								151.1		452.		14.6		98.	620.	48.
003100Z	10.9 158.4			158.4		18.			151.7		51.			146.1	75.	227.			141.3	95.	298.	40.
083106Z 083112Z	10.5 156.9			157.0	45. 40.	19. 17.			150.8		103.			145.4 144.1		264. 260.			140.7		323. 302.	35. 20.
083118Z	10.2 153.0				48.	24.			147.4		188.			142.5		267.		14.2			330.	20.
090 100Z	10.3 151.2			151.2	35.	6.			143.5		132.			137.8		163.			133.2		149.	15.
898186Z	10.2 149.2			149.2	35.	12.		11.9	141.8		162.			136.0	70.				131.5	85.		0.
096112Z	9.4 147.1			147.2	35.	42.			139.7		100.			133.8		102.			129.2	85.	53.	-5.
898118Z	9.1 144.8	30	8.4	144.7	35.	42.	5.	8.3	136.9		139.	0.		131.1		160.			126.7	80.	223.	-15.
090200Z	9.0 143.4	35	9.5	143.0	25.	30.	-10.	9.6	137.4	45.	25.	-10.	10.6	132.7	60.	118.	-15.	12.3	129.1	75.	174.	-20.
890206Z	9.2 141.8	40		141.8	40.	ø.	ø.	9.6	136.4	45.	59.	-15.	18.9	131.8		142.			128.3	70.	203.	-25.
090 212Z	9.2 148.2	45		148.3	40.	8.			135.4					130.5					126.7		228.	
990218Z	9.5 130.9	50		139.1	45.	17.		10.2	134.3					129.5					125.6	80.	260.	-20.
090300Z	10.0 137.5	55		137.6	68.	13.			132.9					128.8					125.3		204.	
898386Z	18.5 136.8			136.0	50.		-10.		131.9	65.	85.			128.2		137.			124.5		173.	
090312Z 090318Z	10.9 134.4			134.3	65. 65.	6. 17.		13.5	128.8		55. 93.			124.1		205. 240.			119.1		324. 355.	-45. -25.
898486Z	12.3 131.7			131.7	65.		-10.		127.1		93. 84.			122.2					117.2		325.	
890406Z	13.0 130.7			130.B	79.				125.9		102.			121.0		261.			116.2	85.	285.	-13. 0.
898412Z	13.7 129.6			129.4	90.	13.			124.7		110.			120.3		190.			116.8	75.	184.	-10.
098418Z	14.4 128.8			128.7	95.	8.			124.8		21.			120.8	90.	26.			117.0	80.	66.	0.
090500Z	15.0 128.0	95	15.1	120.0	95.	6.	Ø.		126.3		145.				130.	291.			122.4	115.	361.	40.
898586 2	15.9 126.9			127.0	95.	8.			124.7		91.					210.			120.9	90.	303.	15.
8985 12Z	16.8 125.8			125.9	95.	8.			123.3		63.				130.				119.5		303.	45.
8985 18Z	17.2 125.1			124.9	100.	11.			122.0		47.			120.4					119.1		313.	30.
090600Z	17.8 124.1			124.8	120.	6.			121.1		54.				100.					100.	283.	35.
898686Z	10.3 123.2			123.1		8.			119.7		41.			117.2	100.	92.			115.0	95.	197.	45.
090612Z 090610Z	10.7 122.2 19.0 121.2			122.8	120. 118.	11.			118.8		72. 49.		21.6 22.1	116.8		108.	30. 35.	22.1 0.0	115.7	190. 0.	231.	70. 0.
698768Z	19.3 128.2			128.1	85.	6.			117.4		49. 58.			115.6		127.	25.	0.0	0.0	0.	-0. -8.	0.
898786Z	19.5 119.2			119.1	98.	13.			115.7		31.			113.6	75.	60.	25. 25.	0.0	0.0	Ø.	-8.	8.
8987122	19.7 118.3			118.2	95.	6.			115.1	95.	30.			113.0	75.	91.	45.	0.0	0.0	ø.	-0.	0.
8987 18Z	28.8 117.5			117.8	95.	25.			115.6	95.	78.	25.	0.0	0.0	e.	-0.	Ð.	0.0	0.0	ē.	-0.	ø.
090000Z	28.5 116.6	75	20.3	116.4	75.	16.			113.1	65.	25.	8.	8.0	0.0	ø.	-0.	8.	0.0	0.0	0.	-0.	0.
090006Z	28.9 115.8			115.6	75.	11.			112.2	50.	23.	8.	8.0	8.8	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0900 12Z	21.3 114.9			115.0	78.	₿.			112.7	45.	65.	15.	0.0	0.0	0.	-0.	0.	0.0	0.0	₽.	-0.	₽.
6988 182	21.7 114.1			114.3	78.	11.	€.	0.0	0.6	€.	-0.	₽.	0.0	0.0	₽.	-0.	ø.	0.0	0.0	0.	-0.	0.
090900 Z	22.1 113.4			113.4	65.	6.	0.	0.0	8.8	0.	-0.	₽.	0.8	0.0	8.	-8.	8.	0.0	0.0	0.	-0.	0.
999906Z	22.5 112.6			112.6	56.	12.	ø.	0.0	0.0	₽.	-0.	Ð.	8.8	0.0	0.	-8.	ø.	0.0	6.0	0.	-0.	0.
0909 127	22.8 111.6	36	22.7	111.5	30.	8.	0.	0.0	0.0	€.	-0.	●.	8.0	0.0	₽.	-0.	0.	0.0	0.0	8.	-0.	0.

	ALL	FORECAS	TS		TYPHO	35 KTS		
	WRNG	24-HR	48-HR	72-HR	LIRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	15.	101.	223.	339.	13.	98.	212.	311.
AVG RIGHT ANGLE ERROR	11.	60.	123.	178.	10.	61.	122.	178.
AVG INTENSITY MAGNITUDE ERROR	3.	17.	27.	31.	3.	16.	26.	29.
AVG INTENSITY BIAS	-0.	11.	11.	15.	~1.	10.	9.	11.
MARKE OF EDSCROOTS	47	43	79	75	44	-	76	12

bistance traveled by tropical cyclone is 4462. NM AVERAGE SPEED OF TROPICAL CYCLONE IS 14. KNOTS

TYPHOON ELLEN FIX POSITIONS FOR CYCLONE NO. 18

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
				• • • • • • • • • • • • • • • • • • • •		
1	278666	9.8N 176.6W	PCN 6	T2.8/2.8	INIT OBS	PGTU
5	270300	9.8N 178.3W	PCN 6			PGTW
3	278688 278658	18.1N 177.7W 18.9N 178.3W	PCN 6 PCN 6	T2.5/2.5 /D1.0/29HRS	ULCC FIX	PGTU KGWC
5	278988	19.4N 178.5W	PCH 6	12.372.3 791.0720FR3	ULCC FIX	PGTW
6	271200	10.7N 179.9W	PCN 6			PGTW
7 8	271748 271 888	11.5N 179.8E 11.6N 179.7E	PCN 6 PCN 6			KGWC PGTW
9	289998	11.8N 178.8E	PCH 6	T2.8/2.8+/S8.8/24HRS		PGTW
10	280300	11.8N 177.1E	PCN 6		III CC ETV	PGTW
11 12	200600 200620	12.2N 176.0E	PCN 6 PCN 6	T3.8/3.8 /D8.5/24HRS	ULCC FIX	PGTW KGWC
13	288900	12.3N 175.4E	PCN 6		ULCC FIX	PGTW
14 15	281288 281688	12.5N 174.0E 13.1N 174.0E	PCN 6 PCN 6	T2.0/2.0	ULCC FIX INIT OBS	PGTW PGTW
16	281888	13.2N 173.4E	PCN 6	12.0/2.0	ULCC FIX	PGTW
17	281968	12.9N 172.5E	PCN 6			KGUC
18 19	282188 29888	13.0N 172.2E 12.9N 171.2E	PCN 6 PCN 6	T2.5/2.5 /D8.5/88HRS		PGTW PGTW
20	298388	12.7N 170.5E	PCN 6	10.0.0.0		PGTW
21 22	298326 298688	12.8N 170.2E	PCN 6 PCN 6	T3.8/3.8 /S8.8/21HRS		KGWC PGTW
23	290900	13.1N 170.2E 13.3N 169.6E	PCN 6			PGTW
24	291200	13.2N 168.7E	PCN 6			PGTW
25 26	291600 291600	13.2N 167.2E 13.3N 166.7E	PCN 6 PCN 6	T3.0/3.0 /D1.0/16HRS		PGTW PGTW
27	292100	13.4N 165.8E	PCN 6		ULCC FIX	PGTW
28	300000	12.9N 164.7E	PCN 6	T2.5/2.5 /S0.0/08HRS		PGTU
29 30	300300 300456	12.7N 164.0E 12.6N 163.6E	PCN 6 PCN 5			PGTW PGTW
31	300600	12.5N 163.4E	PCN 6			PGTW
32 33	300900 301200	12.2N 162.6E 12.1N 161.9E	PCN 6 PCN 6			PGTW PGTW
34	301600	11.9N 160.8E	PCN 6	T3.0/3.0 /S0.0/16HRS		PGTW
35	301800	11.8N 160.2E	PCN 6			PGTW
36 37	302008 310000	11.2N 159.5E 10.7N 158.4E	PCN 5 PCN 6			PGTW PGTW
38	310300	10.6H 157.3E	PCN 6	T3.5/3.5 /D0.5/11HRS		PGTW
39	310600	10.1N 156.2E	PCN 6 PCN 5			PGTW PGTW
49 41	310848 311200	9.6N 155.8E 9.5N 154.4E	PCN 6			PGTW
42	311600	9.5N 153.4E	PCN 6	T2.5/3.0 /W1.0/13HRS		PGTW
43 44	311 900 311947	9.9N 152.8E 10.8N 153.3E	PCN 6 PCN 5			PGTW PGTW
45	010000	10.5N 151.3E	PCN 6			PGTW
46 47	010300 010431	10.6N 151.1E 10.7N 150.5E	PCN 4 PCN 6	T2.0/2.5+/W0.5/11HRS		PGTW PGTW
48	010600	10.5N 149.7E	PCN 6			PGTW
49	010027	18.0N 148.6E	PCN 6			PGTW
50 51	011200 011600	10.1N 146.9E 9.1N 145.8E	PCN 6 PCN 6	T2.5/2.5 /D0.5/13HRS	ULCC FIX	PGTW PGTW
52	011716	8.9N 145.3E	PCN 5	12.0.2.0 - 00.0.10.110	ULCC FIX	PGTW
53 54	012100 02 000 0	8.8N 143.6E 9.7N 144.2E	PCN 6 PCN 6			PGTW PGTW
55	020300	9.5N 143.5E	PCN 6	T2.5/2.5+/S0.0/11HRS		PGTW
56	02060 1	9.2N 142.1E	PCN 5			PGTW
57 58	020900 021200	8.9N 141.1E B.7N 140.4E	PCN 6 PCN 6			PGTW PGTW
59	021600	9.1N 139.6E	PCN 6	T3.0/3.0 /D0.5/13HRS		PGTW
60	021800 022046	9.2N 139.4E 9.5N 138.6E	PCN 6 PCN 6			PGTW PGTW
61 62	022254	9.6N 137.9E	PCN 6			PGTW
63	022254	9.7N 138.0E	PCN 5	T3.0/3.0	INIT OBS	RPMK
64 65	0300 00 03030 0	9.8N 137.5E 10.2N 136.8E	PCN 6 PCN 6	T3.0/3.0 /D0.5/11HRS		PGTW PGTW
66	030548	10.7N 136.1E	PCN 5			PGTW
67 68	030900	11.0N 135.3E	PCN 6			PGTW PGTW
69	031200 031600	11.0N 134.6E 11.5N 133.2E	PCN 4 PCN 6			PGTW
78	031800	11.5N 132.9E	PCN 6			PGTW
71 72	031833 031833	11.5N 132.7E 11.3N 133.1E	PCN 5 PCN 5			PGTW RPMK
73	032100	12.0N 132.4E	PCN 6			PGTW
74	032233	12.2N 132.2E	PCH 5	74 8 44 8 . 64 8 6 6 7 7 7 7		PGTW
75 76	032233 040000	11.7N 132.1E 12.4N 131.8E	PCN 5 PCN 6	T4.8/4.8 /D1.8/24HRS		RPMK PGTW
77	040300	12.8N 131.3E	PCN 2	T4.0/4.0 /D1.0/11HRS		PGTW
78 79	040536	12.8N 130.7E	PCN 3			PGTW PGTW
73	040600	13.3N 130.6E	PCN 4			ruiW

	848988	13.4N 130.2E	PCN 4			PGTW
	848985					PGT⊎
	841688		PCN 6	T4.5/4.5 /D1.8/13HRS		PGTW
	041800		PCN 6			PGTW
	942188		PCN 2		CAT DIA THE	PGTU
	842145 858888		PCN 1 PCN 4		EYE DIA SNM	PGTW PGTW
87	050300		PCN 2	T4.5/4.5 /D0.5/11HRS		PGTU
	050600		PCN 2	14.5/4.5 / DO.5/11/R5		PGTU
	050900					PGTW
98	051200	16.7N 125.9E	PCN 2			PGTU
91	851688	16.7N 125.9E 16.9N 125.2E	PCN 2	T5.5/5.5 /D1.8/13HRS		PGTW
92	05 18 0 0	17.1N 124.9E	PCN 2			PGTW
	0 52100					PGTW
		17.6N 124.5E	PCN 1			PGT₩
	052330	17.8N 124.1E	PCN 1		EYE DIA 20NM	PGTW
	052330	17.9N 124.2E	PCN 1	T6.0/6.0 T6.0/6.0-/D1.5/11HRS T6.0/6.0	INIT OBS EYE DIA 15MM	RODN
97	969399	18.1N 123.5E	PCN 2	16.0/6.0-/D1.5/11HKS	ETE DIM ZOMII	FGIW
20	060643	18.4N 122.9E 18.5N 123.1E	PCN I	T6.8/6.0		RPMK PGTW
100	060900	18.5N 123.7E	PCN 3			PGTW
	861884		PCN 2		EYE DIA 12NM	PGTW
	861288				EIE DIN 12MI	PGTW
	061600		PCN 4	T4.5/5.5+/W1.0/13HRS		PGTU
	861888	19.1N 121.1E	PCN 4			PGTW
185	862183	19.8N 120.3E	PCN 4			PGTW
106	062244	19.2N 120.2E 19.3N 120.2E	PCN 3	T5.0/6.0+/U1.0/19HRS		RPMK
107	962388	19.3N 128.2E	PCN 3	T4.5/5.5+/W1.5/19HRS		RPMK
168	070000	19.2N 120.2E	PCN 4			PGT₩
		19.4N 119.5E				PGTW
	070641	19.7N 11B.9E	PCH 3	T5.0/6.0	INIT OBS	PGTW
		19.5N 118.7E	PCN 4			PGTW
	971299 971699			T4.5/4.5+/S0.0/10HRS		PGTW PGTW
			PCN 4	14.3/4.37/30.0/10HKS		PGTW
115	871926	19.7N 117.8E 20.0N 117.5E	PCN 4			PGTU
116	872188	20.1N 117.2E	PCN 4			PGTW
	072223			T5.8/5.8 /D8.5/23HR\$		RPMK
		28.8N 116.8E	PCN 3	T4.5/4.5	INIT OBS	RODN
	999999		PCN 6			PGTW
	080300	20.7N 116.3E	PCN 6	T4.5/5.0-/W0.5/20HR\$		PGTW
	888688	28.9N 115.6E				PGTW
	080629 080629		PCN 3	74 7 6 9 49 7 60000		PGTW RPMK
123	0000523	21.5N 115.9E	PUN 3	T4.5/5.0 /W0.5/98HRS		PGTW
125	881187		PCN 5			RPMK
		21.6N 114.7E				RDDN
		21.7N 114.9E	PCN 6			PGTW
	081608		PCH 4	T4.5/4.5-/S8.8/13HRS		PGTW
129	961966	21.6N 113.9E	PCN 4			PGTW
	881913					PGTW
		22.1N 113.5E				PGTW
	882282			T4.5/4.5		RKSO
	090000	22.3N 113.1E	PCN 4			PGTU
	090005			T4.8/4.5-/WB.5/25HRS		RODN
	090300	22.2N 113.1E 22.6N 113.8E	PCN 5	T4.5/5.8-/48.5/26HRS		RPMK PGTU
	090688	22.7N 113.8E	PCN 6	T3.5/4.0 /W1.0/11HRS		PGTU
	898758		PCN 5	T3.0/4.0-/U1.5/25HRS		RPMK
	898988		PCN 6	1010/710 /8110/601163		PGTU
		22.7N 118.2E	PCN 5			RPMK
		22.6N 111.5E	PCN 5			RKSO
		22.6N 118.2E	PCN 5			RPMK
143		22.4H 111.2E	PCN 6			PGTU

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT	OBS MSLP	MAX-SFC- VEL/BRG/		MAX- DIR/				ACC NAV		EYE SHAPE		RIEN- TATION	EYE TE OUT / IN/			MSN NO.
1	292311 300153	13.1N 165.3E 13.1N 164.7E	1500FT 1500FT		1988 1987	35 270 48 360	5 15	198		898 368	15 15	8	3				+26 +24 +25			1
3	300512 300012	12.8N 163.9E	1500FT	3159	1003	50 050	5	140	45	950 950 910	5	12	2 20				+23 +24		31	2
5	382858 382329	10.9N 159.2E 11.2N 158.4E		3143	1919 1997	35 338 45 848	70 30	939 110	32	330 020	68 78		15				+18 +18 +26 +26		30	3
7	318411 318647	10.9N 157.5E 10.8N 156.9E	1500FT 1500FT		1007	30 030 35 330	30 60	130	53	220 330	28 58	3	3				+14 +26 +26 +26	+23		4
9 18	312138 818529	18.1N 151.6E 18.4N 149.3E	1500FT 1500FT		1006 1006	25 848 25 338	98 88	130 010		969 339	60 90	6	8 5				+23 +25 +27 +26		31	5 7
11	010622 011519	9.9N 148.4E 8.7N 145.9E	1500FT 700HB	3094	1889	28 298	40	120 110		968 358	115 50	10 20					+27 +24 +10 +10			7 8
* 13 14	611837 626226	8.2N 144.8E 9.3N 142.7E	1500FT	3106	999	50 030	5	230 130	48	090 020	9 8 15	15 5	12				+23 +24		29	9
15 16	828821 821145	9.3N 141.2E 9.2N 140.5E		3007 3109	1000	55 030	10	836 896	37	958 338	3 68	8	5 8	ELLIPTICAL	. 15 5	360	+11 +13	+ 9		10
17 18	822848 8223 13	9.8N 138.2E 9.9N 137.7E	70019 70019	2990 3002		45 330 65 290	30 14	090 210	67 43	330 140	68 120	5 5	_				+13 +14 + 9 +15			11 11

		10 41 174 05	700.0									_	_	D 100111 00				
19	838459	18.4N 136.2E	786MB	2994		50 320	35	990	63	330.	שיז	8	3	CIRCULAR	20		+12 +15 +	- B 12
26	838753	10.7N 135.2E	700MB	2975		55 000	60	130	53	989	90	10	3	CIRCULAR	18		+10 +19 +	-13 12
21	032041	11.9N 132.3E	700MB	2944		70 360	70	128	72	939	100	20	1					13
22	032330	12.2N 131.8E	788MB	2941	985	88 188	- 5	230	51	140	10	10	1	CIRCULAR	20		+14 +17 +	10 13
23	040529	13.0N 130.8E	788MB	2936	982	90 090	6	140	60	858	60	Θ	1	ELL IPTICAL	30 15	878	+15 +20 +	-11 14
24	848821	13.3N 138.3E	788MB	2946		55 290	25	210	50	150	97	8	1					14
25	842832	14.6N 128.1E	788MB	2845		48 838	90	160	82	090	15	10	5	ELL IPTICAL	40 30	030		15
26	842335	15.8H 128.1E	790MB	2827	969	55 340	48	340	68	290	19	15	2	CIRCULAR	25		+16 +19 +	-10 15
27	050005	16.2N 126.6E	790MB	2712	956	78 128	30	198	97	120	29	10	4	CIRCULAR	17		+15 +17	16
28	651844	16.5N 126.1E	788MB	2673				020	83	360	11	10	1	C IRCULAR	15		+16 +19 +	-13 16
29	052057	17.5N 124.3E	788MB	2560	936	78 848	68	160	109	120	27	5	5	C IRCULAR	12		+12 +17	17
30	052343	17.8N 124.8E	700MB	2482	928	120 360	89	010	109	270	15	5	5	CIRCULAR	10		+11 +21	17
31	062158	19.2N 128.5E	700MB	2765		55 210	25	130	69	360	50	4	1					18
32	862349	19.2N 120.2E	786MB	2793	966	88 898	12	170	71	000	45	Θ	1	CIRCULAR	20		+17 +20 +	-15 10
33	878836	19.7N 118.7E	788MB	2756		98 898	15	160	61	898	15	8	5	C IRCULAR	15		+15 +17 +	-13 19
34	071115	19.6N 118.4E	7881B	2742	959	50 360	120	898	66	878	10	Θ	2	C IRCULAR	15		+13 +21 +	- 9 19
35	072236	20.3N 116.8E	766MB	2917	967	60 220	68	180	74	090	30	20	2	CIRCULAR	15		+11 +18 +	-15 20

RADAR FIXES

FIX	TIME	FIX			EYE	EYE	RADOB-CODE		RADAR	SITE
NO.	(Z)	POSITION	RADAR	ACCRY	SHAPE	DIAM	ASWAR TODFF	CONTENTS	POSITION	WMO NO.
1	052300	16.7N 124.2E	LAND				21901 ////		18.3N 121.7E	98231
ż	060000	17.8N 123.9E					22932 42908	EYE 25 PCT ELPTCL DIA 48-60 KMS	18.3N 121.7E	98231
3	969939	17.8N 123.8E					11992 42782	EYE 50 PCT ELPTCL DIA 50-60 KMS	18.3N 121.7E	98231
4	060100	17.9N 123.7E					11752 43305	EYE 35 PCT ELPTCL DIA 35-40 KMS	18.3N 121.7E	98231
5	060130	17.9N 123.6E	LAND				11712 42702	EYE 30 PCT ELPTCL DIA 35-40 KMS	18.3N 121.7E	98231
6	06 0200	18.0N 123.6E					11832 43602	EYE 30 PCT ELPTCL DIA 40-50 KMS	18.3N 121.7E	98231
7	060230	18.0N 123.5E					10872 42701	EYE 60 PCT CIR DIA 40 KMS	18.3N 121.7E	98231
8	060300	18.8N 123.5E					10072 42701	EYE 80 PCT CIR DIA 45 KMS	18.3N 121.7E	98231
. 9	060330	18.1N 123.4E					10872 42901	EYE 100 PCT CIR DIA 40 KMS	18.3N 121.7E	98231
10	060500	10.3N 123.3E					10872 63212	EYE 188 PCT CIR DIA 48 KMS	18.3N 121.7E	98231
11 12	060600 060630	18.4N 123.0E					10712 42902 10712 43202		18.3N 121.7E 18.3N 121.7E	98231 98231
13	060800	18.4N 122.9E 18.5N 122.6E					10742 42802		18.3N 121.7E	98231
14	060900	18.6N 122.5E					40682 42903		18.3N 121.7E	98231
15	868938	18.6N 122.4E					10672 42702		18.3N 121.7E	98231
16	061000	18.6N 122.4E					10521 40000		18.3N 121.7E	98231
17	861838	18.6N 122.3E	LAND				10421 42905		18.3N 121.7E	98231
18	961199	18.6N 122.2E					10411 42901		18.3N 121.7E	98231
19	061130	18.6N 122.1E					10411 42702		18.3N 121.7E	98231
20	061230	18.7N 121.9E					10317 42805		18.3N 121.7E	98231
21	061300	18.7N 121.8E					//// 42901	C. C	18.3N 121.7E	98231
22 23	861438 861588	18.7N 121.6E 18.9N 121.5E					10311 42704 10371 43404	EYE 65 PCT CIR EYE 85 PCT CIR	18.3N 121.7E 18.3N 121.7E	98231 98231
24	961930	19.1N 120.7E					10691 42905	EYE 60 PCT CIR DIA 30 KMS	18.3N 121.7E	98231
25	062000	19.1N 120.7E					10281 40000	EYE 65 PCT CIR DIA 10 KMS	18.3N 121.7E	98231
26	062100	19.2N 120.7E					11461 43284	EYE 55 PCT ELPTCL DIA 20 KMS	18.3N 121.7E	98231
27	062230	19.3N 120.3E					4/// 42983		16.3N 120.6E	98321
28	062300	19.3N 120.3E	LAND				11841 52705	EYE 50 PCT ELPTCL DIA 25 KMS	18.3N 121.7E	98231
29	0623 00	19.2N 120.4E					4/// 42904		16.3N 120.6E	98321
30	070140	19.4N 119.9E					11481 43003	EYE 40 PCT ELPTCL DIA 25 KMS	18.3N 121.7E	98231
31	878200	19.6N 119.5E					10613 43206		16.3N 120.6E	98321
32 33	070230 070240	19.6N 119.4E 19.4N 119.7E					10613 43207 11471 42903	EYE 50 PCT CIR OPEN SW DIA 35 K EYE 30 PCT DIA 25 KMS	16.3N 120.6E 18.3N 121.7E	98321 98231
34	070300	19.5N 119.6E					11181 33310	EYE 35 PCT ELPTCL DIA 20-25 KMS	18.3N 121.7E	98231
35	979650	20.4N 119.3E					6///3 53011	ETE 33 FOR CERTOE DIA ED ES RID	23.3N 116.7E	59316
36	070700	19.7N 118.9E					5/// 53003		18.3N 121.7E	98231
37	671208	19.6N 118.2E					4/// 52707		22.6N 120.3E	46744
38	080200	29.BN 116.7E	LAND				6///2 /2808		22.3N 114.2E	45005
39	080400	20.8N 116.8E					30973 53109		22.3N 114.2E	45005
40	060500	20.8N 116.0E					30913 63106		22.3N 114.2E	45005
41	099999	21.8N 115.5E					30943 73108		22.3H 114.2E	45005
42 43	080900 081000	21.8N 115.4E 21.8N 115.3E					10382 73009 10382 73009		22.3N 114.2E 22.3N 114.2E	45005 45005
44	091100	21.2N 115.3E					3/// 73005		22.3N 114.2E	45005
45	001150	21.1N 115.2E					24934 53010		23.3N 116.7E	59316
46	981299	21.3N 115.8E					30111 73008		22.3N 114.2E	45005
47	001400	21.5N 114.9E					2/// 73010		22.3N 114.2E	45005
48	881588	21.5N 114.6E					2/// 73818		22.3N 114.2E	45005
49	061600	21.6N 114.5E					2//// 73010		22.3N 114.2E	45005
58	001700	21.6N 114.4E					2//// 73010		22.3H 114.2E	45005
51	0 819 0 0	21.7N 114.0E	LAND				2020/ 72911		22.3N 114.2E	45 005

SYNOPTIC FIXES

FIX NO.		FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)			COMMENTS
2	002100	21.7N 114.3E 22.0N 113.7E	070 070	948 928	UMD	45005 45011,	45005

SUPER TYPHOON FORREST BEST TRACK DATA

	BEST TRACK	WARNING	ERRORS	24 H	HOUR FOREC	AST RRORS	48 HOUR	FORECAST ERRORS	72 HOUR FORECAST ERRORS	
MD/DA/HR	POSIT WIND	POSIT WIND		POSIT			NIW TIEN		POSIT WIND DST WIN	
0920122		3.3 143.9 30.		2 140.2	35. 92.		137.2 50.			
		.2 143.0 40.		2 139.3	75. 76.		135.5 90.		6.3 131.6 100. 24230.	
		.0 142.0 60.	B. 10. 14.		90. 61.	25. 5.2			7.5 129.6 110. 20120.	
892186Z		2.7 141.0 65.	8. 10. 15.		90. 76.	-5. 16.7			7.7 120.2 110. 24115.	
		6.6 139.9 65.	6. 5. 15.		85. 97.				8.9 129.2 100. 20220.	
0921182		1.4 139.0 65.	6. 0. 16.		80. 112.	-60. 18.3			9.4 129.8 95. 23825.	
092200Z		5.1 138.1 65.		7 134.6	85. 83.				0.6 127.2 105. 19215.	
092206Z		.0 137.0 70.	1325. 19.	0 133.A	90. 35.		129.5 100.		3.1 125.8 110. 9415.	
092212Z		.4 136.1 115.		3 133.0	140. 74.		130.3 135.	111. 15. 2	2.8 128.5 130. 174. 10.	
092218Z	18.2 134.7 140 16	3.1 134.7 130.	610. 20.	8 131.0	140. 31.	10. 23.2	128.8 135.	46. 15. 2	5.1 127.3 130. 91. 10.	
092300Z	18.6 133.5 150 16	3.7 133.6 140.	810. 21.	2 129.7	135. 37.	5. 23.7	127.5 135.	13. 15. 2	6.1 127.2 130. 125. 15.	
0923 0 62	19.1 132.4 145 19	.2 132.6 145.	13. 0. 21.	7 128.9	148. 41.	15. 24.5	127.2 135.	20. 10. 2	6.9 127.4 130. 172. 15.	
8923122	19.8 131.8 135 19	0.5 131.9 135.	19. 6. 21.	5 128.4	125. 42.	5. 24.2	2 126.8 115.	505. 2	7.5 126.9 105. 1595.	
892318 Z	20.3 131.1 130 26	.0 130.9 135.	21. 5. 22.	2 127.7	125. 51.	5. 25.2	2 126.8 115.	655. 2	8.5 127.4 1 0 5. 188. 0 .	
092400Z	20.8 130.2 130 26	1.8 130.3 125.	65. 24.	0 128.2	110. 51.	-10. 27.0	120.8 100.	20415. 3	0.8 131.5 90. 3955.	
092406Z	21.5 129.6 125 21	.5 129.8 120.	115. 24.	7 128.3	110. 80.	-15. 27.9	128.8 95.	23920. 3	1.6 132.3 80. 4025.	
092412Z	22.2 128.5 120 22	2.2 128.6 120.	6. 0. 26.	2 127.5	110. 102.	-10. 30.8	130.4 90.	36920. 3	5.9 143.1 68. 93020.	
092418Z	23.0 128.0 120 22	2.9 127.8 115.	135. 27.	0 127.8	100. 129.	-20. 31.6	5 131.5 80.	42125. 3	6.0 145.7 50. 95320.	
09250 0 2	23.8 127.3 120 23	5.7 127.4 120.	8. 0.27.	9 127.5	110. 149.	-5. 33.9	136.2 80.		7.5 150.7 50.109115.	
092506Z	24.3 126.9 125 24	1.3 126.9 115.	010. 28.	1 127.0	100. 145.	-15. 33.6	3 135.9 80.		7.5 150.4 50. 907. 0.	
	24.9 126.3 120 25		135. 28.		105. 152.		3 136.2 80.	• • • • • • • • • • • • • • • • • • • •	0.0 0.0 00. 0.	
0 92518Z	25.8 125.8 120 25	5.7 125.8 115.				-5. 33.7	' 135.8 BØ.		0.0 0.0 00. 0.	
	26.8 125.0 115 27			2 125.0			127.5 90.		0.0 0.0 00. 0.	
	27.7 124.3 115 27				100. 78.		3 126.6 85.		0.0 0.0 00. 0.	
	28.2 124.0 110 26			5 123.7	100. 99.	20. 0.0			0.0 0.0 00. 0.	
		3.1 124.0 110.	5. 5. 33.		85. 86.	15. 0.0			0.0 0.0 00. 0.	
		3.8 124.0 100.	12. 5. 32.		85. 230.	20. 0.0			L.O 0.0 OO. O.	
		0.5 124.4 90.	12. 5. 33.		80. 333.	30. 0.0			0.0 0.0 00. 0.	
		.0 125.7 85.	12. 5. 0.		00.	9. 0.0			0.0 0.0 00. 0.	
		.5 126.8 85.	27. 15. 0.		00.	9. 9.6			0.0 0.0 00. 0.	
		2.6 129.3 65.	8. 0. 0.		00.	9. 0.0			0.0 0.0 00. 0.	
092806Z	32.8 132.8 50 32	2.9 132.8 50.	6. 0. 0.	0.0	0. -0 .	0. 0.0	9.9 9.	-0. 0.	0.0 0.0 00. 0.	

	ALL FORECASTS				TYPHOONS WHILE OVER 35 K					
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HF	48-HF	72-HR		
AVG FORECAST POSIT ERROR	11.	97.	224.	3 66.	10.	97.	224.	366.		
AVG RIGHT ANGLE ERROR	Θ.	64.	79.	110.	в.	64.	79.	118.		
AVG INTENSITY MAGNITUDE ERROR	5.	18.	25.	17.	5.	18.	25.	17.		
AVG INTENSITY BIAS	-0.	-5.	-14.	-12.	-0.	-5.	-14.	-12.		
NUMBER OF FORECASTS	32	28	24	20	31	28	24	20		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2191. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 12. KNOTS

SUPER TYPHOON FORREST FIX POSITIONS FOR CYCLONE NO. 11

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
1	170000	7.3N 162.7E	PCN 6	T0.0/0.0		PGTW
2	170300	8.0N 168.6E	PCN 6			PGTU
3	170600	6.8N 161.8E	PCN 6			PGTW
4	170900	5.6N 161.6E	PCN 6			PGTU
5	171288	5.4N 161.9E	PCN 6			PGTW
6	171600	5.4N 159.4E	PCN 6			PGTW
7	171800	5.6N 158.9E	PCN 6			PGTW
8	172188	6.2N 158.5E	PCN 6			PGT⊌
9	160000	6.2N 158.1E	PCN 6	T8.8/8.8 /S8.8/24HR5		PGT₩
10	100300	5.4H 157.6E	PCN 6			PGT⊎
11	180600	5.3N 156.8E	PCN 6			PG TW
12	180900	5.2N 156.0E	PCN 6			PGTW
13	181200	5.2N 155.3E	PCN 6	T1.5/1.5	INIT OBS	PGTW
14	181600	5.1N 154.3E	PCN 6		ULCC FIX	PGT₩
15	181800	5.5N 153.7E	PCN 6			PGTW
16	182188	5.9N 152.6E	PCN 5			PGT₩
17	190000	6.0N 152.5E	PCN 6	T2.0/2.0-/D2.0/12HR5	ULCC FIX	PGT₩
18	190300	6.3H 151.9E	PCN 6		ULCC FIX	PG~1
19	190600	6.4N 151.3E	PCN 6		ULCC FIX	PGT⊎
20	190053	6.0N 150.7E	PCN 5		ULCC FIX	PGTW
21	191627	8.7N 148.3E	PCN 6	T2.0/2.0 /D0.5/16HPS		PGTW
22	191951	9.3N 147.9E	PCN 6		ULCC FIX	PGT₩
23	192147	9.4N 146.9E	PCN 5			PGTW

24	200000	0 54	146 75	DCN C	TO E 40 E 400 E 400U00		DCTI I
			146.3E	PCN 6	T2.5/2.5 /D8.5/89HRS		PGTW
25	200300		145.6E	PCN 6			PGTW
26	200600	18.2N	144.8E	PCN 6			PG TW
27	200832	10.1N	144.4E	PCN 6			PGTW
28	201027	19.3N	144. IE	PCN 6			PGTW
29					T7 8 /7 8 /01 8 /10U00		
	201200		144.0E	PCN 6	T3.0/3.0 /D1.0/12HRS		PGTW
30	20160 0		143.6E	PCN 6			PGTW
31	201800	11.1N	143.6E	PCN 6			PGTW
32	202100	11.BN	142.5E	PCN 6			PGTW
33	202111	11.BN		PCH 6			PGTW
					77 0 47 0	INIT OOC	
34	202112		143.0E	PCN 5	T3.0/3.0	INIT 08S	RPMK
35	210000	11.9N	141.9E	PCN 6			PGTW
36	210300	12.4N	141.4E	PCH 4	T3.5/3.5 /D1.8/15HRS		PGTW
37	210530	12.BN	141.0E	PCH 4			PGTW
38	210900	13.3N		PCN 4			PGTW
39							
	211005	13.5N		PCN 4			PGTW
40	211200	13.3N		PCN 6	T4.0/4.0 /D1.0/12HRS		PGTW
41	211600	14.2N	139.6E	PCN 6			PGTW
42	211866	14.4N	139.0E	PCN 6			PGTW
43	212050		138.5E	PCN 3			PGTW
			138.2E				
44	212245			PCN 3			PGTW
45	212245		130,3E	PCN 3	T4.5/4.5 /D1.5/25HRS		rpmk
46	220000	15.3N	138.1E	PCH 4	T4.0/4.0 /D0.5/12HRS		PGTW
47	220300	15.8N	137.6E	PCH 4			PGTW
48	228517		136.6E	PCN 3	T4.5/4.5	INIT OBS	RODN
49	220600	16.3N		PCN 2	17.3/ 7.3	1111 005	PGTW
50	220900	17.0N		PCN 2			PGTW
51	220944	17.0N	136.4E	PCN 2			PGT₩
52	221200	17.4N	136.1E	PCN 2	T5.0/5.0 /D1.0/12HRS		PGTW
53	221600		135.0E	PCN 2	= · = · · · · · · · · · · · · · · · · ·		PGTW
54	221800		134.7E	PCN 2			PGTW
55	222030		134. 1E	PCN 1			PGTW
56	222223	18.5N	133.9E	PCN 1			PGTW
57	238888	18.5N		PCH 2	T5.5/5.5 /D1.5/12HRS		PGTW
58	230300	18.9N		PCN 2			PGTW
59	230600	19.2N		PCN 2			PGTW
60	230646	19.2N		PCH 3	T5.5/5.5 /D1.0/26HRS		RODN
61	230647	19.0N	132.7E	PCH 1			PGTW
62	230910	19.3N	132.0E	PCN 2			PGTW
63	231103	19.4N		PCH 1			RPMK
					TE E & E 400 E (10)100		
64	231200	19.5N		PCN 2	T5.5/5.5-/D0.5/12HRS		PGTW
65	231600	19.BN		PCN 2			PGTW
66	231800	19.9N	130.9E	PCN 2			PGTW
67	232100	20.3N	130.7E	PCN 2			PGTW
68	232150	20.6N		PCH 1			PGTW
					** * * * *	INIT DDC	
69	232150	20.6N		PCN 1	T6.5/6.5	INIT DBS	RPMK
78	232342	20.6%	130.4E	PCH 2	T5.5/5.5 /S0.0/12HRS		PGTW
71	2 4000 0	20.7N	130.3E	PCN 2			PGTW
72	240300	21.1N		PCN 2			PGTW
73	240600	21.5H		PCN 2			PGTW
74	240634	21.6N		PCN 2			PGTW
75	241041	22.2N	128.8E	PCN 1			PGTW
76	241941	22.1N	128.8E	PCN 1	T6.5/6.5	INIT OBS	RPMK
77	241200	22.4N	128.7F	PCN 2	T5.0/5.5 /W0.5/12HRS		PGTW
78	241600	22.6N		PCN 4	1010-010 - D010-12-M0		PGTW
79	241800	22.9N		PCH 4			PGTW
80	242100	23.3N	127.9E	PCN 4			PGTW
81	242129	23.5N	127.9E	PCN 3		EYE OPEN SSW-SE	PGTW
82	242129	23.4N	128.RE	PCN 1	T6.8/6.5 /W8.5/24HRS		RPMK
83	242321	23.6N		PCN 1	T5.5/5.5-/SØ.0/12HRS		PGTW
						1N1T 000	
84	242321	23.6N		PCN 1	T5.0/5.0	INIT OBS	RODN
85	250300	24.2N		PCN 2			PGTW
86	250600	24.4N		PCN 2			PGTW
87	250622	24.3N	126.8E	PCN 1			PGT⊎
88	250900	24.8N		PCN 2			PGTW
89	251008		126.7E	PCN 2			PGTW
90							PGTW
	251019	24.8N		PCN 2			
91	251200	25.2N		PCN 2	T5.0/5.0-/S0.0/12HRS		PGTW
92	251600	25.4N		PCN 2			PGTW
93	251800	25.7N	125.9E	PCN 2			PGTW
94	252100	26.2N		PCN 2			PGTW
95	252107	26.4N		PCN 1	T		PGTW
96	252259	26.6N		PCN 1	T6.0/6.0 /S0.0/25HRS		RPMK
97	252259	26.6N	125.1E	PCH 1	T5.5/5.5 /S0.0/11HRS		PGTW
98	260000	26.8N		PCN 2			PGTW
99	260300	27.4N		PCN 2			PGTW
		27.6N					PGTW
100	260600			PCN 2			
101	260610	27.5N		PCH 1			PGTW
102	260900	27.9N		PCH 2		EYE DIA 25NM	PGTW
103	260948	27.9N	124.2E	PCN 2			PGTW
104	261200	28.2N		PCN 2		EYE DIA 25NM	PGTW
	261600				TS 0/5 0-/60 0/17400		
105		28.7N		PCN 2	T5.0/5.0-/S0.0/17HRS		PGTW
106	261800	29. IN		PCN 2			PGTW
107	262047	29.4N	123.8E	PCN 3			PGTW
100	270000	29.6N	123.9E	PCN 4	T4.0/5.0 /W1.5/08HRS		PGTW
100	210000			PCH 3	T4.5/5.5-/W1.5/25HRS		REITS
		30. ON					
109	270019	30.0N			14.3/3.3-/W1.3/23NR3		
109 110	270019 270300	29.9N	124. IE	PCH 4	14.3/3.3-/W1.3/23RR3		PuTW
109 110 111	270019 270300 270557	29.9N 30.3N	124. IE 124. 6E	PCN 4 PCN 3	14.3/3.3-/W1.3/23AR3		PGTW PGTW
109 110	270019 270300	29.9N	124. IE 124. 6E	PCH 4	14.3/3,3-/W1.3/23RR3		PuTW
109 110 111	270019 270300 270557	29.9N 30.3N	124.1E 124.6E 124.8E	PCN 4 PCN 3	14.3/3,3-/W1,3/23nk3		PGTW PGTW
109 110 111 112 113	270019 270300 270557 270900 271100	29.9N 30.3N 30.7N 31.0N	124.1E 124.6E 124.9E 125.4E	PCH 4 PCH 3 PCH 4 PCH 5	14.3/3,3°/W1.3/23HR3		PGTW PGTW PGTW RODN
109 110 111 112	270019 270300 270557 270900	29.9N 30.3N 30.7N	124.1E 124.6E 124.8E 125.4E 127.1E	PCH 4 PCH 3 PCH 4	14.3/3,3-7W1.3/23HR3		PGTW PGTW PGTW

116	271680	31.3N 126.5E	PCN 6	T2.5/3.5 /W1.5/16HRS			PGTW
117	272025	32.4N 12B.5E	PCN 5				RODN
118	272100	32.5N 127.5E	PCN 6		ULCC	FIX	PGTW
119	272357	32.6N 129.2E	PCN 3	T3.0/3.0	INIT	085	RKSO
120	280006	32.6N 129.4E	PCN 4	T3.0/4.0 /W1.5/08HRS			PGTW
121	280300	32.9N 130.8E	PCN 6				₽GTW
122	280545	33.0N 132.3E	PCN 5				PGTW
123	280905	33.6N 135.7E	PCN 6				PGTW
124	281200	35.2N 137.BE	PCN 6				PGTW
125	281600	35.0N 140.4E	PCN 6				₽GT⊎
126	281800	35.7N 142.3E	PCN 6				PGTW
127	282355	35.3N 143.7E	PCN 5	T2.0/3.0 /W1.0/24HRS			RKSO

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	780MB HGT	08S MSLP	MAX-SFC- VEL/BRG		MAX- DIR/			-WND ∕RNG	NAV/		EYE SHAPE		ORIEN- TATION	EYE TEM OUT/ IN/		115N NO.
1	202337	12.0N 142.0E	700MB	3032	994	65 160	70	120		030	61	8	2				+13 +		5
2	210252	12.2N 141.4E	700MB	3013		55 050	25	120		050	30	6	2				+12 +	. 9	2
3	210544	12.7N 141.0E	700MB	2981		40 360	30	090		360	30	5	2				+14		6
4	210839	13.2N 140.4E	789MB	2984	987	60 110	40	220		130	70	.5	3	ELLIPTICAL		020	+12 +15 +		<u>.</u>
5	212127	14.9N 138.3E	700MB	2866		65 330	20	200		130	120	15	2	CIRCULAR	96		+12 +15 +		<u> </u>
6	212340	15.1H 138.1E	700MB	2865	975	99 369	30	130		360	20	10	2	CIRCULAR	10		+10 +16 +	-	΄.
7	221057	17.0N 136.2E	700MB	2468	926			090			30	12	1	CIRCULAR	5		+13 +25 +	13	8
9	221345	17.5N 135.7E	700MB	2285				160		898	10	12	ı		_				8
. 9	222030	18.4N 134.2E	700MB	2009		70 310	90	230		120	10	3	1	CIRCULAR	5		+14 +27 +		9
18	222307	18.5N 133.7E	700MB	2068	883	130 210	10	260		210	25	3	1	CIRCULAR	5		+15 +27 +		.,
11	230912	19.3N 132.1E	700MB	2189	898	65 120	82	190		100	17	8	3	CIRCULAR	6		+15 +19 +		11
12	231139	19.5N 132.0E	700MB	2235	902			120		020	21	. 8	3	CIRCULAR	7		+13 +19 +		11
13	232044	20.5N 130.9E	700MB	2314		100 360	30	110	110		30	15	1	ELL IPTICAL			+16 +20 +		12
14	232312	20.8N 130.3E	700MB	2315	911	120 230	30	049		320	60	6	1	CONCENTRIC			+15 +19 +		12
15	240835	21.9N 129.2E	700MB	2376		100 120	22	149	105		48	3	1	ELL IPTICAL	8 4		+16 +19 +	-	13
16	241104	22.2N 128.7E	700MB	2383	919			049			45	5	2	ELLIPTICAL	B 4	110	+16 +19 +		13
17	242032	23.4N 127.8E	700MB	2377	917	80 010	90		110		80	7	3	CIRCULAR	5		+17 +21 +		14
18	242312	23.7N 127.4E	700MB	2393	918	80 210	90	030		290	41	7	3	CIRCULAR	6		+14 +21 +		14
19	250630	24.8N 126.8E	700MB	2302	909			190	101		97	4	2	CIRCULAR	20		+13 +20 +		15
20	251114	24.BN 126.5E	700MB	2392	918			350			40	4	2	ELL IPTICAL			+19 +22 +		15
21	252036	26.3N 125.6E	700MB	2406		90 070			110		120	12	1	ELLIPTICAL	30 26	170	+16 +21 +		16
22	252335	26.BN 125.1E	700MB	2433	924	130 230	18	110		030	30	9	1	CIRCULAR	18		+16 +20 +		16
23	260841	27.8N 124.3E	780MB	2460	926	100 090	60	180		090	80	5	3	CIRCULAR	25		+15 +20 +		17
24	272358	32.7N 129.2E	700MB	2894	976	50 230	68	310	59	240	100	5	5	CIRCULAR	40		+15 +16 +	12	18

RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB-CODE ASWAR TODFF	CONTIENTS	RADAR POSITION	SITE
,	241900	23.3N 128.0E	LAND	FAIR		70		MVG 34/30	26.1N 127.7E	47937
;	242000	23.3N 127.8E		FAIR		60		MVG 32/20	26.1N 127.7E	47937
3	242100	23.4N 127.8E		GOOD		58		MVG 33/20	26.1N 127.7E	47937
4	242200	23.5N 127.6E		GOOD		50		MVG 33/20	26.1N 127.7E	47937
5	242300	23.7N 127.5E		GOOD		55		MVG 33/20	26.1N 127.7E	47937
6	250000	23.7N 127.4E		GOOD		50		MVG 33/20	24.8N 125.3E	47927
7	250100	23.8N 127.3E		GOOD		40		MVG 33/10	24.8N 125.3E	47927
8	250135	24.1N 127.4E	LAND	POOR				MVG 31/15	26.4N 127.8E	47931
9	250200	23.9N 127.3E	LAND	GOOD		40		MVG 33/20	24.8N 125.3E	47927
10	258235	24.2N 127.3E	LAND	POOR					26.4N 127.8E	47931
11	250300	24.0N 127.2E	LAND	GOOD		50		MVG 33/20	24.8N 125.3E	47927
12	258488	24.2N 127.1E		GOOD		60		MVG 35/20	26.1N 127.7E	47937
13	250500	24.2N 127.0E	LAND	GOOD		50		MVG 31/20	26.1N 127.7E	47937
14	250535	24.2N 127.1E		FAIR	ELLIPTICAL			AXIS 40/25	26.4N 127.8E	47931
15	25060 0	24.2N 126.9E					45//3 52911		24.8N 125.3E	47927
16	250600	24.3N 126.9E					11983 73208		26.1N 127.7E	47937
17	250600	24.3N 126.9E		GOOD		50		MVG 31/20	26.1N 127.7E	47937
10	250700	24.4N 126.BE		GOOD		55		MVG 33/20	26.1N 127.7E	47937
19	250735	24.BN 127.2E		POOR					26.4N 127.8E	47931
20	250800	24.7N 126.9E		GOOD		55		MVG 36/30	26.1N 127.7E	47937
21	250810	24.5N 126.8E		FAIR					26.4N 127.8E	47931
22	250935	24.9N 127.0E		FAIR	ELLIPTICAL			AXIS 35/20	26.4N 127.8E	47931
23	250900	24.8N 126.8E		GOOD		55		MVG 33/30	26.1N 127.7E	47937
24	250930	24.BN 126.7E		FAIR	ELLIPTICAL			AXIS 35/25	26.4N 127.8E	47931
25	251030	24.9N 126.6E		GOOD	ELLIPTICAL			AX1S 30/25	26.4N 127.8E	47931
26	251100	25.0N 126.5E		GOOD		55		MVG 32-10	26.1N 127.7E	47937
27	251130	24.9N 126.4E		GOOD	ELLIPTICAL			AXIS 55/45	26.4N 127.8E	47931
28	251230	25.1N 126.3E		GDOD	ELL IPTICAL			AXIS SE/40	26.4N 127.8E	47931
29	251300	25.1N 126.2E		GOOD		50		MVG 30/15	26. IN 127.7E	47937
38	251335	25.1N 126.2E		GOOD	ELL IPTICAL			AXIS 36/20	26.4N 127.8E	47931
31	251400	25.2N 126.2E		GOOD		50		MVG 33-20	26.1N 127.7E	47937
32	251435	25.2N 126.2E		GOOD	ELL IPTICAL			AXIS 30/25	26.4N 127.8E	47931
33	251688	25.5N 125.9E		COOD	F	55		MVG 33/20	26.1N 127.7E	47937
34	251630	25.3N 126.2E		COOD	ELL IPTICAL			AXIS 30/25	26.4N 127.8E	47931
35	251635	25.5N 126.1E		FAIR				M.O. 30. 30	26.4N 127.85	47931
36	251788	25.6H 125.6E		6009		50		MVG 32/20	26.1N 127.7E	47937
37	251735	25.6N 125.9E	LAND	POOR					26.4N 127.8E	47931

-	251900	25.7H 125.8E	LAND									157 35	47077
39	251835	25.8N 125.6E	LAND	GOOD FAIR		60		LLA	¥ 35/18			127.7E 127.8E	47937 47931
49	251988	25.8N 125.8E	LAND	COOD		60		MA	G 36/20			127.7E	47937
41	251935	25.8H 125.9E	LAND	POOR		90			G 36/20			127.8E	47931
42	252000	26.1N 125.8E	LAND	GOOD		40		140.	G 36, 40			127.7E	47937
	252930	26.2N 125.8E	LAND	FAIR	CONCENTRIC	28		***	u 30/40			127.8E	47931
44	252100	26.3N 125.7E	LAND	6000	CONCENTRIC	20		M.	G 32/38			127.7E	47937
45	252200	26.7N 125.5E	LAND	6000		48			G 33, 40			127.7E	47937
46	268888	26.8N 125.1E	LAND	GOOD		46			G 32/25			127.7E	47937
47	260100	26.8N 125.0E	LAND	GOOD		40			G 29-10			127.7E	47937
40	268288	27.0N 124.8E	LAND	GOOD		40			G 31-30			126.8E	47929
49	268388	27.2N 124.7E	LAND	6000		40			G 32/30			126.8E	47929
	268400	27.3N 124.6E	LAND				35/44 53					125.3E	47927
51	268408	27.2N 124.7E	LAND	COOD		35			G 36/20			126.8E	47929
52	268588	27.3N 124.4E	LAND				20874 52					125.3E	47927
53	268588	27.4N 124.5E	LAND	GOOD		30			G 33/20			126.8E	47929
54	268688	27.4N 124.4E	LAND				21815 53					125.3E	47927
55	268688	27.5N 124.4E	LAND	FAIR		40			G 33/20			126.8E	47929
56	260700	27.6N 124.3E	LAND				20815 53	411		24	1. BN	125.3E	47927
57	260700	27.5N 124.5E	LAND				6///3 83	308		26	i. IN	127.7E	47937
58	260700	27.6N 124.4E	LAND	FAIR		30		MV.	G 34/20	26	3.3N	126.8E	47929
59	268888	27.8N 124.2E	LAND				6///5 53	411		24	1.8N	125.3E	47927
60	260000	27.7N 124.3E	LAND	GOOD		25		MV.	G 33/20	26	3.3N	126.8E	47923
61	260900	27.BN 124.3E	LAND	COOD		20		MV.	G 35/20	26	. 3N	126.8E	47929
62	26 1 <i>0</i> 00	27.9N 124.2E	LAND	GOOD		25			G 30/20		. 3N	126.BE	47923
	2611 00	28.8H 124.1E	LAND	GOOD		20			G 31/20			126.BE	47929
	26 i 300	28.2N 124.1E	LAND	GOOD		20			G 34/20			126.8E	47929
65	261400	28.3N 124.0E	LAND	POOR		20			G 34/15			126.8E	47929
66	200010	32.7N 129.3E	LAND	GOOD		25		MV	G 09/30	32	.7N	128.8E	47844

SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)	CONTENTS
1		32.6N 129.3E	965	939	LP10 47843
2	290300	32.7N 131.3E	8 55	929	WMO 47821
3	288688	32.9N 132.8E	858	929	umo 47898
4	291200	34.7N 136.6E	040	012	UMO 47665, 47654, 47651,47778, 47771
5	291500	33.9N 139.4E	648	050	WMD 47678, 47675

TROPICAL STORM GEORGIA BEST TRACK DATA

	BEST TRA	CK		WF.	RHING				24 1	10UR F				48 1	HOUR F				72 H	IOUR FO		
						ERI	RORS				E	RORS				ER	RORS				EK.	RORS .
MO/DA/HR	POSIT	WIND	PC	SIT	MIND	DST	MIND	PC	SIT	WINI	05	r wini) P(15 I T	WIND	DST	MIND	P09	IT	MIND	DST	WIND
0 929 0 02	17.2 118.0	25	0.0	9.9	ø.	-Ø.	0.	0.0	0.0	ø.	-0.	Ð.	0.0	0.0	Ø.	-0.	ø.	0.0	0.0	0.	-0.	0.
892886Z	17.9 117.2	25	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
0928122	18.8 116.7	25	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Θ.
092818Z	19.2 115.7	35	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-ē.	ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	е.
892988Z	19.2 114.8	40	19.3	114.9	50.	8.	10.	20.0	111.4	65.	33.	15.	20.4	107.7	60.	52.	5.	0.0	0.0		-0.	θ.
092906Z	19.2 113.8	55	19.3	113.8	55.	6.	ø.	19.9	109.4	60.	31.	10.	20.8	105.0	50,	25.	10.	0.0	0.0	0.	-0.	0.
0 92912Z	19.3 112.5	55	19.3	112.3	50.	11.	-5.	20.1	107.8	50.	73.	5.	22.0	104.7	40.	78.	10.	0.0	0.0	ø.	-0.	0.
0 92918Z	19.3 111.9	50	19.3	111.6	50.	17.	0.	19.8	108.4	50.	29.	5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
093000 2	19.6 111.0	50	19.4	110.0	50.	16.	0.	20.1	107.4	45.	34.	-10.	0.0	0.0	0.	-0.	ø.	0.0	9.0	ø.	-0.	0.
093006Z	20.1 109.9	50	19.7	110.0	45.	25.	-5. 3	20.6	106.7	45.	68.	5.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	θ.
093012Z	20.2 109.1	45 2	20.2	109.0	45.	6.	0.	21.8	106.0	45.	102.	15.	8.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
093018Z	20.2 108.1	45 2	28.2	108.1	45.	0.	ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
100100Z	20.2 106.8	55 2	20.2	107.1	45.	17.	-10.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
100 106Z	20.5 105.5	40 2	20.5	105.5	40.	0.	0.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
199112Z	20.7 104.6	30 2	20.7	104.6	40.	0.	10.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	Ø.	-0.	ø.	0.0	0.0	0.	-0.	0.

	ALL	FORECAS	TS		TYPH0	ONS WHIL	E OVER	35 KTS
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	10.	53.	52.	0.	0.	ø.	Ø.	Ø.
AVG RIGHT ANGLE ERROR	7.	27.	18.	0.	0.	0.	0.	0.
AVG INTENSITY MAGNITUDE ERROR	4.	9.	8.	0.	6.	0.	0.	0.
AVG INTENSITY BIAS	0.	6.	8.	0.	0.	0.	0.	0.
NUMBER OF FORECASTS	11	7	3	0	0	9	0	9

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 825. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

10. KNOTS

TROPICAL STORM GEORGIA
FIX POSITIONS FOR CYCLONE NO. 12

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
1	286666	17.3N 118.0E	PCN 6	T1.8/1.8	INIT OBS	PGTW
2	280300	17.7N 117.5E	PCN 6			PGT⊍
3	288688	18.8N 117.2E	PCN 6			PGTW
4	280727	18.4N 116.7E	PCN 5	T1.5/1.5	INIT OBS	RPMK
5	288900	18.4N 116.9E	PCN 6			PGTW
6	2812 86	18.8N 116.6E	PCN 6	T1.5/1.5	INIT OBS	PGTW
7	281606	19.4N 116.3E	PCN 6			PGTW
8	281988	19.4N 114.8E	PCN 6		ULCC FIX	PGTU
9	282196	19.3H 114.5E	PCN 6			PGTW
10	282146	19.5N 115.1E	PCN 5			PGTW
11	282146	19.2N 114.5E	PCN 5			RPMK
12	290000	19.8H 114.8E	PCN 6	T3.6/3.0 /D2.8/24HRS		PGTU
13	296300	19.3N 114.5E	PCH 6			PGTU
14	290600	19.2N 113.8E	PCN 6			PGTW
15	298714	19.2H 113.BE	PCN 5	T3.5/3.5 /D2.8/24HRS		RPMK
16	290900	19.4H 112.8E	PCN 6			PGTU
17	291826	19.2N 112.5E	PCN 3			PGTW
10	291200	19.4N 112.3E	PCN 6	T3.8/3.8 /D1.5/24HRS		PGTW
19	291214	19.1N 111.8E	PCN 3			RODN
20	291215	18.9H 112.8E	PCN 5			RPMK PGTU
21	291600	19.1N 112.0E	PCN 6			PGTW
22	291900	19.1N 111.7E	PCN 6			PGTU
23	292100	19.1N 111.5E	PCN 6			PGTW
24	300000	19.1N 118.9E	PCH 6		INIT OBS	RODN
4	700054	19.6N 111.9E	PCN 3	T3.8/3.0	ULCC FIX	PGTW
5	300600	19.7N 110.5E 28.2N 189.8E	PCN 6 PCN 6	T3.5/3.5-/D0.5/30HRS	OCCC PIX	PGTW
2,	388988	28.4N 189.6E	PCN 6	13.3/3.3-/00.3/30NK3	ULCC FIX	PGTW
28 29	301153	20.4N 109.1E	PCN 4		DECE FIX	RODN
38	301200	26.4N 109.0E	PCN 6			PGTW
31	301600	19.9N 108.3E	PCN 6	T3.0/3.0~/S0.0/20HRS		PGTU
32	301000	28. IN 188. IE	PCN 4	13.0/3.0"/30.0/20HK3		PGTW
33	301947	19.8N 187.6E	PCN 5			RODN
34	382188	20.1N 107.7E	PCN 4			PGTU
35	302234	20.2N 107.7E	PCN 4			RODN
36	010000	28.4N 106.8E	PCN 4	T4.8/4.8-/D8.5/18HRS		PGTW
37	810033	20.3N 106.3E	PCH 3	T3.8/3.8 /S8.8/24HRS		RODN
31	J. JUJ3	F0.01 100.3E				

39 48 41	010600 011124 011131	20.4N 106.1E 20.5N 105.5E 20.5N 104.7E 20.6N 104.2E 20.7N 104.6E	PCN 4 PCN 4 PCN 5	T3.0/3.5-/J0.5/24HRS	PGTW PGTW Rodn RPMK PGTW
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FIX NO.	TIME (Z)	FIX POSITION	FLT LVL		MAX-FLT-LVL-UND DIR/VEL/BRG/RNG N	EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	
	200027	10 34 114 05	IFOOTT	200	 				_

RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB-CODE ASWAR TDDFF	CONTENTS	RADAR POSITION	SITE WMO NO.
1 2	29 0900 291500	19.5N 113.0E 19.5N 112.4E					6//// ////		22.3N 114.2E 22.3N 114.2E	45005 45005
3	301100	19.8N 110.3E	: AND				1183/ 3////		16.3N 129.6E	98321

TROPICAL STORM HERBERT BEST TRACK DATA

	BEST TRA	CK		LJA	RN I NG				24	HOUR F	ORECA	IST		48 H	OUR F	DRECA	ST		72 H	IOUR F	ORECA	ST
						ER	RORS				ER	RORS				ER	RORS				ER	RORS
MD/DA/H	R POSIT	WIND	PC	SIT	MIND	DST	WIND	PI	DSIT	WIND	DS1	. MIND	PC	DSIT	WIND	DST	WIND	PO:	SIT	WIND	DST	MIND
1006122	18.8 115.6	25	0.0	0.0	Θ.	·-e.	0.	0.0	0.0	Ø.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.
1006182	11.0 114.7	30	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1007002	11.4 113.8	35	11.3	113.8	35.	б.	ø.	11.8	111.2	45.	34.	Ø,	12.3	100.8	35.	43.	-5.	0.0	0.0	0.	~0.	0.
1007062	11.5 113.0	40	11.4	113.0	40.	6.	0.	12.0	110.1	45.	30.	-5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	~0.	0.
1007122	11.7 112.2	40	11.8	111.8	40.	24.	0.	12.2	108.8	40.	43.	-10.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1007102	11.8 111.5	48	11.9	111.0	40.	30.	0.	12.8	108.3	35.	29.	-10.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	~0.	Ø.
1008002	12.2 110.8	45	12.2	110.4	50.	23.	5.	12.7	107.9	30.	32.	-10.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	~0.	0.
1000062	12.5 110.1	50	12.8	110.3	50.	21.	9.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	Ø.	-0.	0.	0.0	0.0	0.	~0.	0.
1008122	12.6 109.4	50	12.9	109.5	45.	19.	-5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	~0.	0.
1008182	12.8 108.8	45	12.8	198.5	40.	10.	~5.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	~0.	Ø.
1999997	12 9 188 4	40	0 0	00		-0	а	a a	9 9		-0	a	00	00	а	-8	a		а а	а	~0	A

	ALL	FORECAS	TS		TYPHO	ONS WHIL	E OVER	35 KTS
	WRNG	24-HR	48-HR	72~HR	WRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	18.	33.	43.	8.	0.	0.	0.	0.
AVG RIGHT ANGLE ERROR	11.	24.	29.	θ.	Ð.	ø.	ø.	ø.
AVG INTENSITY MAGNITUDE ERROR	2.	7.	5.	0.	0.	ø.	0.	Θ.
AVG INTENSITY BIAS	-1.	-7.	-5.	Ð.	0.	ø.	0.	0.
NUMBER OF EDRECASTS	4	5		Ď.	ā.	a ·	a ·	Ä

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 445. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

7. KNOTS

TROPICAL STORM HERBERT FIX POSITIONS FOR CYCLONE ND. 13

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
1	041800	7.1N 121.8E	PCH 6			PGTU
2	842188	7.2N 120.6E	PCN 6			PGTW
3	858888	7.4N 119.9E	PCH 6			PGTW
4	050400	7.8N 119.4E	PCN 6	T1.0/1.0	INIT OBS	PGTW
5	051600	10.0N 118.5E	PCN 6	T1.0/1.0	INIT OBS	PGTW
6	051800	18.1N 118.1E	PCN 6			PGT⊎
7	9 5218 0	10.4N 117.2E	PCN 6			PGTW
8	969999	10.7N 115.4E	PCN 6		ULCC FIX	₽GTW
9	060400	10.8N 114.9E	PCH 6	T2.0/2.0 /D1.0/24HRS	ULCC FIX	PGT⊎
10	060600	18.7N 114.2E	PCN 6		ULCC FIX	PGT⊎
11	060730	11.0N 115.0E	PCN 3	T1.5/1.5	INIT OBS	RPMK
12	96990 0	10.9N 115.2E	PCH 6		ULCC FIX	PGTW
13	0 6112 3	11.1N 114.9E	PCH 6		ULCC FIX	PGTW
14	06 1 200	11.2N 114.9E	PCN 6			PGTW
15	06 1600	11.3N 114.2E	PCN 6	T2.0/2.0 /D1.0/24HRS		PGTU
16	9 61 990	11.6N 113.7E	PCN 6			PGTW
* 17	862188	11.9N 113.2E	PCN 6			PGTW
18	062219	12.0N 114.2E	PCN 5	T2.0/2.0 /D0.5/15HRS		RPMK
19	070000	11.5N 113.2E	PCN 6			PGTW
26	878983	11.9N 113.0E	PCH 5	T1.9/1.0	INIT OBS	RODN
21	078400	11.4N 113.1E	PCN 4	T2.5/2.5 /D0.5/24HRS		PGTW
22	078688	11.4N 112.9E	PCH 4			PGTW
23	070717	11.9N 113.1E	PCN 3	T3.0/3.0 /D1.5/24HRS		RPMK
24	070900	11.7N 112.7E	PCH 4			PGTW
25	871188	11.7N 111.7E	PCN 4			RODN
26	071200	11.9N 112.8E	PCN 6			PGTW
27	871688	11.8N 111.4E	PCH 6	T3.8/3.8-/D1.8/24HRS		PGT⊎
28	071800	12.0N 111.2E	PCN 6			PGTW
29	872882	11.7N 111.5E	PCN 5			RPMK
30	072100	12.3N 111.4E	PCN 6			PGTW
31	972158	12.2N 111.4E	PCN 5			PGTW
32	072159	12.0N 118.6E	PCN 5			RODN
33	072341	11.6N 111.4E	PCN 5	T3.5/3.5-/01.5/24HRS		RPMK
34	090000	12.3N 111.1E	PCH 6			PGTU
35	088488	13.0H 110.7E	PCH 4	T3.5/3.5-/D1.0/24HRS		PGTW
36	888688	13.2N 118.4E	PCN 4			PGTW
37	000785	12.6N 118.1E	PCN 5	T2.5/2.5	INIT DBS	RODN
38	666966	12.9N 118.0E	PCN 6	· - · · · · · · · · · · · · · · · · · ·		PGTW
39	601030	12.9N 109.5E	PCN 3			RPMK
40	001200	12.6N 189.5E	PCH 6			PGTW
			•			

		12.7N 188.8E 12.8N 188.5E		T2.5/3.5-/W8.5/24HRS	ULCC FIX	PGTW PGTW
43	881958	13.2N 188.7E	PCN 6			RODN
44	682186	12.9N 188.4E	PCN 6			PGTW
45	090000	13.2N 107.9E	PCH 6		ULCC FIX	PGTW

FIX NO.	TIME (Z)	FIX POSITION			MAX-FLT-LVL-WND ACCRY DIR/VEL/BRG/RNG NAV/MET	EYE SHAPE	EYE TEMP (C) DUT/ IN/ DP/SST	

1 878819 11.3N 113.8E 1500FT 998 58 148 28 228 44 148 28 28 4 +23 +24 +22 28 1

TYPHOON IDA BEST TRACK DATA

	BEST TRA	CK		WA	RHING				24 H	IOUR F				48 H	IDUR F	ORECE			72 H	OUR F	ORECA	
						ERI	RORS				E	RORS				ER	RORS				ER	RORS
MD/DA/HR	POSIT	MIND	PC	SIT	WIND	DST	CHIW	PC	IST	WINI) DS	T WIND	P	TIRC	WINI) DS1	. MIND	PO	SIT	MINI) DST	WIND
1006122	17.0 146.4	20	0.0	9.8	8.	-0.	0.	8.8	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	ø.	-0.	0.
188618Z	17.4 145.1	20	8.8	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	0.
1007002	17.9 143.9		0.0	0.0		-ë.	e.	0.0	0.0	ø.	-ø.	ē.	9.0	0.0	ø.	-0.	ø.	0.0	8.0	ø.	-0.	ø.
1007062	18.0 142.9		0.0	0.0		-0.	ē.	0.0	0.0	Δ.	-0.	ø.	0.0	8.0	ē.	-0.	ø.	0.0	0.0	ø.	-0.	ø.
1007122	18.4 141.9		0.0	8.0	a.	-0.	9.	9.0		e.			0.0		0.	-B.	Я.	0.0	0.0	۵.	-B.	ø.
									0.0	٠.	-0.	0.		0.0						70.		
190718Z	19.0 139.9		18.8	148.9	30.	50.		20.7	137.1	45.	238.		22.5		50.	304.			131.9	70.	501.	15.
100800Z	20.0 137.9		20.0	138.0	40.	6.		23.0	134.4	45.	132.	-10.	25.5		50.				132.6	70.	499.	15.
100006Z	20.8 136.4	40	20.8	136.5	40.	6.	0.	23.7	132.3	45.	71.	-15.	26.6	131.0	45.	261.	-20.	31.4	132.9	45.	548.	0.
1008122	21.4 134.8	50	21.3	134.7	50.	Θ.	0. 3	23.6	130.2	70.	185.	10.	26.7	129.2	70.	407.	10.	0.0	0.0	0.	-0.	0.
1008182	22.3 133.2	55	22.2	133.1	55.	Θ.	0.	25.5	129.4	70.	215.	10.	28.8	129.6	70.	405.	15.	0.0	0.0	0.	-0.	0.
100900Z	23.6 132.1	55	23.6	132.1	55.	0.	D. 3	27.9	131.5	65.	185.	0.	33.0	135.2	50.	200.	-5.	0.0	0.0	0.	-0.	0.
1009062	24.8 131.8	60	24.8	131.7	60.	5.		29.4	132.1	60.	95.		33.9	136.8	45.	310.	ø.	0.0	0.0	ø.	-0.	ø.
1009122	26.1 132.2		26.1	132.3	60.	ξ.		34.0	138.7	45.	251.	-15.	0.0	6.0	0.	-0.	ø.	0.0	0.0	ē.	~0.	ø.
1009182	27.4 132.8		27.5	132.8	55.	6.		34.0	138.6	49.			0.0	8.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	0.
101000Z	28.8 133.2											-15.										
			28.7	133.2	65.	6.		34.7	139.6	50.	65.	-5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
101006Z	30.3 133.6			133.5	65.	13.		36.3	143.0	50.	72.	5.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	ø.	-0.	0.
101012Z	31.4 134.8		31.4	134.8	60.	0.	0.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
101018Z	32.3 136.3	55	32.3	136.3	55.	8.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	0.	-0.	0.
1011 0 0Z	33.7 139.1	55	33.6	139.8	55.	16.	0.	0.0	0.0	0.	-0.	Ð.	0.0	0.0	ø.	-0.	0.	0.0	9.0	0.	-0.	0.
101106Z	35.1 142.9	45	35.1	142.8	45.	5.	ø.	0.0	0.0	8.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	₽.	-0.	0.

	ALL	FORECAS	TS .		TYPHOONS WHILE OVER 35 KTS						
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48~HR	72~HR			
AVG FORECAST POSIT ERROR	18.	144.	298.	516.	6.	144.	298.	516.			
AVG RIGHT ANGLE ERROR	6.	58.	95.	25.	6.	58.	95.	25.			
AVG INTENSITY MAGNITUDE ERROR	8.	9.	11.	10.	0.	9.	11.	10.			
AVG INTENSITY BIAS	-0.	-5.	-4.	10.	-0.	-5.	-4.	10.			
NUMBER OF FORECASTS	15	11	7	3	14	11	7	3			

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1889. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 17. KNOTS

TYPHOON IDA FIX POSITIONS FOR CYCLONE NO. 14

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
* 1	050000	17.8N 156.8E	PCN 6			PGTW
2	961688	17.3N 145.4E	PCN 6			PGTW
3	062100	17.8N 144.8E	PCN 6			PGTW
4	878888	17.9N 143.9E	PCN 6	T1.5/1.5	INIT OBS	PGTW
5	878486	17.8N 143.3E	PCN 6		ULCC FIX	PGTW
6	878688	18.8N 142.9E	PCN 6		ULCC FIX	PGT⊌
7	878988	18.1N 142.5E	PCN 6		ULCC FIX	PGT⊍
8	871288	18.2N 142.8E	PCN 6			PGT⊎
* 9	071600	18.5N 141.5E	PCN 6	T2.8/2.8	INIT OBS	₽GT⊌
* 10	871886	18.8N 148.9E	PCN 6		ULCC FIX	PGT₩
11	872817	18.7N 148.2E	PCN 5			PGTW
12	000000	28.8N 138.8E	PCN 4			PGTW
13	060400	20.6N 137.1E	PCN 4	T3.8/3.8 /D1.5/24HRS		PGTW
14	000 523	21.2N 136.5E	PCN 5	T3.5/3.5	INIT OBS	RODN
15	886688	20.9N 136.6E	PCN 4			PGTW
16	000057	21.1M 135.3E	PCN 4			PGTW
17	6 8 1 6 4 6	21.3N 136.0E	PCN 3			RODN
10	8 812 88	21.3N 134.7E	PCN 6			PGTW
19	66 16 66	21.9N 133.6E	PCN 6	T3.5/3.5 /D0.5/24HRS	ULCC FIX	PGTW
26	96 19 99	22.2N 133.1E	PCN 6		ULCC FIX	PGTW
21	6 821 66	22.8N 132.4E	PCN 6			PGTU
22	882137	22.9N 132.5E	PCN 5			PGTW
23	002137	23.4H 133.6E	PCN 5	T3.8/3.8	INIT OBS	RPMK
24	082319	23.8N 132.4E	PCN 3			RODN
25	090000	23.7N 131.7E	PCN 4			PGTW
26	090400	24.5N 131.6E	PCN 2	T4.8/4.0 /D1.8/24HRS		PGTU
27	898518	24.8N 131.9E	PCH 1	T4.8/4.8 /D8.5/24HRS		RODN
28	898688	25.6N 131.9E	PCH 2			PGTW

29	090633	24.8N 131.9E	PCN 3	T4.0/4.0 /D1.0/09HRS		RPMK
30	898653	25.0H 132.2E	PCN 2			PGTW
31	89 8988	25.5N 131.9E	PCH 4		4	PGTW
32	091017	25.7N 132.3E	PCN 3			PGTW
33	891288	26.1N 132.3E	PCN 2			PGTW
34	891688	27.2N 132.6E	PCN 4	T3.5/3.5-/S0.0/24HRS		PGTW
35	091800	27.5N 132.8E	PCN 6		ULÇC FIX	PGTW
36	092116	28.1N 133.2E	PCN 4			PGTU
37	892258	28.8N 133.3E	PCN 5		ULCC FIX	PGTW
38	692258	28.6N 133.1E	PCN 5			RODN
39	100000	28.6N 133.8E	PCN 6			PGTW
40	100300	29.6N 133.9E	PCN 6			PGTW
41	100600	30.0N 133.9E	PCN 6	T3.5/4.0-/W0.5/26HRS		PGTW
42	100900	30.6N 134.6E	PCN 6			₽GTW
43	100956	31.8N 134.8E	PCN 3			₽GTW
44	101200	31.4N 135.0E	PCN 4		ULCC FIX	PGTW
45	181600	31.8N 135.3E	PCH 4	T3.0/3.5 /W0.5/24HRS		PGTW
46	1018 00	32.1N 135.8E	PCN 6		ULCC FIX	PGTW
47	101925	32.8N 137.1E	PCN 5			RODN
48	102055	33.3N 137.6E	PCN 3		ULCC FIX	PGTW
49	10210 0	33.0N 137.4E	PCN 4		ULCC FIX	PGTW
50	102236	33.2N 138,2E	PCN 3	T3.0/3.0		RKSD
51	110000	33.8N 139.1E	PCN 6			PGTW
52	110300	34.6N 140.8E	PCN 4			PGTW
53	110445	34.9N 141.7E	PCN 6			PGTW
54	110600	35.1N 142.8E	PCN 6		ULCC FIX	PGTW
55	110900	35.8N 145.7E	PCN 6			₽GTW
56	111200	36.0N 147.0E	PCH 6		ULCC FIX	PGTW
57	111600	36.8N 151.5E	PCN 6	T1.5/2.5 /W1.5/24HRS		PGTW

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT	OBS MSLP		·SFC- ′BRG/		MAX- DIR/		-LVL- ⁄BRG/				EYE SHAPE	EYE O		EY OUT/		MP (I		MSN NO.
1	000010	20.0N 137.9E	1500FT		1888		010	30	980	44	816	30	10	5				+25	+24	+22	31	1
2	080629	20.0N 136.3E	700MB	3059		50	020	90	120	50	350	25	10	5								2
3	090026	21.1N 135.5E	700MB	3056	997	30	340	98	190	44	010	77	4	5				+10	+12	+12		2
4	082355	23.6N 132.1E	700MB	2988	986	65	280	30	340	51	286	30	7	4					+25	+22		3
5	090238	24.1N 131.8E	700MB	2937		70	140	20	240	69	148	20	5	5					+15	+16		3
6	898616	24.8N 131.7E	700MB	2969		40	170	70	150	61	040	60	10	1				+13	+15	+ 8		4
7	898854	25.3N 131.9E	788MB	2951	986	50	270	10	350	43	300	25	12	1				+13	+15	+10		4
8	092037	28.1N 133.0E	700MB	2910					190	89	130	60	10	5								5
9	092347	28.7N 133.1E	780MB	2985	977	88	280	10	350	67	338	19	19	3	CIRCULAR	8		+20	+22	+11		5
18	100534	30.1N 133.5E	780MB	2878		80	090	48	180	104	898	40	10	6	CIRCULAR	30		+16	+22			6
11	100756	30.6N 133.9E	788MB	2873	973		250	60	310		230	20	7	4				+15	+20			6
12	102038	33.1N 137.3E	700MB	2887			070	85	300	_	210	65	•		ELL IPTICAL	12 85	080	+15		+13		7
13	102302	33.3N 13B.2E	700MB	2901	979		160	35	280	_	170	35	5	2	ELL IPTICAL		060	+12				7

RADAR FIXES

	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB-CODE ASWAR TDDFF	COMPENTS	RADAR POSITION	SITE WMO NO.
NU.	(2)	FUST110N	KHNHK	HCCKI	SHAFE	DIMIT	HOWAR (DDFF	CONTENTS	F031110H	W 10 110.
1	100300	29.6N 133.6E	LAND				35/12 53616		30.6N 131.0E	47869
2	100600	30.2N 133.8E	LAND				35/12 50111		30.6N 131.0E	47869
3	100800	30.6N 134.0E	LAND				35/11 50216		30.6N 131.0E	47869
4	100800	30.7N 133.8E	LAND				5//// 4////		33.3N 134.2E	47899
5	100900	30.9N 134.0E	LAND				5//// 50314		33.3N 134.2E	47899
6	100900	30.8N 134.1E	LAND				33/41 50216		30.6N 131.0E	47869
7	101000	31.0N 134.2E					5//// 50416		33.3N 134.2E	47899
8	101000	30.9N 134.2E	LAND				65/41 50311		30.6N 131.0E	47869
9	101100	31.2N 134.6E					5//// 50522		33.3N 134.2E	47899
10	101200	31.3N 134.8E					5//// 50622		33.3N 134.2E	47899
11	101200	31.4N 134.6E					55//2 /////		35.3N 138.7E	47639
12	101300	31.4H 135.0E					5//// 50516		33.3N 134.2E	47899
13	101300	31.5N 135.0E					55//2 50722		35.3N 138.7E	47639
14	101400	31.6N 135.2E					5//// 50616		33.3N 134.2E	47899
15	101400	31.7N 135.2E					55//2 50316		35.3N 138.7E	47639
16	101500	31.7N 135.5E					5//// 50616		33.3N 134.2E	47899
17	101500	31.8N 135.4E					45//3 50614		35.3N 138.7E	47639
18	101600	31.8N 135.7E					5//// 50619		33.3N 134.2E	47899
19	101600	31.0N 135.7E					65//3 50816		35.3N 138.7E	47639
20	101790	32.2N 136.0E					54//3 50616		35.3N 138.7E	47639
21	101700	31.9N 136.0E					5//// 50619		33.3N 134.2E	47899
22	101800	32.3N 136.2E					54//4 50416		35.3N 138.7E	47639
23	101800	32.2N 136.4E					5//// 50524		33.3N 134.2E	47899
24	101800	32.1N 136.6E					6//// /////		34.6N 135.7E	47773
25	101900	32.4N 136.7E					52/13 50622		35.3N 138.7E	47639
26	101900	32.3N 136.8E					5//// 50624		33.3N 134.2E	47899
27	101900	32.9N 136.9E					6//// /////		34.6N 135.7E	47773
20	102000	33.3N 137.6E					6//// /////		34.6N 135.7E	47773
29	102000	32.6N 137.1E					5/// 50524		33.3N 134.2E	47899
30	102100	33.1N 137.7E					55/// /////		35.2N 137.0E	47636
* 31	102100	32.7N 138.2E	LAND				6//// /////		34.6N 135.7E	47773

32 102200 33.0N 138.2E LAND 65// //// 35.2N 137.0E 4/630 33 102300 33.3N 138.7E LAND 65//4 50735 35.3N 138.7E 47639 34 110000 33.4N 139.4E LAND 55//3 50732 35.3N 138.7E 47639

TYPHOON JOE BEST TRACK DATA

	BEST TRAC	CK		LJA	RN ING				24 1	10UR F	OREC	AST		48 H	IOUR F	OREC	AST		72 H	IOUR F	OREC	AST
						ER	RORS					RRORS					RORS					RRORS
MD/DA/HR	POSIT	WIND	Pt	DSIT	MIND	DST		PC	SIT	WIND			P	DSIT	WIND	DS1	CHIM T	PC	95 I T	MINI	DS'	T WIND
188886Z	8.6 134.1	28	0.0	0.0	0.	-0.	Ø.	8.8	0.0	0.	-0.	Ð.	0.0	0.8	0.	-0.	ð.	Ø.C	0.8	0.	-0.	0.
180812Z	9.5 132.6	28	0.0	8.8	₽.	-0.	0.	8.8	0.0	0.	-0.	ð.	0.0	0.0	0.	-0.	₽.	0.0	0.0	0.	-0.	ø.
100018Z	18.4 131.3	20	8.8	0.0	₽.	-0.	Ð.	6.0	0.0	0.	-0.	₿.	0.0	0.0	0.	-0.	0.	0.0	0.0	e.	-0.	ø.
1009002	11.1 130.2	20	0.0	0.0	₽.	-0.	Ð.	0.8	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	ø.
100906Z	11.6 129.2	20	0.0	0.0	0.	-8.	8.	0.0	0.0	0.	-0.	9.	0.0	0.0	0.	-0.	Ð.	0.0	0.0	0.	-0.	ø.
186912Z	12.0 120.3	20	0.0	0.0	8.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	9.9	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
1889182	12.5 127.4	25	0.0	0.0		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	₽.	0.0	0.0	0.	-0.	ø.
1010002	13.2 126.3	30	0.0	8.8		-0.	е.	6.6	8.8	8.	-8.	8.	0.0	8.8	0.	-0.	9.	8.8	8.8	ø.	-0.	9.
101006Z	14.0 125.1	30	14.0	125.5	30.	23.	8.	15.7	120.9	30.	86.	0.	17.3	117.1	45.	185.	-5.	18.2	113.0	5 5.	145.	-10.
1010122	14.9 123.5	30	15.0	123.5	30.	6.	0.	17.1	110.3	40.	36.	5.	17.5	114.0	50.	51.	0.	18.2	110.0	55.	246.	-10.
101010Z	15.6 122.1	30	15.5	122.3	38.	13.	0.	17.1	118.5	40.	78.	0.	17.5	114.4	50.	87.	-5.	18.1	110.2	55.	264.	5.
101100Z	16.2 120.9	30	15.8	121.4	30.	30.	0.	17.2	117.6	35.	B€.	-10.	17.7	113.4	45.	121.	-15.	17.8	109.2	55.	330.	30.
101106Z	16.4 119.6	38	16.4	119.7	30.	6.	ø.	17.2	114.8	40.	37.	-10.	17.7	110.6	50.	232.	~15.	0.0	0.0	ø.	-0.	ø.
1011122	16.5 118.4	35	16.5	118.7	35.	17.	₽.	17.4	113.7	5 5.	66.	5.	18.6	109.6	65.	243.	0.	0.0	0.0	ø.	-0.	ø.
1011182	16.7 117.2	40	16.7	117.4	40.	11.	0.	17.7	112.5	60.	112.	5.	18.9	100.4	65.	272.	15.	0.0	0.0	ø.	-0.	ø.
101200Z	17.1 116.1	45	17.0	116.0	45.	Θ.	0.	18.2	111.3	60.	163.	0.	19.2	107.2	50.	309.	25.	0.0	9.0	в.	-0.	ø.
101206Z	17.6 115.3	50	17.3	115.4	50.	19.	0.	19.5	111.9	55.	149.	-10.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
1012122	18.2 114.5	50	18.4	114.5	55.	12.	5. 3	22.0	111.9	55.	49.	-10.	0.0	6.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
101210Z	18.9 114.0	55	18.9	113.8	55.	11.	9. 3	21.8	111.7	55.	31.	5.	0.0	0.0	0.	-0.	0.	0.0	8.8	ø.	-8.	0.
101300Z	19.7 1:3.7	60	19.6	113.5	55.	13.	-5.	22.9	113.2	45.	133.	20.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	ø.
1013062	20.6 113.3	65	20.7	113.5	55.	13.	-10.	0.0	0.0	ø.	-0.	0.	0.0	0.0	Ø.	-0.	Ø.	0.0	6.6	ø.	-0.	ø.
1013122	21.5 112.6	65	21.6	112.7	60.	8.	-5.	0.0	0.0	0.	-0.	8.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
101318Z	22.3 111.6	50	22.6	111.9	50.	25.	ø.	0.0	8.0	0.	-0.	ð.	0.0	0.0	0.	-8.	0.	0.0	0.0	ø.	-0.	0.
1014002	23.1 110.8	25	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	6.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	ø.

	ALL	FORECAS	its		TYPHOONS WHILE OVER 35 (
	WRNG	24-HR	48-HR	72-HR	URNG	24-HR	48-HR	72-HR			
AVG FORECAST POSIT ERROR	15.	96.	177.	246 .	14.	81.	159.	218.			
AVG RIGHT ANGLE ERROR	10.	61.	151.	298.	11.	62.	129.	173.			
AVG INTENSITY MAGNITUDE ERROR	2.	7.	10.	14.	3.	6.	θ.	8.			
AVG INTENSITY BIRS	-i.	8.	ø.	4.	-2.	-2.	-4.	-5.			
NUMBER OF FORECASTS	15	12	8	4	10	10	7	3			

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1654. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 12. KNOTS

TYPHOON JOE FIX POSITIONS FOR CYCLONE NO. 15

FIX NO.	TIME FIX (Z) POSITION		ACCRY	DYDRAK CODE	COMMENTS	SITE
* 1	080400	7.2N 131.2E	PCN 6	T1.8/1.0	INIT OBS	PGTW
2	081200	11.3N 130.9E	PCN 6		ULCC FIX	PGT⊎
* 3	090000	13.8N 129.4E	PCH 6	T2.0/2.0 /D1.0/20HR5		PGT₩
* 4	098400	12.7N 130.4E	PCN 6			PGTW
* 5	090653	13.0N 130.1E	PCN 5			PGTW
. 6	090653	11.4N 129.8E	PCH 3	T1.5/1.5		RF11K
* 7	091200	14.9N 127.0E	PCN 6			PGTW
8	092100	13.1H 126.4E	PCN 6		ULCC FIX	PGTW
. 9	092258	12.8N 127.0E	PCN 5			PGTW
10	100000	13.0N 125.5E	PCN 6			PGTW
* 11	100640	13.4N 126.1E	PCN 3	T1.5/1.5 /S0.0/24HRS		RPMK
12	100646	13.5N 126.4E	PCN 5	T2.5/2.5 /D0.5/30HRS		PGTW
13	100956	15.0N 123.2E	PCN 6			PGTW
14	101137	15.5N 122.9E	PCH 5			RODN
15	101137	15.5N 123.0E	PCN 5			RPMK
16	101200	15.0N 123.4E	PCN 6			PGTW
17	101600	15.4H 122.4E	PCN 6			PGTW
18	101800	15.4N 122.2E	PCN 6	T2.0/2.0	INIT OBS	PGTW
19	101925	15.5N 121.7E	PCN 5			PGTW
20	102100	15.7N 121.5E	PCN 6			PGTW
21	102237	15.4N 121.6E	PCN 5	T2.5/2.5 /D1.8/16HRS		RPMK
22	110000	16.0N 120.9E	PCN 6	70.000	**** ***	PGTW
23	110017	16.1H 120.8E	PCN 5	T2.0/2.0	INIT OBS	RODN
24	110627	16.4N 118.7E	PCN 6	T2.8/2.0	INIT OBS	PGTW
25	1111115	16.7N 118.6E	PCN 5			RODH
26	111200	16.4N 118.2E	PCN 6			PGTW

					PGT₩
			T3.0/3.0 /D1.0/24HRS		PGTW
					PGTW
	17.4N 116.6E	PCN 3	T3.0/3.0+/D0.5/24HRS		RPMK
	17.2N 116.5E	PCN 6			PGTW
120300	17.2N 115.8E	PCN 6	T3.5/3.5 /D1.5/21HRS		PGT⊎
120600	17.3N 115.4E	PCN 6			PGTW
120757	17.6N 115.6E	PCN 5	T3.0/3.0	INIT OBS	RODN
120900	17.6N 115.0E	PCN 6			PGTW
121054	17.9N 114.6E	PCN 6			PGTW
121055	18.3N 114.0E	PCN 6		ULCC FIX	RUDH
121200	18.2N 114.3E	PCN 4			PGTW
121600	18.6N 114.2E	PCN 6			PGTW
121800	18.8N 114.2E	PCN 6	T3.5/3.5-/D0.5/24HRS	ULCC FIX	PGTW
122042	19.3N 113.7E	PCN 5			RPMK
122154	19.4N 113.4E	PCN 5			PGTW
122333	19.6N 113.5E	PCN 5	T3.5/3.5 /59.0/21HRS	ULCC FIX	PGTW
130000	19.6N 113.5E	PCN 6			PGTW
130300	20.0N 113.6E	PCN 2			PGTW
130660	20.7N 113.4E	PCN 4			PGTW
130745	20.7N 113.1E	PCN 3	T4.0/4.0	INIT OBS	RPMK
130900	21.1N 113.1E	PCN 2		EYE DIA 12NM	PGTW
131034	21.4N 112.8E	PCN 5		ULCC FIX	RODH
131034	21.4N 112.8E	PCN 5			PGTW
131200	21.7N 112.5E	PCN 6		ULCC FIX	PGTW
131600	22.0N 112.0E	PCN 6		ULCC FIX	PGTW
131800	22.3N 111.8E	PCN 6		ULCC FIX	PGTW
132029	22.8N 111.7E	PCN 5		ULCC FIX	RODN
132100	22.9N 111.5E	PCN 6		ULCC FIX	PGTW
132314	23.2N 111.3E	PCN 6		ULCC FIX	RODH
140000	23.3N 111.1E	PCN 4	T2.0/3.0-/L1.5/24HRS		PGTW
140300	23.7N 110.9E	PCN 6			PGTW
140900	24.6N 110.2E	PCN 6			PGTW
141200	25.1N 110.6E	PCN 6			PGTW
	120757 120900 121054 121055 121200 121600 122604 122042 122154 122333 130000 130306 130306 130306 130306 130306 130306 130306 131030 131030 131030 131030 131030 131030 131030 132314 140300 140300	111800 16.6N 117.0E 112100 16.7N 116.4E 112216 17.4N 116.6E 120000 17.2N 116.5E 120300 17.2N 115.6E 120300 17.3N 115.4E 120300 17.3N 115.6E 120900 17.3N 115.6E 121955 18.3N 114.0E 121955 18.3N 114.0E 121900 18.2N 114.3E 121600 18.6N 114.2E 121600 18.6N 114.2E 121600 19.6N 113.7E 122042 19.3N 113.7E 122042 19.3N 113.6E 130300 20.0N 113.6E 130300 20.0N 113.6E 130900 21.1N 113.1E 130900 21.1N 113.1E 131934 21.4N 112.8E 131934 21.4N 112.8E 131934 21.4N 112.8E 131934 21.4N 112.8E 131934 22.9N 111.5E 131930 22.9N 111.5E	111800 16.6N 117.0E PCN 6 112100 16.7N 116.4E PCN 6 112216 17.4N 116.6E PCN 3 120000 17.2N 116.5E PCN 6 120300 17.2N 115.6E PCN 6 120300 17.3N 115.4E PCN 6 120757 17.6N 115.6E PCN 5 120900 17.3N 115.6E PCN 6 121054 17.9N 114.6E PCN 6 121055 18.3N 114.0E PCN 6 121050 18.2N 114.2E PCN 6 121060 18.2N 114.2E PCN 6 121000 18.2N 114.2E PCN 6 122042 19.3N 113.7E PCN 5 122333 19.6N 113.7E PCN 5 122333 19.6N 113.5E PCN 5 122333 19.6N 113.5E PCN 5 132000 19.5N 113.6E PCN 6 130300 20.0N 113.6E PCN 2 130660 20.7N 113.4E PCN 4 130745 20.7N 113.4E PCN 6 130300 21.1N 113.1E PCN 3 130900 21.1N 113.1E PCN 3 130900 21.1N 113.1E PCN 5 131200 22.9N 111.2.0E PCN 6 131600 22.9N 111.5E PCN 6 131200 22.9N 111.5E PCN 6 132029 22.9N 111.7E PCN 6 132314 23.2N 111.3E PCN 6 1409000 23.3N 111.1E PCN 6 1409000 24.6N 110.9E PCN 6	111808 16.6N 117.0E PCN 6 112108 16.7N 116.4E PCN 6 112216 17.4N 116.6E PCN 3 120000 17.2N 116.5E PCN 6 120300 17.2N 115.8E PCN 6 120300 17.3N 115.4E PCN 6 120757 17.6N 115.6E PCN 5 120900 17.6N 115.0E PCN 6 121055 18.3N 114.0E PCN 6 121055 18.3N 114.0E PCN 6 121200 18.2N 114.3E PCN 6 121200 18.6N 114.2E PCN 6 121200 18.6N 114.2E PCN 6 1212042 19.3N 113.7E PCN 5 122333 19.6N 113.5E PCN 5 122333 19.6N 113.5E PCN 5 130300 20.8N 113.6E PCN 6 130300 20.8N 113.6E PCN 6 130300 20.8N 113.6E PCN 6 130300 21.1N 113.1E PCN 2 130680 21.1N 113.1E PCN 3 130900 21.1N 113.1E PCN 3 130900 21.1N 113.1E PCN 3 131034 21.4N 112.9E PCN 6 131034 21.4N 112.9E PCN 6 131030 22.3N 111.8E PCN 5 131200 22.3N 111.8E PCN 6 132214 23.2N 111.5E PCN 6 132314 23.2N 111.5E PCN 6 140900 23.3N 111.1E PCN 6 140900 24.6N 110.2E PCN 6	111800 16.6N 117.0E PCN 6 T3.0/3.0 /D1.0/24HRS 112100 16.7N 116.4E PCN 6 T3.0/3.0 /D1.0/24HRS 112100 17.4N 116.6E PCN 3 T3.0/3.0 +/D0.5/24HRS 120000 17.2N 116.5E PCN 6 T3.5/3.5 /D1.5/21HRS 120000 17.3N 115.4E PCN 6 T3.5/3.5 /D1.5/21HRS 120000 17.6N 115.6E PCN 6 T3.0/3.0 INIT 005 IN

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT		MAX-SF VEL/BF								EYE SHAPE	EYE ORIEN- DIAM/TATION	-		MP (1	 HO.
* 1		13.1N 126.5E 14.4N 124.8E			1003	30 03 30 14		120										+26 +21	1 2
3	112102	17.8N 116.7E	700MB	2998				160	55	060	65	10	8						 3
4	112325	16.7N 116.1E	700MB	3008	992	40 12	?O 60	230	50	120	55	12	8			+11	+12	+ 8	3
5	120905	18.0N 115.1E	1500FT	2977	988	65 12	20 90	138	43	040	120	15	8				+24	+24	4
6	121056	18.0N 114.5E	1500FT		988	35 02	0 49	228	51	888	60	15	10			+23	+24	+24	4

RADAR FIXES

FIX	TIME	FIX			EYE	EYE	RADOB-CODE		RADAR	SITE
NO.	(2)	POSITION	RADAR	ACCRY	SHAPE	DIAM	ASUAR TODFF	COMMENTS	POSITION	WMD NO.
1	101030	14.9N 123.8E	LAND				1013/ 42702		16.3N 120.6E	98321
2	101200	14.9N 123.7E					1011/ 42505		16.3N 120.6E	98321
3	101300	15.0N 123.5E					1014/ 42907	EYE 60 PCT CIR OPEN E	16.3N 120.6E	98321
4	101330	15.0N 123.4E					10141 42805		16.3N 120.6E	98321
5	101400	15.0N 123.3E					1514/ 42806		16.3N 120.6E	98321
* 6	102300	15.6N 122.1E					40000 ////		16.3N 120.6E	98321
* 7	110030	15.8N 121.7E					1081/ 42916	EYE 80 PCT CIR OPEN N DIA 48KMS	16.3N 120.6E	98321
* 8	110140	16.2N 121.5E					12391 43513	EYE 60 PCT ELLIPTICAL		
* 9	110140	16.1N 120.9E					25/// 42809		16.3N 120.6E	98321
10	110910	16.4N 119.6E					1070/ B29 0 9		16.3N 120.6E	98321
11	111100	16.4N 119.1E					4//// 72708		16.3N 120.6E	98321
12	121150	18.3N 114.6E					22424 73212		16.8N 112.3E	59981
13	122100	19.2N 113.9E					1010/ ////		22.3N 114.2E	45005
14	130100	19.BN 113.9E					209/3 ////		22.3N 114.2E	45005
15	130300	20.1N 113.8E					1081/ 63510		22.3N 114.2E	4500 5
16	1 30 40 0	20.3N 113.7E					1081/ 73511		22.3N 114.2E	45004
17	130650	20.5N 113.5E					12613 53210			59491
18	1 30659	20.9N 113.2E					14612 53312		21.8N 111.9E	59663
19	130750	20.7N 113.3E					12763 53210			59491
20	130759	21.0H 113.2E					14612 53312		21.8N 111.9E	59663
21	130800	20.9N 113.1E					10813 63211		22.3N 114.2E	4500 5
22	130850	21.0N 113.2E	LAND				12713 53210			59491
23	130659	21.2N 113.1E					10422 53312			59491
24	130859	21.1N 113.0E	LAND				3///2 73508		20.0N 110.3E	5975 8
25	130900	21.1N 113.1E					10423 63211		22.3N 114.2E	45005
26	131000	21.2N 112.9E					1041/ 63212		22.3N 114.2E	45005
27	131100	21.2N 112.9E					2086/ 73208		22.3N 114.2E	45005
28	131200	21.3N 112.6E	LAND				1068/ 73108		22.3N 114.2E	45005
29	131300	21.4H 112.7E	LAND				2066/ 73107		22.3N 114.2E	4500 5
30	131400	21.6N 112.5E	LAND				2066/ 83110		22.3N 114.2E	45005
31	131750	22.2N 111.6E	LAND				21541 53209		20. RN 110.3F	59759

SYNOPTIC FIXES

FIX	TIME	FIX	INTENSITY	NEAREST	CONTENTS
NO.	(Z)	POSITION	ESTIMATE	DATA (NM)	
1	131200	21.1N 113.1E	060	050	WMO 59673 40KTS AND 994.9M8 CORRELATES W∕SAT RD
2		21.6N 112.8E	060	020	WMO 59673 60KTS AND 986.4M8
3		22.6N 111.4E	030	020	WMO 59463 10KTS AND 18023

TROPICAL STORM KIM BEST TRACK DATA

	BEST TR	ACK		WA	RHING				24 H	OUR F	ORECA	ST		48 H	IOUR FO	RECAS	ST		72 H	IOUR FI	ORECA!	ST
						ER	RORS				ER	RORS				ERI	RORS				ERI	RORS
MD/DA/HR	POSIT	MINI) PI	DSIT	WIND	DST	WIND	P	351T	WIND	DST	WIND	P09	SIT	WIND	DST	WIND	POS	IT.	WIND	DST	WIND
1014182	10.1 120.3	20	0.0	0.0	0.	~0.	0.	0.0	0.0	0.	-8.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	0.	-0.	0.
1015002	9.3 118.	5 20	0.0	0.0	0.	~0.	0.	0.0	0.0	0.	-0.	B.	0.0	0.0	8.	-0.	a.	0.0	0.0	8.	-8.	e.
1015062	9.3 116.5	20	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	в.
1815122	9.5 115.0	25	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	0.	0.0	0.0	ø.	-0.	e.
101518Z	9.5 114.3	25	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	Ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	0.	-0.	0.
1016002	9.0 112.5	25	0.0	0.0	0.	~0.	0.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	e.	-0.	0.	0.0	0.0	ø.	-0.	Ø.
101606Z	9.1 111.0	3 25	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-8.	0.
1016122	9.8 110.5	3 35	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	8.	-0.	8.
1016182	10.5 109.5	40	10.3	110.3	40.	26.	ø.	11.9	108.2	30.	292.	10.	0.0	0.0	a.	-0.	ø.	0.0	0.0	ø.	-0.	e.
101700Z	11.0 108.0	35	11.2	108.6	35.	37.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	8.0	Ñ.	-0.	ø.	0.0	0.0	ø.	-0.	ø.
1017062	11.6 106.2	2 30	11.5	106.2	30.	6.	ø.	0.0	0.0	ล.	-0.	ø.	0.0	0.0	Ñ.	-0.	ø.	0.0	0.0	ø.	-0.	ø.
1017122	11.9 104.	20	8.8	0.0	ø.	-0.	Ð.	0.0	0.0	ø.	-0.	Đ.	0.0	0.0	ø.	-8.	ø.	0.0	0.0	ø.	-8.	ä.
1017182	12.8 103.3	20	0.0	0.0	ø.	-0.	Ñ.	0.0	0.0	ø.	-0.	A.	0.0	0.0		-0.	ø.	0.0	0.0	ø.	-8.	ø.
1018002	13.6 102.2	20	0.0	0.0	ø.	~ē.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0		-0.	ø.	0.0	0.0	ø.	-0.	Ð.
101806Z	14.2 101.	20	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ø.

	ALL	FORECAS	TS		TYPHO	ONS WHIL	E OVER	35 KTS
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	23.	292.	0.	0.	0.	ø.	0.	ø.
AVG RIGHT ANGLE ERROR	11.	55,	0.	0.	0.	9.	ø.	0.
AVG INTENSITY MAGNITUDE ERROR	0.	10.	0.	0.	ø.	Ø.	0.	0.
AVG INTENSITY BIAS	ø.	10.	0.	0.	8.	ø.	ø.	0.
NUMBER OF FORECASTS	3	1	P	0	Ñ.	Ā.	ā.	Ř.

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1224. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 15. KNOTS

TROPICAL STORM KIM
FIX POSITIONS FOR CYCLONE NO. 16

FIX	TIME	FIX				
NO.	'Z)	POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
					CONTENTS	3116
* i	112188	18 04 170 75	004.6			
* 2	120000	10.8N 139.3E 12.6N 138.5E	PCN 6	T. 0.4 P		PGTW
* 3	120900	12.6N 136.5E	PCN 5	T1.0/1.0	INIT OBS	PGT₩
* 4	130300		PCN 6			PGT₩
* 5		10.0N 132.0E	PCN 6	T1.0/1.0 /S0.0/27HRS		PGT₩
	130600	10.1N 131.0E	PCN 6			PGT⊍
6	141600	10.4N 121.4E	PCN 6			PGTW
7	141880	10.4N 120.6E	PCN 6			PGT⊍
8	142100	9.8N 119.3E	PCN 6			PGTW
.9	150000	9.0N 118.3E	PCN 6			PGTW
10	150300	9.3N 117.9E	PCN 6	T1.0/1.0	INIT OBS	₽GTW
11	150600	9.6N 117.2E	PCN 6			PGTW
12	150900	9.6N 116.7E	PCN 6			PGTW
13	151200	9.3N 116.1E	PCN 6			PGTW
14	151600	9.9N 114.7E	PCN 6	T1.5/1.5	INIT OBS	PGTW
15	151800	9.4N 114.3E	PCN 6			PGTW
16	152100	9.7N 114.0E	PCN 6			PGT⊍
17	160000	9.0N 113.2E	PCN 6			PGT⊎
18	160300	9.1N 112.6E	PCN 6	T2.0/2.0 /D1.0/24HRS		PGTW
19	160600	8.6N 112.3E	PCN 6		ULCC FIX	PGTW
20	160900	9.0N 111.7E	PCN 6		ULCC FIX	PGTW
15	161112	9.6N 111.8E	PCN 5			RODN
22	161200	9.6N 111.2E	PCN 6		ULCC FIX	PGTW
23	161600	9.8N 110.6E	PCH 6	T3.0/3.0 /D1.5/24HRS		PGTW
24	161800	10.3N 110.3E	PCN 6			PGTW
25	161953	10.3N 109.6E	PCN 5		ULCC FIX	RODH
26	162100	10.8N 109.6E	PCN 6		ULCC FIX	PGTW
27	162211	10.9N 108.5E	PCN 5			RPMK
58	162347	10.0N 100.3E	PCN 5		ULCC FIX	RODN
29	170000	11.5N 100.2E	PCN 6			PGTW
30	170300	11.6N 107.0E	PCN 4	T2.5/2.5-/D0.5/24HRS		PGTW
31	178688	11.3N 105.9E	PCN 6		ULCC FIX	PGTW
32	170037	12.1N 105.5E	PCN 5	T2.5/2.5-	INIT OBS	RPMK
33	171200	12.9N 104.8E	PCN 6		ULCC FIX	PGTW
34	171688	12.9N 104.0E	PCH 6		ULCC FIX	PGTW
35	171800	13.2N 103.2E	PCN 6		ULCC FIX	PGTW
36	172100	13.2N 102.8E	PCN 6		- · -··	PGTW
37	186966	13.7N 101.0E	PCN 6			PGTW
38	100300	13.9N 101.3E	PCH 6		ULAC FIX	PGTW
					· • · ·	, 3,0

39 180600 14.5N 100.8E PCN 5

ULCC FIX

PGTW

RADARI FIXES

F'X NC.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB-CODE ASWAR TDDFF	COMMENTS	RADAR POSITION	SITE WMO NO.
1 2 3 4	18 0600 18 0700	13.8N 101.2E 14.0N 101.3E 14.1N 101.0E 14.3N 100.8E	LAND				66/// 42918 66/// 4/// 66/// 42985 6//// ////		13.8M 100.6E 13.8M 100.6E 13.8M 100.6E 13.8M 100.6E	48455 48455 48455 48455

TROPICAL CYCLONE 16-83 BEST TRACK DATA

	BES	T TRA	CK		WA	IRN I NG	ER	RORS					48 H	IOUR FO	RECA!	ST RORS		72 H	IOUR F		ST RORS		
MO/DA/HR	205	IT	WIND	PC	SIT	MIND	DST	WIND	PO	SIT	MIND	DST	WIND	PO	SIT	MIND	DST	WIND	PO	SIT	MIND	DST	MIND
1010122	14.6	99.8	20	0.0	0.0	Ø.	-0.	0.	9.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.
101818Z	14.8	98.4	25	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
101900Z	15.1	96.9	25	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	Ø.	-0.	0.
101906Z	15.9	95.8	30	15.7	95.5	30.	21.	0.	17.2	91.2	35.	161.	10.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
101912Z	16.8	94.9	30	16.8	95.0	30.	6.	0.	20.3	92.0	40.	51.	15.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.
1019182	17.7	94.2	30	17.9	93.7	30.	31.	0.	22.1	91.1	35.	106.	15.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
102000Z	18.3	93.7	25	18.5	94.1	25.	26.	0.	0.0	0.0	0.	-8.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
102006Z	19.1	93.2	25	19.4	94.1	25.	54.	0.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ø.	-0.	0.
1020122	19.9	92.8	25	20.2	93.2	25.	29.	0.	0.0	0.0	ø.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.
102018Z	20.9	92.5	20	0.0	0.0	Ø.	-0.	0.	0.0	0.0	ø.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.

	ALL	FORECAS	TS		TYPHO	ONS WHIL	E OVER	35 KTS
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	28.	106.	0.	0.	0.	0.	0.	0.
AVG RIGHT ANGLE ERROR	25.	96.	8.	0.	0.	0.	0.	0.
AVG INTENSITY MAGNITUDE ERROR	0.	13.	0.	0.	0.	Ð.	0.	0.
AVG INTENSITY BIAS	0.	13.	0.	0.	0.	ø.	0.	0.
NUMBER OF FORECASTS	6	3	0	8	0	9	0	8

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 610. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 11. KNOTS

TC16(W)
FIX POSITIONS FOR CYCLONE NO. 16

SATELLITE FIXES

FIX	TIME	FIX					
NO.	(Z)	POSITIO	DN	ACCRY	DVORAK CODE	COMMENTS	SITE
1	181200		99.8E	PCN 6		ULCC FIX	PGTW
2	101000	14.7N 9	98.3E	PCN 6			PGTW
3	182100		97.6E	PCN 6			PGTW
4	182310	15.7N 9	96.8E	PCN 6	T1.5/1.5	INIT OBS ULAC 15.6N 96.7E	KGWC
5	190000	14.5N 9	96.7E	PCN 6			PGTW
6	190300		96.1E	PCN 6	T2.0/2.0	INIT OBS	PGTW
7	190600		95.8E	PCN 6			PGTW
8	190812		95.6E	PCN 6		ULAC 16.6N 95.6E	KGWC
9	190900		95.6E	PCN 6		ULCC FIX	PGTW
10	191150		94.2E	PCN 6		ULAC 16.6N 94.9E	KGWC
11	191200		94.6E	PCN 6		ULCC FIX	PGT₩
12	191600		93.BE	PCN 6	T1.5/1.5	INIT OBS	PGTW
13	191888		93.5E	PCN 6			PGTW
14	192057		94.BE	PCN 6			KGWC
15	192057		94.2E	PCN 5			RPMK
16	192100		94. 1E	PCN 6			PGT⊍
17	200000		93.7E	PCN 6			PGTW
10	200030		94.5E	PCN 6		ULAC 17.0N 93.6E	KG⊌C
19	200300		94. 1E	PCN 6			PGTW
20	200600		93.8E	PCN 6	T1.0/1.5 /U1.0/27HRS		PGT⊎
21	200900		93.7E	PCN 6			PGTW
22	201130		92.5E	PCN 5			RPMK
23	201200		3.1E	PCN 6			PGT⊍
24	201302		91.9E	PCN 6		EXP LLCC	KGWC
25	201600		92.3E	PCN 6			PGTW
26	202045	21.6N 9	94.4E	PCN 5			RPMK

TYPHOON LEX BEST TRACK DATA

	BEST TRA	CK		LJA:	RNING				24	HOUR	FOREC	AST		48 H	OUR F	ORECA	ST		72 1	AOUR F	ORECA	ST
						ERI	RORS					RRORS					RORS					RORS
MO/DA/HR	POSIT	MIND	PO	SIT	WIND	DST		PC	DSIT	WIN		T WIN	D PI	OSIT	WINI) P(DSIT	WINI		MIND
1022002	16.1 116.8	30	16.4	117.8	30.	21.	0.	17.0	114.5	45.	54.			112.0	50.	97.		17.7		50.		-20.
1022062	16.1 115.5	35	16.3	115.6	30.	13.	-5.	17.3	112.5	40.	92.	-15.	18.0	109.7	35.	215.	-25.	18.6	106.8	35.	225.	-30.
1022122	16.5 114.8	40	16.6	114.8	30.	6.	-10.	17.4	111.4	40.	166.	-15.	18.6	108.2	45.	290.	-15.	20.8	105.7	25.	310.	-40.
1022182	17.2 114.8	45	16.7	114.2	30.	46.	-15.	17.8	111.0	45.	167.	-10.	19.3	100.1	50.	270.	-15.	21.9	106.2	40.	294.	-20.
1023002	17.9 114.6	50	17.9	114.5	35.	6	-15.	19.8	112.4	45.	157.	-10.	21.6	110.0	40.	283.	-30.	0.0	0.0	Ø.	-0.	0.
1023062	17.5 114.1	55	17.6	114.3	45.	13.	-10.	19.5	114.6	48.	143.	-20.	21.4	114.8	40.	346.	-25.	23.3	116.0	35.	632.	-10.
1023122	17.6 114.3	55	17.4	114.6	45.	21.	-10.	18.5	111.9	40.	99.	-20.	20.1	109.9	40.	156.	-25.	0.0	0.0	0.	-0.	0.
1823182	17.5 113.9	55	17.8	113.8	45.	19.	-10.	19.4	112.5	40.	132	~25.	21.5	111.6	40.	274.	-20.	0.0	0.0	Ø.	-0.	ø.
1024002	17.5 113.7	55	17.7	113.7	45.	12.	-10.	19.4	112.5	40.	149.	-30.	21.5	111.6	40.	317.	-15.	0.0	0.0	0.	-0.	0.
1024062	17.4 113.4	60	17.6	112.8	50.	36.	-10.	19.3	111.7	45.	138.	-20.	21.2	111.2	40.	340.	-5.	0.0	0.0	0.	-0.	0.
1024122	17.3 113.1	60	17.4	112.5	50.	35.	-10.	18.2	110.4	45.	51.	-20.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.
1024182	17.2 112.3	65	17.3	112.1	55.	13.	-10.	17.8	110.0	50.	63.	-10.	0.0	0.0	ø.	-0.	Ø.	0.0	0.0	0.	-0.	0.
1025002	17.1 111.5	78	16.8	112.1	68.	39.	-10.	16.4	100.9	55.	104.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1025062	17.3 110.5	65	17.3	110.7	65.	11.	ø.	17.8	100.2	70.	103.	25.	0.0	0.0	8.	-0.	0.	0.0	0.0	0.	-0.	0.
1025122	17.5 109.9	65	17.6	109.8	65.	8.	0.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1025182	17.7 108.9	60	17.7	100.0	65.	6.	5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
1026002	17.7 107.7		-:	107.8	55.	8.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ø.	-0.	0.	0.0	0.0	0.	-0.	0.
1026062	17.8 106.4	45	17.7	106.3	45.	8.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS						
	LIRNG	24-HR	48-HR	72-HR	WRNG	24-HF	4* HR	72-HR			
AVG FORECAST POSIT ERROR	18.	116.	259.	316.	18.	116.	259.	316.			
AVG RIGHT ANGLE ERROR	11.	69.	156.	137.	11.	69.	156.	137.			
AVG INTENSITY MAGNITUDE ERROR	7.	16.	18.	24.	8.	16.	10.	24.			
AVG INTENSITY BIAS	-7.	-13.	-10.	-24.	-7.	-13.	-18.	-24.			
NUMBER OF FORECASTS	19	14	10	5	17	14	10	5			

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 718. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

7. KNOTS

TYPHOON LEX FIX POSITIONS FOR CYCLONE NO. 17

FIX	TIME	FIX				
ND.	(Z)	POSITION	ACCRY	DVBRAK CODE	COMMENTS	SITE
* 1	150600	5.0N 157.4E	PCN 6	T0.0/0.0		PGTW
* 2	150900	4.4N 154.5E	PCN 6	10.0/0.0		PGTW
* 3	151200	4.3N 154.2E	PCN 6			PGTW
* 4	172009	10.2N 138.0E	PCN 5			PGTW
* 5	180000	11.4N 136.9E	PCN 6			PGTW
* 6	180300	12.1N 135.5E	PCN 6			PGTW
7 7	191009	14.6N 129.9E	PCN 6	T1.0/1.0	INIT OBS	PGTW
8	191200	15.2N 129.5E	PCN 6	11.071.0	ULCC FIX	PGTW
9	191600	15.4N 129.3E	PCH 6	T1.5/1.5	INIT OBS	PGTW
19	191800	15.6N 128.7E	PCN 6	11.3/1.3	INTI UBS	PGTW
11	192100	14.9N 127.1E	PCN 6			PGTW
12	192242	14.7N 126.9E	PCN 5			
						PGTW
13	200000 200300	14.6N 126.2E	PCN 6	TI E () E . OO E (17400		PGTW
14		14.8N 125.1E	PCN 6	T1.5/1.5-/D0.5/17HRS		PGTU
15	200618	15.0N 124.5E	PCN 5		ULCC FIX	PGTW
16	200618	14.4N 124.6E	PCN 5	T2.0/2.0	INIT DBS	RPMK
17	200900	14.9N 123.7E	PCN 6		ULCC FIX	PGTW
18	200948	14.8N 123.4E	PCN 5		ULCC FIX	PGTW
19	201200	14.9N 122.8E	PCN 6		ULCC FIX	PGTW
20	201600	15.3N 122.1E	PCN 6	T2.0/2.0-/D0.5/24HRS		PGTW
21	201800	15.1N 121.9E	PCN 6		ULCC FIX	PGTW
22	201903	15.1H 121.6E	PCN 6			PGTW
23	202100	15.1N 121.5E	PCN 6			PGTW
24	202229	15.4N 119.2E	PCN 5	T1.5/1.5+/W0.5/16HRS		RPMK
25	210000	15.2N 120.1E	PCN 4			FGTW
26	210300	14.8N 119.5E	PCN 6	T2.0/2.0+/D0.5/24HRS		PGTW
27	210600	14.9N 118.BE	PCN 6			PGTW
28	210748	16.4N 117.3E	PCN 5	T2.0/2.0 /S0.0/25HRS		RPMK
29	210900	15.4N 118.1E	PCN 6			PGTW
30	211100	15.9N 117.7E	PCN 5			PGTW
31	211100	15.8N 117.9E	PCN 6			RODN
32	211600	16.5N 117.4E	PCN 6	T2.0/2.0 /S0.0/24HRS	ULCC FIX	PGTW
33	211800	16.7N 117.2E	PCN 6		ULCC FIX	PGTW

34	212033	15.5N 117.2E	PCN 5			RPMK
35	212100	15.4N 117.3E	PCN 6		ULCC FIX	PGTW
36	212207	15.8N 117.2E	PCN 5			PGTW
* 37	220000	17.2N 116.9E	PCN 6			PGTW
* 38	220300	17.3N 116.2E	PCN 6	T2.5/2.5 /D0.5/24HRS		PGTW
39	220600	16.3N 115.6E	PCN 4			PGTW
48	220735	16.4N 115.1E	PCN 5	T2.0/2.0 /S0.0/24HRS		RPMK
41	220900	16.4N 115.2E	PCN 6			PGTW
42	221847	16.6N 115.2E	PCN 6		ULCC FIX	RODN
43	221200	16.5N 114.9E	PCN 6		0200 1 17	PGTW
44	221219	16.6N 114.7E	PCN 3			RPMK
45	221600	16.4N 114.7E	PCN 6	T3.0/3.0 /D1.0/24HRS		PGTW
* 46	221800	16.2N 114.7E	PCN 6	13.0/3.0 / 01.0/24/83	ULCC FIX	PGTW
47	222020	18.2N 114.7E	PCN 6		ULCC FIX	RODN
48	222100	17.9N 114.7E	PCN 6		ULCC FIX	PGTW
49	222146	17.8N 114.7E				
			PCN 5	TO E O E OD E (15/105	ULCC FIX	PGTW
* 50	222318	17.0N 115.1E	PCN 5	T2.5/2.5 /D0.5/16HRS		RPMK
51	230000	18.0N 114.6E	PCN 6			PGTW
52	230300	17.8N 114.1E	PCN 4	T3.5/3.5 /D1.0/24HRS		PGTW
53	230600	17.6N 114.3E	PCN 4			PGTW
54	230723	17.6N 114.5E	PCN 3	T3.0/3.0 /D1.0/24HRS		RPMK
55	238900	17.4N 114.0E	PCN 6			PGTW
56	231026	17.5N 114.2E	PCN 4			PGTW
57	231157	17.4N 114.4E	PCN 3			RPMK
58	231200	17.4N 114.0E	PCN 4			PGTW
59	231600	17.5N 113.9E	PCN 6	T3.5/3.5 /D0.5/24HRS	ULCC FIX	PGTW
68	231800	17.8N 113.8E	PCN 6			PGTW
61	232000	17.7N 113.8E	PCN 5			RPMK
62	232100	18.0N 113.5E	PCN 6			PGTW
63	232306	17.9N 113.8E	PCN 4	T3.0/3.0	INIT OBS	RODN
64	232306	17.7N 114.1E	PCN 5	T3.0/3.0 /D0.5/24HRS		RPMK
65	240000	17.2N 113.4E	PCN 6			PGT⊎
66	240037	18.0N 113.5E	PCN 3			RODN
67	240037	17.2N 113.4E	PCN 5	T3.5/3.5 /D0.5/25HRS		RPMK
68	240300	17.5N 113.2E	PCN 6	T4.0/4.0-/D0.5/24HRS		PGTW
69	240600	17.5N 112.8E	PCN 6			PGTW
70	241136	16.9N 113.3E	PCN 3			RODN
71	241136	17.1N 112.9E	PCN 3			RPMK
72	241200	17.2N 112.5E	PCN 6			PGTW
73	241688	17.5N 112.4E	PCN 6	T4.0/4.0 /50.0/13HRS		PGTW
74	241800	17.3N 112.1E	PCN 6			PGTW
75	241955	16.RN 112.3E	PCN 5			RKS0
76	242100	17.2N 111.8E	PCN 6			PGTW
* 77	242245	16.8N 112.4E	PCN 4	T3.5/3.5 /D0.5/24HRS		RODN
78	250000	16.8N 112.8E	PCN 6			PGTW
79	250300	17.3N 111.1E	PCN 4	T4.5/4.5-/D0.5/24HRS		PGTW
80	250658	17.4N 110.4E	PCN 3			PGTW
81	251125	17.6N 189.9E	PCN 3		ULCC FIX	RODN
62	251125	17.8N 110.1E	PCN 4			RPMK
83	251200	17.5N 189.9E	PCN 6			PGTW
84	251600	17.5N 109.3E	PCN 4	T4.5/4.0-/S0.0/24HRS		PGTW
85	251800	17.7N 108.8E	PCN 2			PGTW
86	251943	17.7N 108.7E	PCN 3			RPMK
87	252100	17.9N 108.2E	PCN 4			PGTW
88	252224	17.5N 107.9E	PCN 3	T3.5/3.5 /S0.0/24HRS		RODN
89	252224	17.5N 107.8E	PCH 3	1212-010 - 0010-1-4IKO		RPMK
98	260000	17.7N 107.7E	PCH 4			PGTW
91	260300	17.7N 107.0E	PCN 4	T4.8/4.8-/W0.5/24HRS		PGTW
92	260600	17.7N 106.3E	PCN 4	1310/310 / WO13/ EMIKS		PGTW
93	260900	17.8N 105.8E	PCN 6			PGTW
94	261184	18.1N 105.6E	PCN 5			RODN
95	261233	18.2N 105.5E	PCN 6			RODN
96	261600	18.2N 104.4E	PCN 6	T1.0/2.0 /LB.0/24HRS		PGTW
20	-01000	10.20 104.40	run o	11.0/2.0 /WJ.0/24NR3		FGIW

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL			MAX-FLT-LVL-WND ACCRY DIR/VEL/BRG/RNG NAV/MET	EYE SHAPE	EYE ORIEN- DIAM/TATION			MSN NO.	
ı	228535	16.1N 115.2F	ISABET	1003	35 070 70	150 39 000 00 5 50			+26 +26	32	2	

RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB-CODE ASWAR TODFF	CONMENTS	RADAR POSITION	SITE WHO NO.
	211200	15.7N 124.0E 15.8N 123.9E 16.3N 120.3E 16.5N 120.1E 16.7N 119.9E 16.6N 119.8E 16.8N 119.8E 16.8N 119.5E 16.8N 119.5E	LAND LAND LAND LAND LAND LAND LAND LAND				1031/ 52918 1031/ 52909 15/// 52912 1040/ 52914 1041/ 32914 1041/ 42914 1144/ 43007 15/// 52515	EYE 50 PCT CIR EYE 50 PCT NORTH	16.3N 120.6E 16.3N 120.6E 16.3N 120.6E 16.3N 120.6E 16.3N 120.6E 16.3N 120.6E 16.3N 120.6E 16.3N 120.6E 16.3N 120.6E 16.3N 120.6E	98321 98321 98321 98321 98321 98321 98321 98321 98321
11 12	211330 242350	16.5N 116.3E 17.1N 111.4E					15/// 52514 20744 52906		16.3N 120.6E 16.8N 112.3E	98321 59981

SUPER TYPHOON MARGE BEST TRACK DATA

	BEST TRACK	WARN ING ERRI		HOUR FORECAST ERRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST ERRORS
MO/DA/HR	POSIT WIND		IND POSIT	WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND
1030122		3.0 0.0 00.	9.0 0.0			0.0 0.0 00. 0.
10301BZ		3.0 9.0 00.	0.0 0.0			a.a a.a aa. a.
103100Z		0.0 0.0 00.	0.0 0.0			0.0 0.0 00. 0.
103106Z		3.0 0.0 00.	. 0.0 0.0			8.0 0.0 00. 0.
1031122			15.8 143.7			2.0 151.8 75. 849. ~30.
1031182		2.9 144.6 35. 13.	1. 12.8 143.5			8.2 147.7 75. 650. ~55.
110100Z			5. 12.3 137.6			0.4 137.6 65. 18575.
110106Z	11.8 142.1 35 1		. 14.3 137.0			3.3 141.2 45. 476100.
1101122			. 16.2 137.8			3.7 141.8 45. 52095.
1101182		4.4 141.3 50. 49.	. 19.2 141.5	60. 18715.	22.7 145.5 50, 582, -80, 25	5.0 150.5 45. 990. ~90.
110200Z	14.5 140.6 50 14	4.8 140.3 50. 25.	. 19.5 139.3	65. 15015.	23.3 144.3 55. 59085. 26	5.3 152.5 40.1112. ~90.
1102062	15.3 140,2 65 15	5.5 140.5 65. 21.	9. 19.7 139.5	75. 15915.	23.4 144.4 55. 629. ~90. 26	6.3 152.5 40.1101. ~90.
1102122	16.2 140.2 70 10	5.5 140.0 65. 21. ·	5. 20.8 142.1	65. 32440.	24.0 147.0 55. 78285. 27	7.0 157.6 40.1342. ~85.
1102182	16.6 139.7 75 17	7.0 139.7 70. 24. ·	5. 21.0 140.0	70. 27268.	25.5 145.0 60. 72775 <i>.</i> 28	8.4 154.0 40.1129. ~80.
110300Z	17.0 139.1 80 17	7.0 138.9 75. 11. ·	5. 20.4 137.5	95. 18155.	25.1 140.6 75. 502 <i>.</i> -55. 28	8.3 146.5 50. 688. ~70.
110306Z		7.4 138.1 90. 13.). 19.2 135.1	120. 6125.	22.6 133.1 110. 14120. 26	6.0 137.0 100. 13015.
110312Z	17.6 137.5 105 17	7.6 137.3 100. ll. ·	5. 10.3 133.9	120. 2920.	20.6 130.5 115. 19410. 29	5.0 131.5 105. 457. ~10.
1103182	17.9 136.5 130 16	3.0 136.3 110. 13. –2	9. 19.7 132.5	120. 7915.	22.8 130.5 110. 23010. 27	7.0 133.0 95. 5675.
110400Z		3.2 1 3 5.1 1 40 . 11.	9. 19.6 131.0	160. 147. 30.		5.7 127.1 140.1133. 50.
110406Z		9.5 134.3 145. 21.	9. 20.1 130.2			a.o
110412Z		9.7 134.1 145. 6.	i. 19.5 131.4	140. 174. 15.	22.4 128.3 125. 661. 10. (0.0 0.0 0. -0. 0.
1104182	19.2 133.8 135 19		3. 21.2 130.4			0.0 0.0 0. -0. 0.
110500Z		9.8 133.3 130. 17.	3. 21.8 131.8			0.0 0.0 00. 0 <i>.</i>
1105062		0.3 133.3 130. 17.). 22.4 133.0			0.0 0.0 00. 0.
1105122		1.3 133.7 125. 13.). 25.3 138.0			0.0 0.0 00. 0.
110518Z			5. 25.9 139.2			a.a a.a aa. a.
110600Z			5. 27.2 141.2			a.o
110606Z	23.9 137.6 115 23					9.0 9.0 99. 9.
1106122		5.4 140.1 100. 11				a.o
110618Z		7.8 143.6 90. 6				0.0 0.0 00. 0.
1107002	31.2 148.1 90 3	1.2 149.1 120. 6. 3	9.0 0.0	00. 0.	0.0 0.0 00. 0.	3.0 0.0 00. 0.

	ALL	FORECAS	TS		TYPHO	ONS WHIL	E OVER	35 KTS
	₩RNG	24-HR	48-HR	72-HR	WRNG	24-HR	49-HR	72-HR
AVG FORECAST POSIT ERROR	19.	191.	484.	755.	19.	191.	484.	755.
AVG RIGHT ANGLE ERROR	14.	134.	240.	282.	14.	134.	240.	282.
AVG INTENSITY MAGNITUDE ERROR	6.	18.	36.	63.	6.	18.	36.	63.
AVG INTENSITY BIAS	-1.	-9.	-28.	-56.	-1.	-9.	-28.	-56.
NUMBER OF FORECASTS	27	23	19	15	27	23	19	15

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2370. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 13. KNOTS

SUPER TYPHOON MARGE FIX POSITIONS FOR CYCLONE NO. 18

	IX O.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
	1	290300	4.8N 156.0E	PCN 6	T1.5/1.5	INIT OBS	PGTW
	3	298688	3.8N 155.7E	PCN 6			PGTW
*	3	290900 292100	3.8N 155.2E 2.2N 152.5E	PCN 6 PCN 6		ULCC FIX	PGTW PGTW
~	3	300300	5.9N 151.1E	PCN 6	T1.5/1.5+/S0.0/24HRS	OCCC PIA	PGTW
	6	300600	5.9N 149.5E	PCN 6	11.071.31730.0724103		PGTW
	7	300900	5.5N 149.3E	PCN 6			PGTW
	8	300924	5.5N 149.3E	PCN 5			PGTW
	9	301200	6.7N 149.4E	PCN 6			PGTW
	10	301600	7.0N 148.9E	PCN 6	T2.0/2.0+	INIT OBS ULCC FIX	PGTW
	11	301800	7.4N 148.3E	PCN 6		ULCC FIX	PGTW
	12	302039	7.7N 147.7E	PCN 5			PGTW
	13	302204	7.7N 146.9E	PCH 5			PGTW
	14	310000	7.5N 146.7E	PCN 6			PGTW
寮		310300	7.8N 145.9E	PCN 6		ULCC FIX	PGTW
	16	310544	9.8N 145.8E	PCN 3	T2.5/2.5 /D1.0/28HRS		PGTW
	17	310600	10.5N 145.4E	PCN 4			PGTW
	18	310900	10.6N 144.8E	PCN 6			PGTW
	19	311200	10.7N 144.8E	PCN 6			PGTW
	20	311600	10.9N 144.7E	PCN 6			PGTW
	21	311829	10.9N 144.6E	PCN 6	T3.0/3.0 /D1.0/26HRS		PGTW

26 0.08331 11.49 14.22 PM 57 29 0.1822 12.69 141.22 PM 57 20 0.1822 12.69 14	* 1 2 3 4 5	010640 010949 012100 012344	FIX POSITION 18.0N 141.6E 12.2N 141.8E 12.7N 141.3E 14.1N 140.6E 14.5N 140.3E 15.3N 140.1E	700MB 700MB		VEL /BRG /RNG 50 050 170 30 020 140 45 010 30	MAX-FLT-LVL-LIND ACCRY DIR/VEL/BRG/RNG NAV/MET 118 53 858 178 5 18 158 45 828 148 5 5 010 35 270 38 5 5 110 43 010 30 8 5 300 49 260 35 8 1 200 60 110 48 8 6		EYE TEMP (C) MSN NO. +27 +26 +25 30 23 +11 +18 3 +25 +26 +24 30 4 +25 +27 +23 31 4 +18 +17 +8
27 8 18531 1 1.4 H 42.4E PCN 5 PCN 6 PCN 6 PCN 1						AIRCR	AFT FIXES		
27 818531 11.44 12.45 PCH 5 T2.5-2.5 SODM 28 011926 12.14 14.45 PCH 6 PCH 7 PCH 6 PCH 7 PCH 6 PCH 7 PCH 6 PCH 7 PCH	93 94	070300 070600	33.3N 150.9E 34.8N 152.8E	PCN 6	T3.5/4.5-/	/W1.5/24HRS		PGTW PGTW	
27 818531 1141 1242 PCH 5 72.5-2.5 RODM PCTU PC	91	062254	30.1N 147.7E	PCN 3			- · -	PGTW	
27 8 18531 1 1 1 1 4 12 4 5 PCH 5 PCH 6 PC		062100	29.2N 145.7E	PCN 4	T4.0/4.0		INIT OBS	PGT⊌	
27 818531 11.44 142.46 PCN 5 72.572.5 RODH PCTU PCT		061952	28.2N 144.4E 29.0N 145.2E					PGT⊌	
27 818531 11.44 142.46 PCh 5 72.5/2.5 RODN PGTU PGT	86	061800	27.8N 143.6E	PCN 4	T4.5/5.5-/	/Wd.5/24HRS		PGT₩	
27 818531 11.4 142.46 PCN 5 72.5/2.5 RODH 28 818596 12.1 14.24 PCN 6 PCN 6 PCN 6 PCN 1	84	061200	25.4H 139.9E	PCN 2	T4 5 # 5	40 50400		PGTW	
27 818531 11.4 142.46 PCN 5 72.5/2.5 RODH 28 819596 12.1 N 142.46 PCN 5 PCN 6 PCN 6 PCN 1	82	060853	24.5N 138.4E	PCN 1				₽GTW	
27 618531 11.4 142.4E PCN 5 6 81820 12.1N 142.4E PCN 5 9 611022 12.5 PCN 6 9 FCTU 9 74 8 811020 12.5 N 141.4E PCN 6 9 FCTU 9 74 8 811020 12.5 N 141.4E PCN 6 9 FCTU 9 74 8 811010 13.4 N 141.4E PCN 6 9 FCTU 9 PCN 1 9	80	969399 969611	23.2N 136.3E 23.9N 137.5F	PCN 2 PCN 1				PGT₩	
27 818531 11.4 142.46 PON 5 8 81820 12.1N 142.46 PON 5 9 81820 12.1N 142.66 PON 6 9 86TU 9 81820 12.1N 141.46 PON 4 9 81820 12.5N 141.46 PON 6 9 86TU 9 81820 12.5N 141.46 PON 6 9 86TU 9 81820 12.5N 141.46 PON 6 9 86TU 9 81820 14.5N 140.86 PON 14 9 875.85 PON 14 9 81820 14.5N 140.86 PON 15 9 875.85 PON 15 PO	78	052316	22.5N 135.5E	PCN 1	T4.0/5.0	/W1.0/17HRS		PGTW	
27 818531 1 1.4h 142.4E PCN 5	76	051909	21.9N 134.6E	PCN 1				₽GTW	
27 61853 1.4 142.46 PCN 5 T2.57.2.5 RODN 28 611892 12.1 142.66 PCN 6 PCTU 29 611822 12.6 141.4E PCN 4 PCTU 31 611609 12.0 141.4E PCN 6 T4.87.4 PCTU 31 611609 12.0 141.4E PCN 6 T4.87.4 PCTU 31 611609 13.0 141.4E PCN 6 T4.87.4 PCTU 32 611816 14.44 141.4E PCN 6 T4.87.4 PCTU 33 611935 14.60 141.3E PCN 6 T4.87.4 PCTU 33 611935 14.60 141.3E PCN 6 T4.87.4 PCTU 34 628080 14.50 140.3E PCN 3 T4.87.4 PCTU 36 62819 14.70 133.3E PCN 3 T4.87.4 PCTU 37 628080 15.1 140.4E PCN 2 T4.87.4 PCTU 38 628019 16.20 140.4E PCN 3 T4.87.4 PCTU 40 628036 15.90 140.4E PCN 3 T4.87.4 PCTU 41 621803 16.20 140.4E PCN 3 PCN 3 PCTU 42 621280 16.70 133.5E PCN 6 T5.87.5 PCTU 42 621280 16.70 133.5E PCN 6 T5.87.5 PCN 1 43 621803 17.30 133.5E PCN 1 T5.87.5 PCN 2 PCTU 44 621803 17.30 133.5E PCN 1 T5.87.5 PCN 2 PCTU 45 633696 17.70 133.5E PCN 2 T4.57.4 PCN 2 PCTU 46 633696 17.70 133.5E PCN 2 T4.57.4 PCN 2 PCTU 47 638990 17.70 133.5E PCN 2 T4.57.4 PCN 2 PCTU 48 633696 17.70 133.5E PCN 2 T5.87.5 PCN 2 PCTU 49 633696 17.70 133.5E PCN 2 T5.87.5 PCN 2 PCTU 49 633690 17.70 133.5E PCN 2 T4.57.4 PCN 2 PCTU 40 633690 17.70 133.5E PCN 2 T6.87.5 PCN 2 PCTU 40 633690 17.70 133.5E PCN 2 T7.877.8 PCN 2 PCTU 40 633690 17.70 133.5E PCN 2 T7.877.8 PCN 2 PCTU 40 633690 17.70 133.5E PCN 2 T7.877.8 PCN 2 PCTU 41 62 632100 10.70 133.3E PCN 2 PCN 2 PCTU 42 64000 10.70 133.3E PCN 2 PCN 2 PCTU 43 64000 10.70 133.3E PCN 2 PCN 2 PCTU 44 6400 10.70 133.3E PCN 2 PCN 2 PCTU 45 64000 10.70 133.3E PCN 2 PCN 2 PCTU 46 64000 10.70 133.3E PCN 2 PCN 2 PCTU 47 64000 10.70 133.3E PCN 2 PCN 2 PCTU 48 64000 10.70 133.3E PCN 2 PCN 2 PCN 2	74	05 1600	21.5N 134.2E	PCN 2	T5.0/6.0 /	/W1.0/24HRS			
27 618531 11.4 H 142.4E PCN 5	73	0 51200	21.0N 133.8E	PCN 2				PGT⊌	
27 018531 11.49 142.4E PCN 5	71	050623	20.4N 133.3E	PCN 1			INIT OBS INIT OBS	RPMK	
27 8 18531 11.4N 42.6E PCN 5 72.5/2.5 RODN 28 8 18999 12.1N 142.6E PCN 6 PCTU 29 8 11822 12.6N 141.4E PCN 6 PCTU 31 8 11609 13.4N 141.4E PCN 6 PCTU 31 8 11609 13.4N 141.4E PCN 6 PCTU 33 8 11956 14.6N 141.3E PCN 6 PCTU 33 8 11956 14.6N 141.3E PCN 7 35 9 12382 14.6N 140.5E PCN 3 PCTU 36 0 22080 14.6N 140.5E PCN 2 T4.8/4.8 DCN 7 37 0 28390 15.1N 140.4E PCN 2 T4.8/4.8 DCN 7 38 0 2255 15.NN 139.6E PCN 3 T4.8/4.8 DCN 7 41 821881 16.2N 140.6E PCN 4 PCN 4 41 821881 16.2N 140.6E PCN 5 T4.8/4.8 DCN 7 42 821280 16.7N 140.5E PCN 6 T5.8/5.8-/D1.8/24RS EYE DIA 38NM RPYK 48 0 22240 17.1N 139.5E PCN 1 T5.8/5.8-/D1.8/24RS EYE DIA 38NM RPYK 49 0 338680 17.3N 139.5E PCN 1 T5.8/5.8-/D1.8/24RS EYE DIA 38NM RPYK 40 0 22240 17.1N 139.5E PCN 1 T5.8/5.8-/D1.8/24RS EYE DIA 38NM RPYK 49 0 338680 17.3N 139.5E PCN 2 T4.5/4.5 PCTU 40 0 338680 17.3N 139.5E PCN 2 T4.5/4.5 PCTU 40 0 338680 17.3N 139.5E PCN 2 T5.8/5.8-/D1.8/24RS EYE DIA 38NM RPYK 40 0 338680 17.3N 139.5E PCN 2 T5.8/5.8-/D1.8/24RS EYE DIA 38NM RPYK 40 0 338680 17.3N 139.5E PCN 2 T5.8/5.8-/D1.8/24RS EYE DIA 38NM PCTU 50 0 338680 17.3N 137.5E PCN 2 T5.8/5.8-/D1.8/24RS EYE DIA 36NM PCTU 51 0 338080 17.3N 137.5E PCN 2 T7.8-/D2.5/24RS EYE DIA 36NM PCTU 52 0 44200 18.3N 134.5E PCN 2 T7.8-/D2.5/24RS EYE DIA 36NM PCTU 53 0 441600 19.3N 133.5E PCN 2 T6.8/6.8-/D2.5/24RS EYE DIA 36NM PCTU 54 0 441200 18.7N 134.5E PCN 2 T6.8/6.8-/D2.5/24RS EYE DIA 36NM PCTU 55 0 441200 18.7N 134.5E PCN 2 T6.8/6.8-/D2.5/24RS EYE DIA 36NM PCTU 56 0 441200 18.7N 134.5E PCN 2 T6.8/6.8-/D2.5/24RS EYE DIA 36NM PCTU 56 0 441200 18.7N 134.5E PCN 2 T6.8/6.8-/S8.8/24RS EYE DIA 36NM PCTU 56 0 441200 18.7N 134.5E PCN 2 T6.8/6.8-/S8.8/24RS PCN 2	69	05060 0	20.3N 133.5E	PCN 2		/wii .5/24HRS	THEY MAN	PGTW	
27	67	85888 8	19.7N 133.3E	PCN 2				PGTW	
27	65	842100	19.6N 133.5E	PCN 2				PGTW	
27	63	041600	19.2N 133.7E	PCN 2	T6.0/6.0-/	/S0.0/24HRS	EYE DIA 36NM	PGT₩	
27 818531 11.4M 142.4E PCN 5 T2.5/2.5 RODM 28 818990 12.1M 142.9E PCN 6 PCN 6 29 811822 12.6N 141.4E PCN 6 30 11280 12.8N 141.4E PCN 6 31 811602 13.4M 141.4E PCN 6 31 811602 13.4M 141.4E PCN 6 32 811815 14.4M 141.4E PCN 6 33 811956 14.6N 141.3E PCN 6 34 812302 14.5N 144.3E PCN 6 34 812302 14.5N 148.9E PCN 3 35 812302 14.5N 148.9E PCN 3 36 8289600 14.6N 148.4E PCN 2 37 828300 15.1M 148.1E PCN 2 38 828519 14.7M 139.9E PCN 3 39 828519 15.3M 139.9E PCN 3 30 828519 15.3M 139.9E PCN 3 40 828935 15.9M 148.9E PCN 3 41 821803 16.9M 139.5E PCN 6 42 821803 16.9M 139.5E PCN 6 43 821803 16.9M 139.5E PCN 6 45 822180 17.8M 139.9E PCN 6 45 822180 17.8M 139.9E PCN 2 47 8389600 17.1M 139.9E PCN 2 48 838580 17.7M 139.9E PCN 2 49 838580 17.7M 139.9E PCN 2 49 838580 17.7M 138.9E PCN 2 49 838580 17.7M 138.9E PCN 2 49 838580 17.7M 138.9E PCN 2 51 838990 17.7M 137.9E PCN 2 51 838990 17.7M 137.9E PCN 2 52 831280 17.7M 137.9E PCN 2 53 831680 17.7M 137.9E PCN 2 54 831880 17.7M 137.9E PCN 2 55 832180 18.6M 135.5E PCN 2 57 848090 18.7M 137.9E PCN 2 58 848300 18.3M 133.9E PCN 2 59 848090 18.7M 135.5E PCN 2 59 848090 18.7M 135.5E PCN 2 59 848090 18.3M 134.9E PCN 2 50 502180 18.3M 134.9E PCN 2 50 5032180 18.3M 134.9E PCN 2 50 503218	61	041058	18.8N 134.5E	PCN 1				RPMK	
27 818531 11.4N 142.4E PCN 5 72.5.5 RODN 28 018980 12.1N 142.8E PCN 6 PCTU 29 011922 12.6N 141.4E PCN 6 PCTU 310 011200 12.9N 141.4E PCN 6 PCTU 310 011200 12.9N 141.4E PCN 6 PCTU 310 011200 13.4N 141.4E PCN 6 PCTU 310 011200 14.4N 141.4E PCN 6 PCTU 310 011200 14.4N 141.4E PCN 6 PCTU 310 011200 14.4N 141.4E PCN 6 PCN 1 PCTU 310 011200 14.5N 140.8E PCN 3 PCN 3 PCTU 310 011200 15.1N 140.1E PCN 2 PCN 3 PCTU 310 011200 15.1N 140.1E PCN 2 PCN 3 PCTU 311 011200 15.1N 140.4E PCN 3 PCN 3 PCTU 411 02100 16.7N 139.8E PCN 3 PCN 3 PCTU 411 02100 16.7N 140.3E PCN 6 PCN 4 PCTU 412 021200 16.7N 140.3E PCN 6 PCN 4 PCTU 413 02100 16.7N 140.3E PCN 6 PCN 4 PCTU 414 02100 16.7N 140.3E PCN 6 PCN 6 PCTU 415 021200 17.1N 139.8E PCN 6 PCN 6 PCTU 416 021200 17.1N 139.5E PCN 6 PCN 6 PCTU 417 02100 17.1N 139.5E PCN 6 PCN 6 PCTU 418 030300 17.3N 139.6E PCN 2 PCN 6 PCTU 419 030300 17.3N 139.6E PCN 2 PCN 6 PCTU 42 031000 17.3N 139.6E PCN 2 PCN 6 PCTU 43 031000 17.3N 139.6E PCN 2 PCN 6 PCTU 44 031000 17.3N 139.6E PCN 2 PCN 6 PCTU 45 032240 17.1N 139.9E PCN 2 PCTU 46 032240 17.1N 139.9E PCN 2 PCTU 47 033000 17.3N 139.6E PCN 2 PCN 2 PCTU 48 033000 17.3N 139.6E PCN 2 PCN 2 PCTU 49 033000 17.3N 139.6E PCN 2 PCN 2 PCTU 50 033000 17.3N 139.6E PCN 2 PCN 2 PCTU 51 033000 17.3N 139.6E PCN 2 PCN 2 PCTU 52 031200 17.7N 137.8E PCN 2 PCTU 53 031600 17.9N 135.6E PCN 2 PCTU 54 031000 18.1N 135.9E PCN 2 PCTU 55 032100 18.1N 135.9E PCN 2 PCTU 56 032210 18.1N 135.9E PCN 2 PCTU 57 040000 18.2N 135.3E PCN 2 PCN 2 PCTU 57 040000 18.2N 135.3E PCN 2 PCN 2 PCTU 57 040000 18.2N 135.3E PCN 2 PCN 2 PCTU 57 040000 18.2N 135.3E PCN 2 PCN 2 PCTU 57 040000 18.2N 135.3E PCN 2 PCN 2 PCTU	59	040600	18.5N 134.5E	PCN 2	17.077.0-/	/ UZ . 3/24MRS		PGT₩	
27 818531 11.4M 142.4E PCN 5 T2.5/2.5 RODH 28 818988 12.1N 142.0E PCN 6 PCN 4 38 811208 12.6N 141.2E PCN 6 39 811920 12.8N 141.2E PCN 6 31 811508 13.4N 141.4E PCN 6 31 811508 13.4N 141.4E PCN 6 32 811816 14.4N 141.4E PCN 6 33 811956 14.6N 141.3E PCN 6 34 812382 14.6N 148.5E PCN 3 35 812382 14.5N 140.8E PCN 3 36 826808 15.1N 140.1E PCN 2 37 826308 15.1N 140.1E PCN 2 37 826308 15.1N 140.1E PCN 2 38 826519 14.7N 133.9E PCN 3 39 826519 15.3N 133.9E PCN 3 40 826636 15.9N 140.8E PCN 3 41 821801 16.2N 140.4E PCN 3 42 821208 16.7N 140.3E PCN 6 43 821208 16.7N 140.3E PCN 6 44 821803 16.9N 139.5E PCN 6 45 822240 17.1N 138.9E PCN 6 46 822240 17.1N 138.9E PCN 1 47 838080 17.3N 138.5E PCN 2 48 838308 17.3N 138.5E PCN 2 49 838566 17.3N 138.5E PCN 2 51 838980 17.3N 138.5E PCN 2 51 838980 17.3N 138.5E PCN 2 52 831200 17.7N 137.0E PCN 2 53 831600 17.9N 137.0E PCN 2 54 831800 17.7N 137.0E PCN 2 55 831800 17.7N 137.0E PCN 2 56 831800 17.7N 137.0E PCN 2 57 831800 17.7N 137.0E PCN 2 58 831800 17.7N 137.0E PCN 2 59 631800 17.7N 137.0E PCN 2 50 631800 17.7N 137.0E PCN 2 51 831800 17.7N 137.0E PCN 2 52 831800 17.7N 137.5E PCN 2 54 831800 17.7N 137.5E PCN 2 55 831800 17.7N 137.5E PCN 2 56 831800 17.7N 137.5E PCN 2 57 631800 17.7N 137.5E PCN 2 58 831800 17.7N 137.5E PCN 2 59 631800 17.7N 137.5E PCN 2 50 631800 17.7N 137.5E PC	57	040000	18.2N 135.3E	PCN 2	77.00			PGTW	
27 918531 11.4M 142.4E PCN 5 T2.5/2.5 RODN 28 918908 12.1H 142.0E PCN 6 PCTU 29 911802 12.6N 141.4E PCN 4 PGTU 30 911802 12.6N 141.4E PCN 6 PGTU 31 911806 13.4M 141.4E PCN 6 T4.8/4.8 /D1.8/22HRS PGTU 32 911816 14.4M 141.4E PCN 6 T4.8/4.8 /D1.8/22HRS PGTU 33 911956 14.6N 143.5E PCN 6 PGTU 33 912302 14.5N 140.8E PCN 3 T4.8/4.8 /D1.5/24HRS PGTU 34 912302 14.5N 140.8E PCN 3 T4.8/4.8 /D1.5/24HRS PGTU 37 929309 15.1M 140.1E PCN 2 T4.8/4.8 /D1.5/24HRS EYE DIA 28NM PGTU 38 928519 15.3M 139.8E PCN 3 T4.8/4.8 /D1.5/24HRS PGTU 40 928036 15.9M 140.8E PCN 3 PGTU 41 921209 16.7M 140.8E PCN 4 PCN 4 42 921209 16.7M 140.3E PCN 6 PCN 6 43 921209 16.7M 140.3E PCN 6 44 921903 16.9M 139.5E PCN 6 45 922248 17.1M 139.9E PCN 1 T5.8/5.8-/D1.8/24HRS EYE DIA 38NM RPPK 47 939090 17.1M 139.9E PCN 1 T5.8/5.8-/D1.8/24HRS EYE DIA 38NM RPPK 48 939506 17.2M 139.3E PCN 1 T5.8/5.8-/D1.8/24HRS EYE DIA 38NM RPPK 49 939506 17.7M 137.3E PCN 2 PGTU 50 939500 17.7M 137.3E PCN 2 PGTU 51 939900 17.7M 137.3E PCN 2 PGTU 52 931200 17.7M 137.3E PCN 2 PGTU 53 931200 17.7M 137.3E PCN 2 PGTU 53 931200 17.7M 137.3E PCN 2 PGTU 54 939900 17.7M 137.3E PCN 2 PGTU 55 931200 17.7M 137.3E PCN 2 PGTU 55 931200 17.7M 137.3E PCN 2 PGTU 56 913600 16.7M 137.3E PCN 2 PGTU 57 931200 17.7M 137.3E PCN 2 PGTU 58 931200 17.7M 137.3E PCN 2 PGTU 59 931200 17.7M 137.3E PCN 2 PGTU 50 931200 17.7M 137.3E PCN 2 PGTU 59 931200 17.7M 137.3E PCN 2 PGTU 50 931200 17.7M 137.3E PCN 2 PGTU	55	832100	18.1N 135.8E	PCN 2				PGTW	
27 918531 11.4N 142.4E PCN 5 T2.5/2.5 RODN 28 019900 12.1N 142.0E PCN 6 PGTU 30 011020 12.6N 141.4E PCN 6 PGTU 31 011600 13.4N 141.4E PCN 6 T4.0/4.8 /D1.0/22HRS PGTU 32 011016 14.4N 141.4E PCN 6 PGTU 33 011016 14.4N 141.4E PCN 6 PGTU 33 011016 14.4N 141.4E PCN 6 PGTU 33 011016 14.6N 141.3E PCN 6 PGTU 34 012302 14.5N 140.8E PCN 3 PGTU 35 012302 14.5N 140.8E PCN 3 PGTU 36 020000 14.6N 140.4E PCN 2 PGN 3 PGTU 38 020519 14.7N 139.8E PCN 3 T4.0/4.8 /D1.5/24HRS EYE DIA 20NM PGTU 40 020300 15.1N 140.1E PCN 2 PGN 3 PGTU 41 021001 16.2N 140.4E PCN 3 PGTU 42 021200 16.7N 140.3E PCN 6 PGN 3 PGTU 43 021003 16.9N 139.5E PCN 6 PGN 6 PGN 6 PGN 6 PGN 6 PGTU 44 021003 16.9N 139.5E PCN 6 PGN 6 PGN 6 PGN 6 PGN 6 PGN 7 PGTU 45 022400 17.1N 130.9E PCN 6 PGN 6 PGN 7 PGTU 46 022240 17.1N 130.9E PCN 1 T5.0/5.8-/D1.0/24HRS EYE DIA 30NM RPYK 47 030000 17.1N 130.9E PCN 2 PGN 1 T5.0/5.8-/D1.0/24HRS PGTU 49 030000 17.1N 130.9E PCN 2 PGN 1 T5.0/5.8-/D1.0/24HRS PGTU 49 030000 17.1N 130.9E PCN 2 PGN 1 T5.0/5.8-/D1.0/24HRS PGTU 49 030000 17.1N 130.9E PCN 2 PGN 1 T5.0/5.8-/D1.0/24HRS PGTU 49 030000 17.1N 130.9E PCN 2 PGN 1 T5.0/5.8-/D1.0/24HRS PGTU 49 030000 17.1N 130.9E PCN 2 PGN 1 T5.0/5.8-/D1.0/24HRS PGTU 49 030000 17.1N 130.9E PCN 2 PGN 1 T5.0/5.8-/D1.0/24HRS PGTU 49 030000 17.1N 130.9E PCN 2 PGN 1 T5.0/5.8-/D1.0/24HRS PGTU 49 030000 17.1N 130.9E PCN 2 PGN 1 T5.0/5.8-/D1.0/24HRS PGTU 49 030000 17.1N 130.9E PCN 2 PGN 1 T5.0/5.8-/D1.0/24HRS PGTU 49 030000 17.1N 130.9E PCN 2 PGN 2 PGN 1 T5.0/5.8-/D1.0/24HRS PGTU 49 030000 17.1N 130.9E PCN 2 PGN 1 T5.0/5.8-/D1.0/24HRS PGTU 49 030000 17.1N 130.9E PCN 2 PGN 2 PGN 2 PGTU 49 030000 17.1N 130.9E PCN 2 PGN 1 T5.0/5.8-/D1.0/24HRS PGTU 49 030000 17.1N 130.9E PGN 2 PG	53	031600	17.9N 136.6E	PCN 2	T6.0/6.0-/	/D1.0/24HRS		PGTW	
27 818531 11.4H 142.4E PCH 5 T2.5/2.5 RODH 28 018980 12.1N 142.0E PCH 6 PCH 4 29 018980 12.1N 142.0E PCH 6 29 018980 12.2N 141.4E PCH 6 30 011820 12.6N 141.4E PCH 6 31 011600 13.4M 141.4E PCH 6 32 011816 14.4M 141.4E PCH 5 33 011956 14.6N 141.3E PCH 6 34 012382 14.6N 140.5E PCH 3 35 012382 14.6N 140.5E PCH 3 36 020000 14.6N 140.8E PCH 3 37 020380 15.1N 140.1E PCH 2 37 020380 15.1N 140.1E PCH 2 38 020519 14.7N 139.9E PCH 3 39 020519 15.3N 139.9E PCH 3 40 020036 15.9H 140.4E PCH 3 40 021001 16.2N 140.4E PCH 3 41 021001 16.2N 140.4E PCH 3 42 021200 16.7N 140.3E PCH 6 43 021600 16.9H 139.5E PCH 6 44 021003 16.9N 139.5E PCH 6 45 022240 17.1N 139.9E PCH 4 46 022240 17.1N 139.9E PCH 2 47 030000 17.3N 139.9E PCH 2 48 030300 17.3N 139.9E PCH 2 49 030300 17.3N 139.9E PC	51	030900	17.7N 137.8E	PCN 2			EYE DIA 18NM	PGTW	
27 818531 11.4N 142.4E PCN 5 T2.5/2.5 RODN 28 618988 12.1N 142.0E PCN 6 PCTU 38 618988 12.1N 142.2E PCN 6 PCTU 38 611826 12.6N 141.4E PCN 6 PCTU 38 611206 12.8N 141.4E PCN 6 PCTU 31 611606 13.4N 141.4E PCN 6 PCTU 32 811816 14.4N 141.4E PCN 5 PCTU 33 811956 14.6N 141.3E PCN 6 PCTU 34 612302 14.6N 148.5E PCN 3 PCTU 35 628080 14.5N 148.8E PCN 3 T4.8/4.8 PCN 3 PCTU 37 628308 15.1N 148.1E PCN 2 PCN 3 T4.8/4.8 PCN 3 PCTU 38 828519 14.7N 139.8E PCN 3 T4.8/4.8 PCN 3 PCTU 40 828036 15.9N 148.4E PCN 3 PCN 3 PCTU 41 821608 16.7N 148.3E PCN 6 PCN 3 PCTU 42 821280 16.7N 148.3E PCN 6 PCN 3 PCTU 43 821608 16.9N 139.5E PCN 6 PCN 3 PCTU 44 821608 16.9N 139.5E PCN 6 PCN 6 PCTU 45 822180 16.7N 148.3E PCN 6 PCN 7 PCTU 46 822248 17.1N 138.9E PCN 6 PCN 1 T5.8/5.8-/D1.8/24HRS EYE DIA 38NM RPMK 47 838688 17.1N 138.9E PCN 2 PCTU	49	030506	17.2N 138.2E	PCN 1			EYE DIA 18NM	RODN	
27 818531 11.4N 142.4E PCN 5 T2.5/2.5 RODN 28 818980 12.1N 142.0E PCN 6 PCTU 30 811820 12.8N 141.2E PCN 6 PGTU 31 811860 13.4N 141.4E PCN 6 T4.8/4.8 /D1.8/22HRS 32 811816 14.4N 141.4E PCN 6 PGTU 33 811816 14.4N 141.4E PCN 6 PCN 1 PGTU 34 812392 14.6N 148.5E PCN 3 PGTU 35 8269080 14.6N 148.5E PCN 3 T4.8/4.8 /D1.5/24HRS 36 8269080 14.6N 148.4E PCN 2 PGTU 37 826390 15.1N 148.1E PCN 2 T4.8/4.8 /D1.5/24HRS EYE DIA 28NM PGTU 38 8269519 15.3N 133.9E PCN 3 T4.8/4.8 /D1.5/24HRS 40 826963 15.9N 148.0E PCN 3 T4.8/4.8 /D1.5/24HRS 41 821881 15.9N 148.0E PCN 3 PGTU 42 821880 16.7N 148.3E PCN 6 ULCC FIX PGTU 43 821880 16.9N 139.6E PCN 6 T5.8/5.8-/D1.8/24HRS 44 821880 16.9N 139.5E PCN 6 T5.8/5.8-/D1.8/24HRS 45 822100 17.8N 139.5E PCN 6	47	030000	17.1N 138.9E	PCN 2				PGTW	
27 818531 11.4N 142.4E PCN 5 T2.5/2.5 RODN 28 018930 12.1N 142.0E PCN 6 PGTU 30 011020 12.6N 141.4E PCN 6 PGTU 31 011020 12.9N 141.2E PCN 6 PGTU 32 011816 14.4N 141.4E PCN 6 T4.8/4.8 /D1.8/22HRS PGTU 33 011956 14.6N 141.3E PCN 6 PGTU 34 012302 14.6N 140.5E PCN 3 PGTU 35 012302 14.6N 140.5E PCN 3 PGTU 37 020300 15.1N 140.1E PCN 2 T4.8/4.8 /D1.5/24HRS EYE DIA 20NM PGTU 38 020519 14.7N 139.0E PCN 3 T4.8/4.8 /D1.5/24HRS EYE DIA 20NM PGTU 40 020036 15.9N 140.0E PCN 4 PGTU 41 021001 16.2N 140.3E PCN 6 ULCC FIX PGTU 42 021200 16.7N 140.3E PCN 6 T5.8/5.8-/D1.8/24HRS PGTU	45	022100	17.0N 139.2E	PCN 4	T5.0/5.0-/	/D1.8/24HRS	EYE DIA 38NM	PGT₩	
27 818531 11.4N 142.4E PCN 5 T2.5/2.5 RODN 28 618988 12.1N 142.0E PCN 6 PCTU 39 611826 12.6N 141.4E PCN 4 PGTU 30 611206 12.8N 141.4E PCN 6 PGTU 31 611606 13.4N 141.4E PCN 6 PGTU 31 611606 13.4N 141.4E PCN 6 PGTU 32 611816 14.4N 141.4E PCN 5 PGTU 33 611956 14.6N 141.3E PCN 6 PGTU 34 612302 14.6N 140.5E PCN 3 PGTU 35 612302 14.5N 148.8E PCN 3 T4.8/4.8 INIT OBS RPINK 36 626080 14.5N 148.8E PCN 2 PGTU 37 626308 15.1N 148.1E PCN 2 T4.8/4.8 /D1.5/24HRS EYE DIA 28NM PGTU 38 626519 14.7N 139.8E PCN 3 T4.8/4.8 /D1.5/24HRS PGTU 49 626086 15.9N 140.0E PCN 3 PGTU 40 626086 15.9N 140.0E PCN 3 PGTU 41 621081 16.2N 140.4E PCN 3 PGTU	43	021600	16.8N 139.6E	PCN 6	T5.0/5.0-/	/D1.0/24HRS	· • · ·	PGTW	
27 818531 11.4N 142.4E PCN 5 T2.5/2.5 RODN 28 018980 12.1N 142.0E PCN 6 PGTU 30 011820 12.6N 141.4E PCN 6 PGTU 31 011600 13.4N 141.4E PCN 6 T4.8/4.8 /D1.8/22HRS PGTU 32 011816 14.4N 141.4E PCN 6 PGTU 33 011956 14.6N 141.3E PCN 6 PGTU 34 012302 14.6N 148.5E PCN 3 35 012302 14.6N 148.5E PCN 3 36 020000 14.6N 140.4E PCN 2 PGTU 37 020300 15.1N 140.4E PCN 2 PGTU 38 020519 15.3N 133.0E PCN 3 T4.8/4.8 /D1.5/24HRS EYE DIA 20NM PGTU 39 020519 15.3N 133.0E PCN 3 PGTU	41	021001	16.2N 140.4E	PCN 3			ULCC FIX	PGTW	
27 818531 11.4N 142.4E PCN 5 T2.5/2.5 RODN 28 018900 12.1N 142.0E PCN 6 PGTU 30 011920 12.6N 141.4E PCN 6 PGTU 31 011600 13.4N 141.4E PCN 6 PGTU 32 011816 14.4N 141.4E PCN 6 T4.8/4.8 /D1.8/22HRS PGTU 33 011956 14.6N 141.3E PCN 6 PGTU 34 012302 14.6N 140.5E PCN 3 PGTU 35 012302 14.5N 140.8E PCN 3 T4.8/4.8 INIT OBS RPHK 36 020000 14.6N 140.4E PCN 2 PGTU 37 020300 15.1N 140.1E PCN 2 T4.8/4.8 /D1.5/24HRS EYE DIA 20NM PGTU	39	828519	15.3N 139.BE	PCN 3	1.110			PGTW	
27 818531 11.4N 142.4E PCN 5 T2.5/2.5 RODN 28 018980 12.1N 142.0E PCN 6 PCN 4 29 018920 12.5N 141.4E PCN 4 38 011820 12.8N 141.4E PCN 6 31 011600 13.4N 141.4E PCN 6 T4.8/4.0 /D1.8/22HRS 32 011816 14.4N 141.4E PCN 5 33 011956 14.6N 141.3E PCN 6 34 012302 14.6N 141.3E PCN 6 35 012302 14.6N 140.8E PCN 3 36 012302 14.5N 140.8E PCN 3 37 012302 14.5N 140.8E PCN 3 38 012302 14.5N 140.8E PCN 3 39 012302 14.5N 140.8E PCN 3 30 012302 14.5N 140.8E PCN 3 30 012302 14.5N 140.8E PCN 3 31 012302 14.5N 140.8E PCN 3	37	020300	15.1N 140.1E	PCN 2			EYE DIA 20NM	PGTW	
27 818531 11.4N 142.4E PCN 5 T2.5/2.5 RODN 28 018980 12.1N 142.0E PCN 6 PGTU 29 011802 12.6N 141.4E PCN 6 PGTU 30 011200 12.9N 141.2E PCN 6 PGTU 31 011600 13.4N 141.4E PCN 6 T4.8/4.8 /D1.0/22HRS PGTU 32 011816 14.4N 141.4E PCN 6 T4.8/4.8 /D1.0/22HRS PGTU 33 011956 14.6N 141.3E PCN 6 PGTU	35	012302	14.5N 140.8E	PCH 3	T4.0/4.8		INIT OBS	RPMK	
27 010531 11.4N 142.4E PCN 5 T2.5/2.5 RODN 28 010900 12.1N 142.0E PCN 6 PGTW 29 011022 12.6N 141.4E PCN 4 PGTW 30 011200 12.8N 141.2E PCN 6 PGTW 31 011600 13.4N 141.4E PCN 6 T4.0/4.0 /D1.0/22HRS PGTW	3 3	011956	14.6N 141.3E	PCN 6				PGTW	
27 818531 11.4N 142.4E PCN 5 T2.5/2.5 RODN 28 818988 12.1N 142.8E PCN 6 PGTW 29 811822 12.6N 141.4E PCN 4 PGTW	31	01160 0	13.4N 141.4E	PCN 6	T4.8/4.8	/D1.0/22HRS		PGT⊎	
27 818531 11.4N 142.4E PCN 5 T2.5/2.5 RODN	29	011022	12.6N 141.4E	PCN 4				PGTW	
26 010531 11.4N 142.2E PCN 5	27	010531	11.4N 142.4E	PCN 5	T2.5/2.5			RODN	
25 010300 10.5N 142.6E PCN 6 T2.5/2.5 /S0.0/21HRS ULCC FIX PGTW	25	010300	10.5N 142.6E	PCN 6	T2.5/2.5	/S0.0/21HRS	ULCC FIX		
22 312017 18.9N 143.9E PCN 5 PGTU 23 312143 11.1N 143.6E PCN 5 PGTU * 24 010000 18.1N 142.7E PCN 6 PGTU	23	312143	11.1N 143.6E	PCN 5				PGTW	

9	022331	17.0N 138.9E	700MB	2793	964	60 3	10 16	23	80.4	97	140	12	5	1	ELLIPTICAL	35	25	360	+10	+18	+ 8	ć
10	030552	17.3N 138.2E	700MB	2665	949	90 0				98 6		30	10	ż					+15	+19	+17	i
11	030833	17.6N 137.8E	700MB	2575	940	50 3		9 19	90	92 6	080	25	10	3	CIRCULAR	15			+12	+19	+ 9	છ
12	031105	17.6N 137.5E	700MB	2507				30	50	91 2	290	30	10	3								6
13	032031	18.1N 135.8E	700MB	2266		130 3	60 9	10	90 1	13 3	350	29	10	10	CIRCULAR	21			+12	+21	+14	9
14	032347	18.2N 135.2E	700MB	2187	897	130 1		2	20 1	36	190	5	8	i	ELL IPTICAL	27	20	010	+19	+25	+12	ū
15	040631	18.5N 134.2E	700MB	2154		100 0	40 48	1 1	10 I	09 6	040	30	10	1	CIRCULAR	15			+13	+21	+15	100
16	040919	18.7N 134.2E	700MB	2157	896	70 3		3 3 5	50 1	31 2	260	18	5	2	CIRCULAR	20			+16	+20	+15	10
17	042041	19.6N 133.6E	700MB	2279		100 0	20 14	4 13	3O 1	108	020	12	В	2								11
18	042327	19.8N 133.4E	700MB	2295	909	130 3	10 16	9:	60 1	20 3	310	10	8	2	CIRCULAR	20			+13	+19	+17	11
19	050830	20.5N 133.4E	700MB	2276		40 1	40 95	5 26	90 1	19	100	20	7	3						+19	+ 8	177
20	051105	21.2N 133.6E	700MB	2311	913			16	90 1	24 2	210	10	8	3	CIRCULAR	24			+13	+19	+ 7	12
21	052031	22.1N 134.9E	700MB	2396		80 3	20 86	9 19	50 I	111 6	070	13	15	2	CIRCULAR	25			+15	+17		1.7
22	0 52325	22.6N 135.4E	788MB	2423	923	100 2	00 26	5 17	0 1	47 6	070	35	8	4	CIRCULAR	40			+15	+13		13
* 23	060830	25.3N 137.7E	700MB	2315		110 2	20 17	2	30 I	119	140	90	6	4						+ 9	+ 4	1 </td
24	061115	25.2N 139.8E	700MB	2439	927			0.	30	48 4	290	88	5	5	CIRCULAR	32			+11	+17	+ 7	1 - !
25	062036	29.2N 145.4E	700MB	2593		130 2	00 46	3 28	3Ø 1	116 2	200	40	5	10								15
26	062356	31.2N 147.8E	700MB	2665	954	120 1	80 26	3					5	5					+10	+18	+12	150
27	070532	34.8N 152.3E	700MB	2769	959	90 2	20 9	27	0	85 2	220	91	10	5					+18	+26		16
28	070905	37.8N 152.1E	700MB	2891				25	9	72	150	115	10	20					+ B	+ 4		16

NOTICE - THE ASTERISKS (*) INDICATE FIXE UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

TROPICAL STORM HORRIS BEST TRACK DATA

	BEST TRA	CK		WA	RN ING	ED	RORS		24 H	IOUR F	ORECA:	ST RORS		48 H	OUR FO		ST RORS		72 H	IOUR F		ST RORS
MD/DA/HR	POSIT	MIND	PC	SIT	MIND	DST		Pí	DSIT	MINE		MIND	PO:	SIT	WIND	DST	MIND	PO!	SIT	WIND		MIND
110000Z	16.8 156.5		8.0	0.0	0.	-0.	0.	0.0	0.0		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
110006Z	17.4 154.7	35	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	0.
1108122	17.9 153.8	46	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
110018Z	18.4 152.1	45	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
11 8966 Z	18.8 151.8	58	18.6	151.6	50.	17.	0.	21.0	151.2	50.	110.	5.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.
11 8986 Z	19.4 151.5	45	19.5	151.4	50.	8.	5.	23.6	153.7	35.	12.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
11 89 12Z	20.2 151.5	45	20.0	151.8	40.	21.	-5.	23.1	156.0	30.	132.	5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1109182	21.1 151.8	45	21.2	152.2	35.	23.	-10.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
111 000 Z	22.2 152.7	45	22.1	152.8	45.	8.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
111 006 Z	23.4 153.7	35	23.1	153.9	40.	21.	5.	0.0	0.0	ø.	-0.	0.	0.0	0.0	Ø.	-0.	0.	0.0	0.0	0.	-0.	0.
1110122	24.9 154.6	25	24.6	154.1	40.	33.	15.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.	0.9	0.0	0.	-0.	0.

	ALL	FORECAS	TS		TYPH0	ONS WHIL	E OVER	35 KTS
	URNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	19.	85.	0.	0.	ø.	ø.	0.	0.
AVG RIGHT ANGLE ERROR	15.	53.	0.	0.	0.	0.	Ð.	0.
AVG INTENSITY MAGNITUDE ERROR	6.	3.	0.	0.	Θ.	0.	0.	0.
AVG INTENSITY BIAS	1.	3.	0.	0.	0.	0.	0.	0.
NUMBER OF FORECASTS	7	3	8	0	8	8	0	0

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 721. NM
AVERAGE SPEED OF TROPICAL CYCLONE IS 12. KNOTS

TROPICAL STORM NORRIS
FIX POSITIONS FOR CYCLONE NO. 19

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
1	072051	16.5N 157.5E	PCN 4	T1.5/1.5	INIT OBS	PGTW
ż	000000	16.6N 156.5E	PCN 6			PGT₩
3	080300	17.1N 155.8E	PCN 6			PGTW
4	000600	17.4N 154.9E	PCN 6			PGTW
5	989999	17.5N 154.3E	PCN 6			PGT₩
6	888931	17.5N 153.9E	PCN 5			PGTW
7	881296	17.6N 153.4E	PCN 6			PGT₩
ė	081649	18.3N 152.1E	PCN 5	T2.0/2.0	INIT OBS	PGTW
ğ	001040	18.4N 151.8E	PCN 6			PGTW
10	882218	18.5N 151.9E	PCN 3	T3.0/3.0 /D1.5/25HRS		PGTW
ii	090000	18.5N 152.8E	PCN 4			PG™
12	898388	18.6N 151.6E	PCN 4			PGTU
13	090534	18.8N 152.1E	PCN 4			PGTW
14	090750	19.3N 151.9E	PCN 6			PGT⊎
15	090909	19.3N 152.0E	PCN 6		•	PGTW
16	091200	19.7N 152.3E	PCN 6			PGTW
17	091600	20.9N 151.6E	PCN 6			PGTW
18	091819	21.2N 152.0E	PCN 5	T2.0/2.0-/50.0/25HRS		PGTW
19	092030	21.7N 152.7E	PCN 5			PGTW
20	892149	21.7N 153.2E	PCN 5			PGTW
21	100000	22.0N 153.1E	PCN 6			PGTW
22	100522	23.0N 153.8E	PCN 3	T3.0/3.00	INIT OBS EXP LLCC	PGT⊍ RPMK
23	100522	23.2N 154.0E	PCN 6	T2.5/2.5	INIT OBS	PGTW
24	100600	23.3N 153.7E	PCN 4			PGTW
25	198847	23.7N 153.9E	PCN 6			PGTW
26	191200	24.5N 154.6E	PCN 6			PGTW
27	101807	25.9N 155.8E	PCN 6			PGTW
28	102157	26.6N 156.5E	PCN 3			PGTW
29	110000	27.5N 157.5E	PCN 6	T2.0/2.0-/W1.5/18HRS	ULCC FIX	FGIW

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT	OBS MSLP	MAX-SFC VEL/BRG								EYE SHAPE		OR LEN- YAT LON	EYE TEMP DUT/ IN/ DI		MSN NO.
4 5	090824 092057 092352	18.7N 151.8E 19.7N 151.SE 20.1N 151.4E 21.5N 152.4E 22.1N 152.8E 24.0N 153.8E	700MB 1590FT 700MB 700MB 700MB 850MB	3056 3070	994 998	50 220 50 130 45 360 45 030	20 08	230 150	45 48 25	040 230 040	25 15 70	6 7 8 6 5 5	1	CIRCULAR ELLIPTICAL	15 20 1	5 148	+16 +23 +26 +24 +11 +17 + 5 +14 +20 + 3 +11 +17 + 3 +20 +26	3 3	1 2 2 3 3 4

TYPHOON ORCHID BEST TRACK DATA

BEST TRACK				WARNING ERRORS				24	HOUR I	FORECAST ERRORS			48 HOUR FO			ST RORS		72 HOUR FORECAST ERROR				
MD/DA/HR	POSIT	MINE) P(DSIT	WIND	DST	T WIND	PC	SIT	WIN	D DS	T WIND	P	DSIT	MIND	DS1	LNIM	P	OSIT	WINI	DS'	T WIND
1114122	13.8 147.2	20	0.0	0.8		-0.	0.	0.0	9.8		-0.	0.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	8.
1114182	13.3 146.4	20	0.0	0.0		-0.	ø.	0.0	0.8		-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ø.
1115002	12.7 145.6	28	0.0	0.0		-8.	ø.	8.8	0.6		-8.	ē.	0.0	8.8	8.	-6.	8.	0.0	8.8	9.	-8.	8.
1115062	12.3 144.6	20	0.0	0.0		-0.	9.	0.0	0.0		-0.	8.	0.0	0.0	ø.	-0.	ē.	0.0	0.0	ø.	-0.	Ð.
1115122	12.0 143.6	20	0.0	0.0		-8.	0.	0.0	8.8		-0.	ø.	8.0	0.0	ø.	-ē.	ø.	0.0	0.0	ø.	-0.	0.
1115182	11.8 142.7	20	0.0	0.8		-0.	0.	0.0	0.6		-0.	0.	0.0	9.0	0.	-B.	ø.	8.0	0.0	8.	-0.	8.
111600Z	11.3 141.5	20	0.0	0.0		-0. -0.	Ø.	9.0	0.6		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-B.	9.
111606Z			0.0			-0. -0.					-0. -0.	Ø.	0.0	0.0	0.	-0. -0.	0.	0.0	0.0	0.	-0.	0.
	10.3 141.0	20		0.0		•	0.	0.0	0.0		-0. -0.				ø.	-0.				0.	-0. -0.	Ð.
1116122	9.3 139.7	20	0.0	0.0		-0.	8.	0.0	0.0			ø.	0.0	0.0			8.	0.0	0.0			0. 0.
1116182	9.7 138.0	25	0.0	0.0		-0.	0.	0.0	0.6		-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	
111700Z	9.7 136.3	25	0.0	0.0		-0.	0.	0.0	0.0		-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.
1117062	10.4 134.6	30	0.0	0.0		-0.	0.	0.0	0.0		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	8.
111712Z	12.6 132.9	30	0.0	0.0		-0.	0.	0.0	0.6		-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.
1117182	12.4 131.6		12.4			29.		16.0	126.5		240.		19.2			493.		22.2		90.	589.	5.
111 800 Z	12.5 130.5		12.6			8.			126.5		168.		17.9	124.8				21.0		45.	452.	-45.
111 906 Z	13.0 129.7			129.1		46.	-5.		124.5		328.		20.3			478.		23.4		40.	593.	-55.
111812Z	12.8 128.8	45	12.8	128.6	40.	12.	-5.	14.2	128.2	50.	122.	-10.	15.8	126.0		177.		18.1		40.	242.	-60.
111818Z	12.5 128.5	58	12.2	128.4	45.	19.	-5.	13.9	128.7	50.	126.	-15.	15.5	126.3	50.	138.	-35.	17.7	124.6	45.	192.	-55.
111900Z	12.8 128.2	50	12.6	129.1	50.	13.	0.	13.4	126.1	40.	109.	-30.	14.1	124.1	30.	122.	-60.	14.5	122.1	25.	205.	-75.
1119 0 6Z	12.5 127.8	55	12.7	127.9	55.	13.	Ð.	13.4	126.6	50.	82.	-25.	14.0	124.0	50.	105.	-45.	14.2	122.0	45.	236.	-60.
111912Z	12.2 127.8	60	12.2	127.2	55.	35.	-5.	12.9	125.2	55,	82.	-25.	13.6	123.3	50.	133.	-50.	13.0	121.1	40.	299.	-65.
1119182	12.1 127.6	65	12.4	127.2	55.	30.	-18.	12.7	125.7	60.	46.	-25.	13.4	123.7	50.	122.	-50.	13.8	121.6	48.	285.	-70.
112000Z	12.2 127.5	70	12.2	127.5	65.	ø.	-5.	12.5	126.2	70.	60.	-20.	13.2	124.2	65.	131.	-35.	13.8	121.6	60.	311.	-50.
112996Z	12.7 127.2	75	12.3	127.4	70.	27.	-5.	13.0	126.6	80.	55.	-15.	13.9	122.9	75.	193.	-30.	14.8	119.8	70.	412.	-50.
1129122	12.9 126.6	60	12.8	126.6	85.	6.	5.	13.5	123.1	80.	146.	-20.	14.2	119.9	70.	358.	-35.	15.8	116.4	85.	569.	-40.
112018Z	13.2 126.3	85	13.2	126.1	90.	12.	5.	13.9	122.6	80.	168.	-20.	14.2	119.7	70.	377.	-40.	15.5	116.2	85.	569.	-35.
1121862	13.5 126.1	98	13.5	126.1	90.	ø.	ø.	14.5	124.3	100.	79.	Ð.	14.9	121.7	95.	279.	-15.	15.0	118.8	85.	419.	-25.
112186Z	13.9 125.B	95	14.1	125.6	98.	17.	-5.	15.2	123.1	100.	162.	-5.	16.4	128.1	88.	357.	-48.	18.4	117.6	85.	448.	-15.
112112Z	14.2 125.5	100	14.2	125.3	100.	12.			123.3			5.	15.6	120.8	85.	322.	-40.	17.7	118.2	95.	401.	0.
11211BZ	14.6 125.4					12.				105.				120.9	85.	307.	-35.	17.6	118.3	90.	377.	5.
112200Z	14.9 125.6	100	14.8	125.5	100.	В.			124.6			-15.	15.0	122.8	85.	220.	-25.	15.9	120.4	65.	274.	-18.
112206Z				125.6					125.5		46.			121.6	75.			28.0		65.	138.	0.
1122122	15.6 125.9					8.	-15.	17.7	126.1		42.	-50.	21.7	128.4	65.	320.	-30.	24.9	134.0	55.	633.	0.
1122182	16.1 125.9					A.			126.2					128.3		264.		23.9		55.	683.	5.
112300Z	16.3 126.3			126.2		8.			127.3					129.2				24.1		55.	694.	5.
112306Z	16.8 126.3					6.				130.				129.3				24.1		100.	784.	55.
1123122	17.8 126.2					8.				120.				128.1		283.		24.5			705.	60.
1123182	17.3 125.9					8.	5.	19.0	126.4	140.	116.	55.				272.	80.	24.6	134.5	120.	796.	85.
112400Z	17.5 125.6					6.			125.6		91.			128.0	95.			24.4		75.	789.	45.
112406Z				125.3		6.			125.6		59.		21.4			270.	50.	0.0	0.0	0.	-0.	0.
1124122	17.3 125.2			125.3		B.			125.6		69.			127.8		316.	48.	0.0	0.0	ø.	-0.	Ð.
1124182	17.7 124.9			125.1		17.			124.3		39.		19.7			261.	30.	0.0	0.0	ø.	-8.	ø.
112506Z	17.9 124.7			124.1		35.			123.5		52.		18.7	121.8		324.	25.	8.8	0.0	8.	-0.	ø.
1125062	18.0 124.6			124.6		a.			123.4		68.	15.	0.0	0.8	0.	-0.	ē.	0.0	0.0	a.	-0.	0.
112512Z	18.4 124.4			124.2		17.			123.6		166.	0.	9.8	0.0	Đ.	-0.	ø.	0.0	0.0	ø.	-8.	8.
1125182	18.5 124.9			123.4		86.	5.	0.0	0.8		-0.	Ð.	0.0	0.0	0.	-B.	Ð.	0.0	6.0	a.	-0.	ø.
1126002	18.1 124.4			124.2		11.		18.6	123.6		286.	8.	8.8	8.8	8.	-0.	9.	9.8	8.8	8.	-8.	8.
112606Z	17.4 124.7			124.7		36.	-5.	0.0	0.6		-0.	8.	0.0	0.0	ø.	-0.	8.	8.0	9.0	8.	-0.	19.
112612Z	16.5 124.9			124.8		19.	0.	0.0	0.0		-0.	ð.	8.8	9.8	ē.	-Ð.	0.	0.0	0.0	e.	-0.	0.
112618Z	15.5 124.2			124.8		39.	0.	0.0	0.8		-0.	0.	0.0	0.0	ø.	-B.	0.	0.0	0.0	a.	-0.	0.
1127002	14.2 124.9			124.9		99. 0.	0.	0.0	0.6		-0.	0.	0.0	0.0	ø.	-8.	8.	0.0	0.0	Ø.	-0.	ð.
. 12,007	164.7	30	.4.2	124.3		υ.	٠.	0.0	0.6		-₽.	u.	0.0	0.0	υ.	-0.	υ.	0.0	5.0	٠.	٠.	٠.

	ALL	FORECAS	TS		TYPHO	35 KTS		
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	16.	117.	267.	459.	17.	112.	265.	446.
AVG RIGHT ANGLE ERROR	10.	54.	160.	343.	10.	53.	160.	332.
AVG INTENSITY MAGNITUDE ERROR	5.	21.	36.	30.	5.	21.	37.	37.
AVG INTENSITY BIAS	-2.	-4.	-18.	-17.	-2.	-4.	-11.	-20.
MINGED OF ERDECOSTS	70	27	70	26	77	32	20	25

DISTRNCE TRAVELED BY TROPICAL CYCLONE IS 2214. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 7. KNOTS

TYPHOON ORCHID FIX POSITIONS FOR CYCLONE NO. 20

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
1	140432	12.9N 146.4E	PCN 6			PGTW
2	141200	14.8N 147.2E 13.2N 146.8E	PCN 6 PCN 6	T1.0/1.0	INIT 08S	PGTW PGTW
4	141800	13.1N 146.6E	PCN 6			PGTW
* 5 * 6	142141 150000	11.8N 142.6E	PCN 3 PCN 4			PGTW PGTW
* 7	150300	11.7N 142.3E 11.7N 142.0E	PCN 6	T0.5/0.5	INIT OBS	PGTW
8	151800	12.7N 143.2E	PCN 6	T1.0/1.0 /S0.0/26HRS	ULCC FIX	PGTW
9 1 8	152300 160300	11.4N 141.6E 11.4N 141.1E	PCN 5 PCN 6	T1.5/1.5 /01.0/24HRS	ULCC AT 12.6N 142.BE	PGTW PGTW
11	160600	10.3N 141.2E	PCN 6	11.3, 1.3 , 51.0, 24.10		PGTW
12	16 0900 1612 00	9.5N 140.5E	PCN 6			PGTW PGTW
13 14	161600	9.2N 139.6E 9.3N 139.8E	PCN 6 PCN 6	T1.5/1.5 /D0.5/22HRS	ULCC FIX	PGTW
15	161834	9.5N 138.5E	PCN 5	_	ULCC FIX	PGTW
16 17	1621 66 162239	10.0N 138.1E 9.7N 136.3E	PCN 6 PCN 5			PGTW PGTW
18	170000	9.7N 136.0E	PCN 6			PGTW
19 20	170300 170537	9.7N 135.3E 9.8N 135.4E	PCH 6 PCH 5	T1.5/1.5 /S0.0/24HRS	ULCC FIX ULCC FIX	PGTW PGTW
21	171200	12.1N 132.6E	PCN 6		OLCC PIA	PGTW
22	171600	12.5N 131.2E	PCN 6	T3.0/3.0 /D1.5/24HRS		PGTU
23 24	171821 172183	12.4N 131.1E 13.0N 130.1E	PCN 6 PCN 5			PGTW PGTW
25	172184	12.8N 131.7E	PCN 5			RPMK
26 27	18 0000 18 0300	12.7N 130.1E 13.3N 129.5E	PCN 6 PCN 6	T2.5/2.5 /D1.0/24HRS		PGTW PGTW
28	188688	13.5N 128.9E	PCN 6			PGTW
29 38	18 0767 18 0900	13.6N 128.9E 13.5N 128.9E	PCN 5 PCN 6			PGTW PGTW
31	181200	13.3N 128.1E	PCN 6			PGTW
* 32 33	181600	12.7N 127.3E 12.4N 127.5E	PCN 6 PCN 6	T3.8/3.0-/S0.8/24HRS		PGTW PGTW
33 34	1818 06 1821 88	12.8H 127.7E	PCN 6			PGTW
35	182336	12.7H 128.2E	PCH 5		****	PGTW
36 37	182336 19 6 388	12.2N 128.5E 12.7N 128.0E	PCN 5 PCN 6	T3.0/3.0 T3.0/3.0-/D0.5/24HRS	INIT OBS	RPMK PGTU
30	190654	12.7N 127.2E	PCN 5			PGTW
39 48	19 0900 1912 00	12.4N 127.4E 12.6N 127.2E	PCN 6 PCN 6			PGTW PGTW
41	191688	12.2N 127.3E	PCN 6	T3.5/3.5-/D0.5/24HRS		PGT₩
42 43	1918 86 191939	12.7N 127.2E 12.2N 127.5E	PCN 6 PCN 5			PGTW RPMK
44	192100	12.3N 126.9E	PCN 6			PGT⊎
45 46	1922 83 192314	12.1N 127.5E 12.3N 127.4E	PCN 3 PCN 3			PGTW PGTW
47	192314	12.1H 127.4E	PCN 3	T3.0/3.0	INIT 08S	RODN
48 49	200300 200642	12.3N 127.2E 12.4N 127.4E	PCH 4 PCH 1	T4.0/4.0-/D1.0/24HRS		PGTW PGTW
58	201013	12.9H 126.9E	PCN 1			PGTW
51	281843	12.8H 127.2E	PCN 1			RODN
52 53	281288 281688	12.8N 126.6E 13.1N 126.4E	PCN 2 PCN 4	T4.5/4.5-/D1.5/24HRS		PGTW PGTW
54	201800	13.2N 126.1E	PCH 4			PGTW
55 56	261927 262168	13.5N 126.3E 13.3N 126.8E	PCN 3 PCN 4			PGTW PGTW
57	202142	13.2N 126.1E	PCH 4			PGTW
58 59	202252 202252	13.1N 126.0E 13.2N 126.1E	PCN 3 PCN 3	T4.0/4.0 /D1.0/24HRS		PGTW RODN
60	210300	13.9N 125.6E	PCN 2			PGTW
61 62	210629 210629	14.2N 125.7E 14.2N 125.6E	PCN 1 PCN 3	T5.0/5.0 T4.5/4.5-/D0.5/27HRS	INIT OBS	RPMK PGTW
63	218988	14.4N 125.3E	PCN 2	14.3/4.0 / 50.3/2/11/03		PGTW
64 65	211622 211266	14.3N 125.3E 14.5N 125.3E	PCN 4 PCN 2			PGTW PGTW
66	211600	14.5N 125.4E	PCN 2	T5.8/5.0	INIT OBS	PGTW
67 68	2118 66 211914	14.9N 125.6E 14.9N 125.6E	PCN 2 PCN 1			PGTW PGTW
69	211914	14.8N 125.5E	PCH 1			RODH
70		15.8H 125.3E	PCH 5		ULCC FIX	PGTU
71 72	22 0000 22 00 12	15.8N 125.4E 14.7N 125.7E	PCN 6 PCN 1	75.8/5.8 /S8.8/19HRS	ULCC FIX	PGTW RPTSK
73	220300	15.1N 125.7E	PCN 2	75.8/5.8 /D8.5/21HRS	EYE DIA 25MM	PGTW
74 75	220600 220617	15.4H 125.6E 15.3H 125.7E	PCN 2 PCN 3	T5.8/5.8 /S8.8/24/RS		PGTW RP190
76	220900	15.5N 125.7E	PCN 4	,_,_,		PGTU
77 78	2212 66 2216 66	15.6N 125.9E	PCH 4 PCH 4	T4.5/5.8-/JB.5/24RS		PG TW PG TW
		16.1N 126.1E	PCN 4			PGTU

83 84 86 87 89 90 91 92 93 95 96 97 98 99 100 102 103 106 106 106 107 108 111 111 111 113	232328 240309 240552 240608 240909 241027 241109 241200 241209 242306 242306 242306 250600 250721 251039 252245 260600 260600	16.4H 126.2E 16.4H 126.3E 16.6H 126.3E 16.6H 126.3E 17.1H 126.2E 17.1H 126.1E 17.2H 125.9E 17.3H 125.9E 17.5H 125.5E 17.5H 125.5E 17.5H 125.5E 17.5H 125.5E 17.6H 125.6E 17.6H 125.6E 17.6H 125.6E 17.9H 124.6E 18.9H 124.6E	PCR 2 2 PCR 2 1 1 1 2 1 2 PCR	T4.5/4.5 T6.5/6.5-/9 T5.5/5.5-/9 T5.8/5.8 /4 T5.8/5.5 /4 T5.8/6.8 /4 T4.8/5.8-/4 T4.5/5.5 /4	2.8/24HRS 8.5/21HRS 1.8/24HRS 6.5/38HRS 1.5/24HRS 1.5/24HRS 1.5/24HRS	EYE DIA : EYE DIA : INIT OBS EYE DIA : EYE DIA : EYE DIA :	15NM 26NM 36NM 28NM	PGTUPGTUPGTUPGTUPGTUPGTUPGTUPGTUPGTUPGTU		
					AIRCR	AFT FIXES				
FIX NO.	TIME (Z)	F1X POSITION	FLT LVL		MAX-SFC-WND VEL/BRG/RNG	MAX-FLT-LVL-UND DIR/VEL/BRG/RNG			EYE TEMP OUT/ IN/ DP	
3 4 5 6 7 8 9 10 1 12 13 4 15 16 7 18 9 10 1 12 13 4 15 16 7 18 9 22 22 24 25 26 28 29 3 1 2 3 3 3 4 3 5 6 7	182128 190023 190754 191035 192110 192336 200834 201319 210833 210233 211118 220917 221156 2209217 221156 2209217 221156 220931 231118 232256 240836 241189 24231	12.5N 130.5E 13.8N 129.2E 12.6N 120.8E 12.5N 120.8E 12.5N 127.0E 12.1N 127.7E 12.2N 127.5E 12.9N 127.2E 12.1N 127.5E 12.9N 126.2E 13.5N 126.2E 13.5N 126.2E 14.1N 125.5E 14.2N 125.5E 14.2N 125.5E 14.2N 125.5E 14.2N 125.5E 17.9N 126.2E 16.2N 126.3E 17.9N 126.2E 17.5N 125.3E 17.9N 124.8E 17.9N 124.8E 18.9N 124.8E 18.9N 124.8E 18.9N 124.8E 18.2N 124.8E	1500FT 700HB 950HB 950HB 950HB 950HB 950HB 950HB	2632 2648 958 2588 942 2589 943 2655 2665 2614 2632 947 2491 2591 933 2460 2457 931 2583 941 2636 2791 2828 2926 992 3081 992 3087 1085		040 35 320 40 110 49 040 90 040 55 310 102 320 59 210 15 040 55 310 68 130 50 020 51 040 56 340 30 140 63 050 15 290 76 180 17 330 78 240 16 210 80 130 18 020 75 310 18 170 80 060 90 030 89 320 30 166 105 100 23 350 105 240 23 140 93 070 20 140 94 090 22 040 101 30 10 200 115 100 23 060 102 350 21 130 85 050 25 130 85 050 25 130 85 050 25 130 85 050 25 130 85 050 25 130 85 050 25 130 85 050 25 130 85 050 25 130 85 050 25 130 85 050 25 130 85 050 25 130 85 050 25 130 85 050 26 130 85 050 60 102 350 61 103 300 37 330 51 270 15 080 55 320 60 100 30 330 64 070 39 330 64 070 39 330 64 070 39 330 64 070 39 330 64 070 39 330 64 070 39 330 64 070 39 330 64 070 39 330 64 070 39 330 64 070 39 330 64 070 39 330 64	8 4 CIRCULAR 15 4 15 5 CIRCULAR 18 2 CIRCULAR 8 5 12 2 18 3 CIRCULAR 8 3 CIRCULAR 8 3 CIRCULAR 8 3 CIRCULAR 18 2 CIRCULAR 18 3 CIRCULAR 18 2 CIRCULAR 18 3 CIRCULAR 2 CIRCULAR 5 5 CIRCULAR 6 7 CIRCULAR 6 8 7 CIRCULAR 6 9 7 CIRCULAR	20 20 25 22 20 30 17 30 17 20 25 25 25 25 25	+23 +11 +13 +11 +28 +26 +18 +8 +18 +8 +19 +18 +18 +11 +17 +18 +12 +16 +12 +13 +18 +14 +14 +18 +15 +13 +16 +13 +13 +16 +15 +13 +17 +15 +13 +17 +15 +13 +17 +15 +13 +17 +15 +13 +17 +15 +15 +16 +13 +15 +16 +11 +15 +16 +11 +15 +16 +11 +15 +16 +11 +15 +16 +11 +15 +16 +11 +17 +16 +18 +14 +18 +19 +14 +19 +16 +19 +14 +11 +19 +14 +11 +19 +14 +11 +19 +14 +12 +14 +18 +24 +23 +15 +24 +23 +24 +24 +24 +23 +24 +24	4 4 29 5 5 6 6 7 7 7 8 8 8 9 9 9 9 10 10 11 12 12 13 13 14 15 15 16 16 17 18 18 19 19 20 20 20 21 28 21
FIX NO.	TIME (Z)	FIX POSITION	RADAR F	EYE ACCRY SHAPE	DIAM	RADOB-CODE ASWAR TODEF	COMMENTS		RADAR POSITION	SITE WMO NO.

5///2 42713

13.5N 127.6E LAND

14.0N 124.3E

98447

* 2	190130	13.6N	127.1E	LAND	5///2	42923							14.0N	124.3E	98447
* 3	190200	13.7N	126.8E	LAND	5///2	43226							14.8N	124.3E	98447
* 4	190330	13.8N	126.6E	LAND	5///2	42711							14.0N	124.3E	98447
* 5	190400	13.8N	126.6E	LAND	5///2	40000							14.8N	124.3E	98447
* 6	190600	13.6N	126.5E	LAND	5///2	42228							14.0N	124.3E	98447
* 7	190700	13.6N	126.5E	LAND	5///2	40000							14.6N	124.3E	98447
8	190800	12.7N	127.3E	LAND	5///3								14.0N	124.3E	98447
9	191000	12.6N	127.0E	LAND	5///2	42205							14.0N	124.3E	98447
10	191100	12.3N	126.9E	LAND	5///2	51916							14.0N	124.3E	98447
11	191200	12.3N	126.9E	LAND	5/1/2	50000							14.0N	124.3E	98447
12	191300	12.3N	126.9E	LAND	5/1/2	52704								124.3E	98447
13	201100	12.BN	126.9E	LAND	20503	529//								124.3E	98447
14	201208	12.8N	126.BE	LAND	20513	53208							14.0N	124.3E	98447
15	261366	12.8N	126.BE	LAND	20243	52404							14.6N	124.3E	98447
16	201400	12.BN	126.7E	LAND	10413	52508	EYE	CIR	50	PCT	OPEN	NE		124.3E	98447
17	201500	12.BN	126.7E	LAND	10323	40000	EYE	CIR	50	PCT	OPEN	NE		124.3E	98447
18	210000	13.5N	126.2E	LAND	11111	53405								124.3E	98447
19	210100	13.6N	126.1E	LAND	10413	52708								124.3E	98447
20	210400	13.BN	125.8E	LAND	10513		EYE	CIR	40	PCT	OPEN	NNE		124.3E	98447
21	210800		125.7E	LAND	10893									124.3E	98447
22	211000	14.4N	125.5E	LAND	10813									124.3E	98447
23	211400		125.5E	LAND	10713						OPEN			124.3E	98447
24	211500		125.6E	LAND	10713		EYE	CIR	40	PCT	OPEN	HHE		124.3E	98447
25	212288		125.6E	LAND	10713									124.3E	98447
* 26	212300		124.8E	LAND	4///									121.6E	98321
27	220100		125.7E	LAND	10713									124.3E	98447
28	220230		125.6E	LAND	10743									124.3E	98447
29	220300		125.7E	LAND	10713									124.3E	98447
30	220500		125.BE	LAND	10713									124.3E	98447
31	220800		126.0E	LAND	10613									124.3E	98447
32	221000		126.1E	LAND	50405									124.3E	98447
33	221186		126.2E	LAND	2/612									124.3E	98447
34	221200		126.3E	LAND	2/612									124.3E	98447
35	250700		124.3E	LAND	11/21									121.6E	98231
36	250800		124.3E	LAND	11121									121.6E	98231
37	251500		124.0E	LAND	5////									121.6E	98231
38	251600		123.9E	LAND	5////									121.6E	98231
39	251800		123.8E	LAND	5///									121.6E	98231
40	251900		123.7E	LAND	5////									121.6E	98231
41	252 100		123.4E	LAND	21602									121.6E	98231
42	252200		123.1E	LAND	21612									121.6E	98231
43	252300		123.0E	LAND	25552									121.6E	98231
44	270600	13.4H	124.7E	LAND	2////	52205							14.0N	124.3E	98447

NOTICE - THE ASTERISKS (*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

TYPHOON PERCY BEST TRACK DATA

	BEST TRACE	K		WF	IRN 1 NG				24	HOUR				48 H	IOUR F	OREC			72 H	IOUR F	ORECA	
							RORS					RORS					RORS	_				RORS
MD/DA/HR		MIND		SIT	MIND		MIND		SIT	MIN		L MĪHE		DSIT	WINI		T WIND		DSIT	MIND		_
1117 00 Z	10.5 110.0	15	8.8	0.0	0.	-8.	0.	0.0	0.6		-0.	e.	0.0	8.8	8.	-8.	۵.	0.6	0.0	●.	-0.	₽.
1117 8 6Z	10.8 111.8	15	0.0	0.0	0.	-8.	0.	0.0	0.6	0.	-8.	0.	0.8	0.0	₽.	-Ð.	Ð.	0.6	0.0	₽.	-0.	8.
1117122	9.8 111.0	15	8.6	0.0	0.	-8.	ø.	0.0	0.6	0.	-0.	0.	0.0	0.0	₽.	-8.	Ð.	8.8	0.0	€.	-8.	€.
1117182	9.6 111.1	15	0.0	0.0	€.	-8.	0.	0.0	0.6	0.	-0.	Ø.	0.0	0.0	8.	-0.	8.	0.0	8.0	●.	-0.	٥.
1119862	9.5 111.1	29	8.8	8.8	8.	-0.	9.	0.0	8.6	9.	-0.	₽.	8.0	8.8	0.	-0.	e.	0.0	8.8	8.	-8.	0.
1119862	9.0 111.6	20	0.0	0.0	ø.	-0.	8.	0.0	8.6	9.	-0.	Ð.	0.0	0.0	0.	-0.	₽.	8.0	6.6	0.	-8.	₩.
111812Z	8.6 112.0	20	0.0	0.0	0.	-0.	0.	0.0	0.6	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-8.	0.
111818Z	8.6 112.6	25	0.0	0.0	8.	-0.	ø.	0.0	0.8	0.	-0.	8.	0.6	8.8	ø.	-0.	ø.	6.8	0.0	0.	-0.	₽.
1119002	8.9 113.1	48	8.0	0.0	Ð.	-0.	ø.	8.0	0.6	0.	-0.	0.	0.8	0.0	8.	-0.	0.	8.8	0.0	0.	-0.	8.
111906Z	8.7 112.7	45	8.7	112.8	45.	6.	ø.	9.6	111.7	50.	138.	-15.	10.3	110.3	45.	185.	-15.	12.8	188.8	25.	388.	-15.
1119122	8.1 112.6	50	8.3	112.6	60.	12.	10.	8.6	110.9	65.	83.	-5.	9.2	189.5	60.	188.	5.	10.6	107.2	55.	388.	20.
1119182	7.5 112.4	55	8.8	111.3	60.	182.	5.	9.9	109.4	65.	188.	ø.	10.6	108.0	50.	312.	A.	11.4	106.5	38.	489.	-5.
112000Z	7.4 111.8	68		111.7	60.	В.	Đ.		110.0		97.	-5.	9.5	107.7		316.		11.0	105.6		563.	10.
112006Z	7.3 111.6	65	B. 1	111.2	65.	54.	ø.		110.2		123.	5.	9.8	188.2	65.	309.		10.3	184.8	55.	653.	25.
1120122	7.3 111.4	78		111.5	75.	6.	5.		118.3		101.	30.	8.7	108.7	80.	283.		10.0	107.1		567.	35.
1120102	7.4 111.3	65		111.0	75.	19.	10.		109.2		189.	30.	9.4	107.6	70.	392.		10.7	106.0		676.	5.
112100Z	7.6 111.6	60		111.5	75.	6.	15.		118.5		100.	15.	9.0	109.2	50.	333.		10.2			728.	25.
112186Z	7.6 111.8	60		111.6	70.	13.	10.		111.2		109.	10.	8.5	109.0	40.	398.	18.	9.5	106.3		816.	5.
1121122	7.5 112.0	55		112.8	60.	e.	5.		111.6		147.	15.	8.6	109.7	40.	469.	10.	9.3	106.2		905.	10.
1121182	7.6 112.3	50		111.5	60.	48.	10.		109.4		279.	15.	8.5	107.5	40.	590.	15.	9.2	104.2	30.1		10.
112200Z	7.7 112.7	45		112.7	50.	6.	5.		111.4		209.	5.	7.8	118.7	35.	499.	10.	0.0	0.0	В.	-0.	ø.
1122062	7.8 113.0	40		112.8	45.	12.	5.		112.6		226.	5.	7.7	111.0	30.	575.	5.	0.0	0.8	ø.	-0.	ø.
1122122	7.9 113.4	35		113.4	40.	6.	5.		113.9		160.	5.	9.0	111.9	30.	593.	10.	8.9	0.0	Ð.	-0.	ø.
1122182	8.2 114.1	35		113.9	40.	13.	5.		112.6		286.	10.	9.1	110.7	30.	717.	10.	0.0	8.8	ø.	-0.	e.
1123002	8.6 114.8	35		114.9	35.	13.			121.8		206.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	ø.
112306Z	8.6 115.7	30		115.4	35.	40.			117.5		147.	10.	9.0	0.0	0.	-0.	Θ.	0.0	0.0	e.	-0.	Ð.
112312Z	8.8 116.6	30		116.6	35.	ø.			118.6		195.	10.	0.0	0.0	ø.	-0.	Θ.	0.0	0.0	В.	-0.	Ø.
1123182	9.6 117.4	25		117.3	35.	13.			117.6		205.	10.	0.0	0.0	0.	-0.	В.	0.0		0.	-0.	Ø.
1123162 112400Z	10.4 118.7			118.3	39.	24.					-8.	N.	0.0	0.0	0.	-0. -0.	0. 0.	0.0		Ø.	-0. -0.	J.
							5.	0.0	0.0			٥.				-0.						
112406Z	11.3 120.0	25		119.2	30.	47.	5.	0.0	0.6		-0.	ø.	0.0	0.0	Ø.	-0.	В.	0.0	0.0	0.	-0.	0.
1124122	12.0 121.3			121.2	25.	19.	5.	0.0	0.0		-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-8.	0.
112418Z	12.4 122.4	20	12.5	122.5	20.	Θ.	ø.	0.0	8.6	9.	-0.	Ø.	0.0	0.0	0.	-0.	9.	0.0	0.0	0.	-0.	8.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 3					
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR		
AVG FORECAST POSIT ERROR	21.	173.	409.	660.	28.	148.	289.	457.		
AVG RIGHT ANGLE ERROR	11.	86.	184.	361.	9.	88.	207.	350.		
AVG INTENSITY MAGNITUDE ERROR	5.	11.	14.	15.	6.	13.	18.	13.		
AVG INTENSITY BIAS	5.	8.	12.	11.	6.	8.	14.	3.		
NUMBER OF FORECASTS	23	19	15	11	16	12	В	4		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1123. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

6. KNOTS

TYPHOON PERCY FIX POSITIONS FOR CYCLONE NO. 21

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
1	181288	B.6N 112.0E	PCN 6		ULCC FIX	PGT⊎
Ž	181600	8.7N 112.9E	PCN 6	T1.8/1.8	INIT OBS	PGTW
3	182188	8.8N 113.1E	PCN 6			PGTW
4	182336	8.7N 113.3E	PCN 5	T2.5/2.5	INIT OBS	PGTW
5	182336	9.9N 113.1E	PCN 5	T3.0/3.0	INIT OBS	RPMK
6	190300	8.8N 112.8E	PCN 6	•		PGTW
7	190600	8.7N 112.4E	PCN 6			PGTW
* 8	190900	8.7N 111.6E	PCH 6			PGTW
9	191184	8.8N 112.6E	PCN 3	T3.0/3.0 /S0.0/12HRS		RPMK
* 10	191200	9.0N 111.4E	PCH 6	10.070.00		PGTW
11	191216	8.3N 112.2E	PCN 5		ULCC FIX	RODN
	191600	8.9N 111.8E	PCN 6	T3.0/3.0	INIT OBS	PGTW
* 12			PCN 6	13.0/3.0	11111 333	PGTW
* 13	191888	9.3N 111.5E				RPMK
14	191939	7.5N 111.6E	PCN 5			PGTW
* 15	192100	8.9N 111.6E	PCN 6			PGTW
16	192203	7.4H 111.2E	PCN 5			PGTW
17	200000	7.5N 111.4E	PCH 6			
* 18	200056	8.3N 111.0E	PCH 3	T4.0/4.6-/D1.0/22HRS		RPMK

19	200300	7.4N 111.4E	PCN 4	T4.8/4.8-/D1.8/24HRS		PGTW
26	200600	7.7N 111.2E	PCN 4			PGTW
21	200824	7.3N 111.2E	PCN 3			RPMK
22	200900	7.7N 111.0E	PCN 6			PGTW
23	201043	7.1N 110.7E	PCN 5			RODH
* 24	201154	7.3N 118.4E	PCN 3			RODH
25	201154	7.2N 111.2E	PCN 5			RPMK
26	201200	7.5N 111.3E	PCN 6			PGTW
27	201600	8.0N 111.1E	PCN 6	T4.5/4.5-/D1.5/24HRS		PGTW
28	261666	8.3N 111.0E	PCN 6			PGTU
29	202100	7.5N 110.9E	PCN 6			PGT⊌
38	202323	7.4N 111.1E	PCN 5	T4.8/4.8 /S8.8/23HRS		RPMK
31	210000	7.5N 111.7E	PCH 6			PGTW
32	210300	7.7N 110.8E	PCN 6			PGTW
33	210600	7.7N 111.7E	PCN 6	T3.0/4.0 /WI.0/27HRS		PGT⊎
34	219911	7.2N 112.1E	PCH 3	T3.0/4.0-/W1.6/24HRS		RPMK
35	210900	7.9N 111.BE	PCN 6		EXP LLCC	PGTW
36	211132	7.3N 111.2E	PCN 5			RPMK
37	211200	7.6N 111.6E	PCN 6		ULCC FIX	PGTW
* 38	211600	7.6N 111.1E	PCN 6	T2.5/3.5-/W2.0/24HRS		PGTU
* 39	211600	8.0N 118.6E	PCN 6			PGTW
48	212302	7.8N 112.7E	PCN 3	T2.5/3.5 /W1.5/24HRS		PGTU
41	212302	7.8N 112.7E	PCN 3	T2.5/3.5 /W1.5/24HRS		RPMK
42	2 20000	7.7N 112.7E	PCN 4			PGT⊎
43	220012	7.7N 112.9E	PCN 3	T2.0/2.0	INIT OBS	RODN
44	220012	7.7N 112.7E	PCN 3			RPMK
45	220300	7.8N 112.8E	PCH 4	T2.8/3.0 /W1.8/21HRS		PGT⊍
46	220600	7.8N 112.9E	PCH 4		EXP LLCC	PGT⊎
47	220759	7.5N 113.1E	PCH 3			RPMK
48	220900	7.8N 113.1E	PCN 6		EXP LLCC	PGTW
49	221288	7.9N 113.4E	PCN 6		EXP LLCC	PGTW
50	221600	7.7N 113.9E	PCN 6	T1.5/2.5 /W1.8/24HRS		PGTW
51	221800	8.2N 113.8E	PCN 6			PGTW
52	222100	8.5N 113.5E	PCN 6		ULCC 8.5N 112.1E	PGTW
53	222241	8.3N 114.9E	PCN 3	T2.8/2.5+/W0.5/24HRS		RPMK
54	222350	8.7N 115.8E	PCN 3	T1.0/2.0 /J1.0/24HRS		RODN
55	222350	8.5N 114.8E	PCN 3	70 0 0 0 00 00 00 00 00 00 00 00 00 00 0		RPMK
56	230000	8.5N 115.2E	PCH 4	T2.0/2.8 /50.0/21HRS		PGTU
57 58	230000 230300	8.3N 114.7E 8.9N 115.1E	PCN 6 PCN 6			PGTW PGTW
59	230600	8.6N 115.1E	PCN 4		EVB LLCC	PGTU
68	238746	9.0N 115.9E	PCN 3		EXP LLCC	RODN
61	230746		PCN 3			RPMK
62	230900	8.6N 116.7E 8.8N 116.1E	PCN 6		EVB LLCC	PGTW
63	231121	8.4N 116.4E	PCN 5		EXP LLCC	RPMK
64	231200	8.8N 116.6E	PCN 6		EVP 11.00	PGTU
65	231600	8.9N 116.9E	PCH 6	TB.5/1.5 /W1.8/24HRS	EXP LLCC	PGTW
66	231888	9.4N 117.4E	PCN 6	19.3/1.3 /WI.0/24MR3		PGTW
67	232100	9.6N 117.5E	PCN 6			PGTW
68	232328	10.6N 118.6E	PCN 5	T1.0/2.0 /U1.0/24HRS		PGTW
69	232328	8.2N 117.5E	PCN 5	T1.8/2.8 /W1.8/24HRS		RPMK
79	240300	10.6H 117.3E	PCN 6	11.0/2.0 /WI.0/24NR3		PGTU
71	240600	11.0N 119.6E	PCN 6			PGTW
72	241100	10.9N 121.1E	PCN 5		ULCC FIX	RODH
73	241100	10.7N 121.1E	PCN 5		ULCC FIX	RPMK
74	241600	11.0N 121.3E	PCN 6		JUG FIA	PGTW
, -	1000	**************************************	run o			rulw

AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT	09S MSLP		-SFC- /BRG/	-UND RNG	MAX- DIR/		-LVL- ⁄BRG/				EYE SHAPE	EYE C	RIEN- TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
1	191642	8.2N 112.6E	700MB	2976	986	60	156	30	888		348	22	10		CIRCULAR	48		+14 +16 + 6	1
2	192136	7.3N 112.3E	788MB	2956	985				140	51	040	30	15	5					2
3	192331	7.4H 112.8E	788MB	2934	901	65	140	12	220	54	140	30	15	3	ELL IPTICAL	15 10	100	+13 +20 +10	2
4	200905	7.2N 111.5E	700MB	2843		55	278	5	120	79	630	30	15	5	CIRCULAR	28		+20 +10 + 9	3
5	201135	7.2N 111.5E	789MB	2857	971				250	76	186	35	15	2	ELL IPTICAL	28 15	116	+17 +18 +10	3
6	202041	7.4N 111.3E	786MB	2876					160	68	969	18	18	3	ELL IPTICAL			+14 +16 +18	4
7	202344	7.6N 111.6E	700MB	2959	985	88	150	33	190		120	68	22	3				+15 +17 +11	4
	216956	7.5N 112.6E	788MB	2978	986		248		858		328	68	12	_				+13 +15 + 9	5
9	211142	7.7N 111.9E	788MB	2960	986				270		210	30	12	-				+11 +15 + 9	5
18		7.7N 112.7E	7801B	2993	991	16	100	128	230		130	30	18	_				+16 +15 + 9	6
ii	220845	7.9N 113.1E	1500FT	3855	997		250		349		268	39	6					+20 +20	7
• •						30	230	60					_	_					
12	221126	7.8N 113.3E	786MB	3874	1002				260	40	150	30	6	3				+13 +10	7
13	238241	8.8N 114.8E	1500FT		1004	35	668	48	180	27	969	90	6	5				+24 +25 +19	8

TROPICAL STORM RUTH BEST TRACK DATA

	BEST TRAC	ж		u	RN I NS	50	RORS		24	HOUR	FORECE	ST RORS		48 1	HOUR F		ST		72 F	OUR I	ORECA	ST RORS
HD/DR/HR	POSIT	MIND	-	SIT	UNI			-	DSIT	ШIN				DSIT	WINE			-	SIT	WIN		
1121062	7.5 145.3	25	8.8	8'8'	מאנש	-B.	N.				-B.	ו הזווח	0.0	0.0	B.	-Da	B.	6.8	0.0	ØIN	-0.	0. 0.
1121122	7.8 144.6	25 25	8.8	8.8	Ð.	-0.	Ð.	8.8 8.8	0.0		-8.	B.	0.0	0.0	B.	-B.	0.	0.0	0.0	8.	-0. -8.	0.
1121182	8.8 143.8	25 25	8.8	8.8	B.	-0. -0.	Ð.	8.6	0.0		-8.	B.	0.0	0.0	8.	-B.	ø.	0.0	0.0	٥.	-0. -0.	0.
112288Z	8.1 142.9	25 25	8.8	0.0	0.	-0.	8.	0.0	8.8		-8.	Θ.	0.0	0.0	ø.	-B.	ø.	0.0	0.0	Ø.	-0. -0.	ø.
1122 0 6Z	8.2 142.2	25	8.8	0.0	0.	-0. -0.	8.	0.0 0.0	0.6		-a.	ů.	8.0	0.0	ð.	-8.	8.	0.0	0.0	٥.	-8.	ð.
1122122	8.3 141.6	25 25	8.8	0.0	Ø.	-0. -0.	0.	D. D	0.0		-0. -0.	٥.	8.0	9.0	Ð.	-0.	0.	0.0	0.0	ø.	-8.	ø.
1122182	8.6 141.0	25 25	0.0	6.8	0.	-0. -0.	0.	0.0	0.6		-8.	0.	0.0	8.8	0.	-8.	0.	0.0	8.8	0.	-8.	ø.
1123002	9.0 140.3	30	9.2	149.2	30.	13.		11.4	136.7		257.	25.	14.9	134.3	65.	433.		19.2	134.2	55.	405.	35.
1123062	9.3 148.4	30	9.4	148.6	30.	13.	0.	18.9	136.8		215.	25.	14.1	135.1	65.	342.		19.2	136.0	65.	378.	45.
1123002 112312Z	9.1 140.9	30	9.2	148.9	30. 30.	6.	0.		130.0		110.	25. 25.	13.0	139.1	68.	256.		16.8	137.4	65.	359.	45.
1123122	8.6 140.5	30	8.9	140.9	30.	25.	0. 0.	10.0			134.	25. 25.		130.2	60.	200. 308.		17.6	137.4	78.	435.	43. 50.
1124002		20 20			30. 20.	25. 6.	ø. Ø.	10.4	139.5		-0.	23. A.	13.4	0.0		-8.	40.			ro. A.		9.
112406Z	8.4 139.8 8.4 139.4	20	8.4	139.9	20. 0.	-0.		0.0	0.6		-0. -8.	ø.			8. 8.	-0. -8.	0. 0.	0.0		ø.	-8. -8.	ø.
1124002	8.4 138.8	20	8.0	0.0 0.0		-0. -0.	0. 0.	0.0	0.6		-e. -e.	Ð.	0.0	0.0 8.0		-0. -8.		0.0	0.0 0.0	٥.		e.
1124182	8.5 138.3	26 25	8.8		ø.	-0. -8.		0.0	0.0		-0. -0.	٥.		0.0 0.0	Ð.		ø.			0.	-0.	
		23 20		0.0	0.		9.	0.0	8.6		-0. -0.	D.	0.0 0.0		e.	-0.	0.	0.0	0.0	٥.	-0.	0.
112500Z 112506Z	8.6 137.9 8.9 137.5	20	0.0	0.0	0.	-0.	0.	0.0	9.6		-0. -0.			0.0 0.0	ø.	-0. -0.	0.	9.0	0.0 0.0	0.	-0.	0. 0.
				0.0	ø.	-0.	8.	0.0	0.6		-0.	Ø.	0.0		0.		0.	0.0		0.	-0.	
1125122		20	0.0	0.0	ø.	-0.	ð.	0.0	0.6			ø.	0.0	0.0	ø.	-0.	0.	0.0	0.0	ø.	-0.	0.
1125182	11.8 133.1	20	0.0	0.0	0.	-0.	0.	0.0	0.8		-0.	0.	8.8	0.0	0.	-0.	0.	0.0	0.0	8.	-0.	0.
1126002	12.7 132.3	20	0.0	0.0	Ø.	-0.	0.	0.0	0.0		-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	٥.	-0.	0.
112606Z	13.7 132.0	20	0.0	0.0	Ø.	-0.	0.	0.0	0.6		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.
1126122	14.5 131.4	20	0.0	0.0	ø.	-0.	0.	0.0	0.0		-0.	8.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-8.	0.
112618Z	15.1 130.2	28	8.8	9.8	8.	-8.	9.	0.0	0.6		-8.	ø.	0.0	0.0	Ø.	-8.	ø.	0.0	0.0	8.	-0.	0.
112700Z	15.6 129.6	25	8.0	0.0	0.	-0.	0.	0.0	0.6		-0.	0.	0.0	0.0	9.	-0.	0.	0.0	0.0	0.	-0.	0.
112706Z	16.0 129.2	25	0.0	0.0	ø.	-0.	0.	0.0	0.6		-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	8.6	0.	-8.	0.
1127122	16.5 129.0	25	0.0	0.0	ø.	-0.	0.	0.0	0.6		-8.	0.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.
1127182	17.0 128.8	30	0.0	0.0	0.	-0.	ø.	0.0	0.6		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1128 96 Z	17.4 120.6		17.3	120.7	55.	В.	0.	18.9	127.3		50.	5.	19.8	125.5	50.	78.	15.	0.0	0.0	0.	~0.	0.
112006Z	17.8 128.4		17.7	128.4	60.	6.	0.	19.1	126.6		43.		20.0	124.8	50.	126.	20.	0.0	9.0	Ø.	-0.	0.
1120122	18.3 128.0			128.1	60.	8.	0.	19.4	126.2		48.		20.2	123.9	60.	178.	40.	0.0	0.0	0.	-0.	0.
112010Z	18.3 127.4			127.6	60.	11.	0.	19.1	125.6		27.	20.	0.0		0.	-0.	0.	0.0	0.0	0.	-0.	0.
112900Z	18.3 126.7			126.7	50.	12.		16.3	125.1		135.	5.	0.0	0.0	ø.	-0.	ø.	0.8	0.0	ø.	-0.	0.
1129 0 6Z	18.5 126.4				45.	19.		17.9	125.3		13.	10.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1129122	18.6 126.1			126.4	45.	29.	0.	17.7	125.5		8.	10.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	ø.
112918Z	18.7 125.8		17.8	126.1	40.	57.	ø.	0.0	0.6		-0.	8.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ø.	-8.	0.
113000Z	18.5 125.6		18.5	125.5	35.	6.	0.	0.0	0.6	0.	-0.	ø.	0.0	0.0	ø.	-0.	0.	0.0	0.0	Ø.	-0.	0.
1 13006Z	18.0 125.5		18.1	125.6	30.	8.	0.	0.0	0.8	0.	-0.	ø.	0.0	0.0	Θ.	-0.	0.	0.0	0.0	0.	-0.	0.
113012Z	17.6 125.4	20	17.6	125.2	20.	11.	0.	0.0	0.6	9.	-8.	9.	0.0	0.0	e.	-0.	0.	0.0	0.0	٥.	-0.	8.

	ALL	FORECAS	ITS		TYPHO	ONS WHIL	E OVER	35 KTS
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	15.	94.	246.	394.	8.	0.	0.	0.
AVG RIGHT ANGLE ERROR	8.	56.	162.	353.	٥.	0.	0.	0.
AVG INTENSITY MAGNITUDE ERROR	0.	16.	35.	44.	0.	0.	0.	ø.
AVG INTENSITY BIAS	0.	16.	35.	44.	8.	ð.	0.	0.
NUMBER OF FORECASTS	16	11	7	4	P	А	R	P

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1615. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

7. KNOTS

TROPICAL STORM RUTH
FIX POSITIONS FOR CYCLONE NO. 22

S SITE
PGTU PGTU PGTU PGTU PGTU PGTU PGTU PGTU
S

14	218447	8.8N 145.4E	PCN 6	T0.5/0.5 /S0.8/26HRS		PGTW
* 15	210841	9.6N 145.1E	PCN 6			PGTW
* 16	210951	9.8N 144.8E	PCN 6			PGTW
* 17	211732	10.1N 144.1E	PCN 6	T1.5/1.5 /D0.5/26HRS		PGTW
* 18	211900	10. IN 143.8E	PCN 6		ULCC FIX ULCC FIX ULCC FIX MLCC FIX MLCC FIX MLCC FIX MLCC FIX EXP LLCC EXP LLCC INIT OBS	PGTW
* 19	212231	10.2N 143.3E	PCN 5		ULCC FIX	PGTW
* 28	226666	10.7N 142.9E	PCN 6		ULCC FIX	PGTW
* 21	220380	11.2N 142.6E	PCN 6	T1.5/1.5 /D1.0/23HRS	ULCC FIX	PGTW
	220600	11.3N 140.8E	PCN 6		ULCC FIX	PGTW
* 23	221266	11.0N 140.5E	PCH 6		MLCC FIX	PGTU
	221688	18.9N 141.1E	PCN 6	T1.8/1.5 /W0.5/24HRS		PGT⊎
	221886	10.9N 140.9E	PCN 6			PGTW
	222100	18.7H 148.5E	PCN 6			PGTW
	230000	9.0N 140.5E	PCN 4			PGTW
	230300	9.5N 140.1E	PCN 6	T2.5/2.5 /D1.0/24HRS		PGTW
	238685	9.5N 139.6E	PCN 5			PGT₩
	231200	9.0N 140.9E	PCN 6		51.00 1 1 50 E	PGTW
	232147	9.1N 139.4E	PCN 5		EXP LLCC	PGTW
	240000	8.5N 139.8E	PCN 4	T1.0/2.8 /W1.5/21HRS	EXP LLCC	PGTW
	240300	8.5N 139.5E	PCH 4		EXP LLCC	PGTW PGTW
	241937	7.8N 138.6E	PCN 6	T1.5/1.5	INIT OBS	PGTU
	242306 250600	8.1N 136.8E 8.7N 136.2E	PCN 6 PCN 6			PGT⊍ PGTW
7 30 37		9.2N 135.BE	PCN 6			PGTW
	251200	9.9N 135.5E	PCN 6			PGTU
	251600	11.7N 134.5E	PCN 6		ULCC FIX	PGTU
	251825	12.3N 132.2E	PCN 5	T2.8/2.8 /D8.5/24HRS	ALCC FIN	PGTW
	268600	11.8N 132.4E	PCN 6	12.0/2.0 / DO.3/2-41K3		
	261299	14.5N 132.2E	PCN 6		ULCC FIX ULCC FIX INIT OBS ULCC FIX ULCC FIX	PGTW
	261600	14.5N 130.5E	PCN 6		ULCC FIX	PGTW
44		15.0N 129.9E	PCN 6		ULCC FIX	PGTU
45	270000	15.5N 129.5E	PCN 6	T1.5/1.5	INIT OBS ULCC FIX	PGTW
46	270300	15.6N 129.6E	PCN 6	T1.5/1.5	ULCC FIX	PGTW
47		15.7N 129.2E	PCN 6			PGTW
49	270900	15.6N 128.8E	PCH 6			PGTW
49	270956	16.1N 129.4E	PCN 6			PGT⊌
58	271200	16.6N 129.3E	PCN 6			PGTW
51	271688	17.1N 128.8E	PCN 6		ULCC FIX	PGTW
52	271988	17.3N 128.7E	PCN 6			PGTW
53	272855	17.5N 128.6E	PCN 6			PGTW
54		17.5H 128.4E	PCN 6			PGTU
55		17.6N 128.6E	PCH 4	T3.5/3.5 /D2.0/27HRS		PGTW
	288688	17.9N 128.5E	PCH 6			PGT₩
57		17.9N 120.7E	PCN 5			PGTW
58	288988	18.0N 128.2E	PCN 4			PGTW
59	290935	18.1N 128.3E	PCN 4			PGTW
50	291840	19.3N 128.4E	PCN 4	T3.5/3.5	INIT OBS	PGTW
61		18.3N 128.2E	PCN 3			RPMK
	281200	18.2N 128.2E	PCN 6			PGTW
	281688	18.3N 127.7E	PCN 4			PGTU
	2818 00 2821 00	18.3N 127.5E	PCN 4 PCN 6			PGTW PGTW
65	282320	18.3N 127.2E 18.1N 126.9E	PCN 5			PGTW
66 67	282328	18.1N 126.9E	PCN 5	T2.5/2.5	INIT OBS	RODN
68	290300	18.3N 126.3E	PCN 4	T3.8/3.5 /W0.5/24HRS	INTI ODS	PGTW
69	298632	18.6N 126.4E	PCN 1	13.0/3.3 / Wg.3/24/183		PGTW
	290900	18.8N 126.2E	PCN 6			PGTW
	291018	18.3N 125.7E	PCN 6	T2.8/3.8-/W1.5/24HRS		PGTW
	292155	18.2N 125.6E	PCN 3			PGT⊎
73		19.2N 125.6E		T2.6/2.0	INIT OBS EXP LLCC	RPMK
74		18.3N 125.7E	PCH 3			PGTW
75	388628	17.8N 125.7E	PCN 3	T1.5/2.5-/U1.5/27HRS	EXP LLCC	PGTW
76	301138	17.8N 125.8E	PCN 5			RODH

AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL		09S 16LP	MAX-SFC-LIND VEL/BRG/RHG		FLT-I			ACCR NAV/M		EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
NG. 1 2 3 4 4 5 6 7 8 9 18 11 12 12 13 14 14	222345 230624 2306624 23030 232335 250522 272340 200532 200612 202310 290531 290602 292632	9.2H 148.2E 9.3H 148.7E 9.3H 148.7E 9.2H 148.7E 8.5H 138.9E 8.4H 138.9E 8.9H 137.6E 17.7H 128.4E 17.7H 128.4E 17.9H 128.8E 18.2H 126.8E 18.2H 126.8E 18.2H 126.8E 18.2H 126.8E	1500FT 1500FT 1500FT	3133 1 3133 1 1 3029 3030 3032 3032 3075	16LP 1884 1888 1881 1885 1885 1885 1885 1885	38 228 38 38 288 68 28 188 89 18 380 68 25 248 45 68 028 24 18 68 238 38 45 388 18 45 248 13 46 318 98	120 090 110 120 160 230 020 150 140 140 125 250 200	20 32 30 20 14 17 44 67 74 43 43	399 320 320 310 130 240 270 340 230 330 360 350	RNG 135 120 90 35 45 31 40 45 23 55 53 60 120	8 1 7 9 25 2 15 1 5 10 10 6 6 12	9 8 6	SHAPE CÎRCULAR ELL IPTICAL	32	+28 +26 +25 +25 +27 +26 38 +27 +25 33 +15 +13 +12 +29 +28 +25 29 +25 +24 +24 38 +14 +18 +18 +16 + 7 +17 -16 + 6 +14 +15 + 6	3 4 4 5 5 6
15 16 17	292359 300539 300753	18.6N 125.6E 18.1N 125.6E 17.8N 125.4E	1500FT 1500FT 700MD	3152 1 3146 1	1006 1005 1009	45 278 25 35 278 48 5 138 38	616 650 110	37 : 15 (288	35 128 98		7 6 6			+26 +25 31 +28 +25 38 +14 +14 + 6	12 13 13

NOTICE - THE ASTERISKS (*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

THE SECOND PROPERTY OF THE PRO

TROPICAL STORM SPERRY BEST TRACK DATA

	BEST TRAC	ж	WA	RHING				24	HQUR F				48 H	OUR F				72 F	OUR F		
					EK	RORS				ER	RORS				ER	RORS				ERI	RORS
MD/DA/HR	POSIT	MIND	POSIT	WIND	DST	WIND	P	TIZO	WINI	DST	WIND	Pt	DSIT	WIND	DST	MIND	POS	SIT	WIND	DST	WIND
1262182	16.2 132.2	30	16.5 132.1	30.	19.	Ð.	16.9	129.5	50.	179.	0.	17.0	127.8	65.	362.	30.	0.0	0.0	ø.	-0.	0.
1203062	16.1 131.7	40	16.2 131.4	45.	18.	5.	16.0	129.4	55.	223.	10.	16.8	127.7	65.	325.	35.	0.0	0.0	0.	-0.	0.
1203062	17.3 131.4	45	16.3 131.2	45.	61.	0.	16.2	129.5	55.	208.	15.	0.0	0.0	0.	-0.	0.	9.0	0.0	ø.	-0.	0.
12 0 312Z	18.0 131.9	55	16.6 132.0	40.	84.	-15.	15.7	131.1	30.	130.	-5.	0.0	8.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.
12 6 316Z	18.6 132.4	50	16.9 132.4	40.	66.	-10.	16.1	132.2	30.	58.	-5.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.
1204002	17.8 132.8	45	18.0 132.9	55.	13.	10.	17.1	133.2	60.	96.	30.	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	0.
12 848 6Z	17.1 133.0	48	17.1 132.8	55.	11.	15.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.
1284122	16.5 133.2	35	16.5 132.9	50.	17.	15.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	₽.
1264192	16.0 133.2	35	16.1 132.6	45.	35.	10.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	0.
1295997	15.5 133.3	38	15.6 133.3	30.	6.	A	9 . B	9.9	ι α	-8	-		B B		-0	n.	A 8	B B	ρ.	-B	Α.

	ALL	FORECAS	TS		TYPHO	DNS WHIL	E OVER	35 KTS	
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR	
AVG FORECAST POSIT ERROR	33.	149.	343.	8.	0.	0.	0.	ø.	
AVG RIGHT ANGLE ERROR	19.	91.	237.	0.	0.	0.	0.	0.	
AVG INTENSITY MAGNITUDE ERROR	8.	11.	33.	0.	8.	ø.	0.	0.	
AVG INTENSITY BIAS	3.	8.	33.	0.	8.	8.	0.	e.	
NUMBER OF FORECASTS	10	6	2	0	8	Ð	B	8	

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 350. NM
AVERAGE SPEED OF TROPICAL CYCLONE IS 6. KNOTS

TROPICAL STORM SPERRY FIX POSITIONS FOR CYCLONE NO. 23

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
				5 Tol. 11 Tol. 12 Tol.	0011 20	01.12
* 1	381888	9.4N 141.5E	PCN 6			PGTW
- ·	382133	9.4N 148.2E	PCN 5			RPHK
* 3	302237	9.8N 140.6E	PCN 6		ULCC FIX	PGTU
- 4	011600	13.2N 135.5E	PCN 6	T1.0/1.0	INIT OBS ULCC FIX	PGTW
5	Ø11996	13.0N 135.7E	PCN 6	1110-110	ULCC FIX	PGTU
6	612166	13.4N 135.6E	PCN 6		OLCO I IA	PGTW
ž	812215	12.5N 134.9E	PCN 5		ULCC FIX	PGTW
è	020114	13.8N 134.6E	PCN 5	T1.5/1.5	INIT DBS ULCC FIX	PGTW
9	020554	15.7N 133.9E	PCN 6			PGTW
18	628986	15.8N 133.1E	PCN 6			PGTW
11	021054	16.2N 133.2E	PCN 6			PGTW
12	821288	16.4N 132.9E	PCN 6			PGTW
13	821688	16.5H 132.5E	PCN 6	T2.5/2.5 /D1.5/24#R\$		PGTW
14	621845	16.7N 132.0E	PCN 5			PGTW
15	022651	16.4N 131.6E	PCN 5			PGTW
16	822324	16.2N 131.7E	PCN 5	T2.5/2.5	INIT 08S	RPMK
17	622334	16.0N 131.5E	PCN 5			PGTW
18	63865 4	16.0N 131.4E	PCN 3	T3.0/3.0 /D1.5/24HRS		PGT⊎
19	636366	16.1N 131.3E	PCN 6			PGTW
28	838452	16.6N 131.5E	PCN 5			PGTW
21	030542	16.6N 131.1E	PCN 5	T3.0/3.0	INIT OBS ULCC FIX	RODH
22	031200	18.3N 132.4E	PCN 6			PGTW
23	031335	17.9N 131.8E	PCN 5		ULCC FIX	PGTW
24	631600	18.1N 132.2E	PCN 6	T3.5/3.5-/D1.0/24HRS		PGTW
25	031027	18.2N 131.9E	PCN 5			RPMK
26	031827	10.3N 132.5E	PCN 5			PGT₩
27	032030	18.5N 132.7E	PCN 5			PGTW
28	032313	18.5N 132.7E	PCN 5			PGTW
* 29	032313	18.9N 133.2E	PCH 5		ULCC FIX	RODN
30 31	848834 848388	18.5N 132.7E 17.2N 132.8E	PCN 5 PCN 6	T3.0/3.0 /S0.0/24HRS		PGTU
32	040530	17.2N 132.9E	PCN 5			PGTW PGTW
33	041010	17.3N 132.6E	PCN 4		ULCC 18.7N 136.8E	PGTW
* 34	841288	17.2N 132.1E	PCN 6		ULCC 19.0N 137.4E	PGTW
35	041815	16.2N 133.4E	PCN 5		ULCC 15.0M 137.4E	RPMK
36	042150	15.5N 132.8E	PCH 5			PGTU
37	042251	15.6N 132.9E	PCN 3	T1.5/2.5 /W1.5/23HRS		PGTU
38	858888	15.4N 132.9E	PCN 4	11.0-E10 / WILO-ESHK3		PGTW
39	656614	15.5N 133.0E	PCN 3			PGTU
40	656386	14.9N 132.8E	PCN 4		EXP LLCC	PGTW
	9-9-30-0	1-1-27 13E. DE	ron =		EW. FFFF	ruiw

AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700M9 HGT	OBS MSLP	MAX-SFO VEL/BRG			FLT-LVI VEL/BRI				EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
3 4 5 * 6 7	030021 030910 031203 032243 040058 041137 042138 042336	16.5N 131.5E 18.0N 131.7E 18.1N 132.0E 17.9N 132.7E 16.8N 133.1E 17.9N 132.6E 15.8N 133.2E 15.6N 133.3E	700MB 700MB 700MB 700MB 700MB 700MB 1500FT	3120 3091 3049 3119 3135 3149	1009 1004 1006 1012 1009 1010	65 168 35 198 70 368 40 358 40 028 40 298	12 0 20 70 60	180 250 200 020 030 270 048 020	44 090 33 200 80 070 65 360 41 360 16 200 31 020 33 290	92 9 12 9 20 9 50 9 58 9 90	10 25 14 8 9 1 20 2	8 3 1 0	CIRCULAR	35	+10 + 9 + 9 +11 +10 +10 + 7 +11 + 8 +15 + 9 +26 +25 +10 + 4 +29 +29 +23 +28 +29 +24	2 3 3 4 5 6 6

PER 18 18 18 18 18 18 18 18 18 18 18 18 18	N.S. CATCHARL CONTROL	3534550		7.5.5	المناد			, i i	1	350.5	1646	1		الأمل	4	दर्ग हैं						
P4.4																						
Fai																						
1 .													1									
								TR	OPICAL	STOR	H THE	LMA										
									BEST	TRACK	DHIR											
							_						•									
13		BEST TRA	CK	u	W HING	ERR	ORS		24 1	HOUR F		ST RORS		48 1	HOUR F	FORECA ER	st Rors		72 H	OUR F	ORECA: ERI	ST RORS
15	HD/DA/HR	POSIT	MIND	POSIT	WIND		MIND	PO	SIT	WIND	DST		P	OSIT	MINI			POS		WIND		WIND
12.7	121412Z 12141 8 Z	9.6 142.8	28 1 28	0.0 6.0	6.	-0.	8.	9.8	0.8	8.	-0. -8.	₽.	0.0	9.8	6.	-8. -8.	0.	8.8	0.0 0.0	0.	-8. -8.	Ø.
123	121 586 Z	18.8 139.8	25	8.8 B.8	B.	-0. -8.	8.	0.0 8.8	8.8	8. 8.	-8.	B.	8.8	8.8	8.	-8.	8.	9.8	8.8	8.	-8.	8.
	121506Z	10.0 130.5	25	0.8 0.0	ē.	-a.	8.	0.8	0.0	0.	-0.	8.	0.0	0.0	8.	-0.	ø.	0.0	0.0	ø.	-0.	ø.
	1215122	11.4 137.2	30	8.8 8.8	0.	-8.	8.	0.0	0.6	0.	-0.	ð.	0.8	0.0	0.	-0.	8.	0.0	8.8	₽.	-0.	Ð.
	12151 8 Z	11.8 135.9	35	0.0	€.	-0.	0.	8.8	8.8	0.	-0.	0.	0.0	8.8	0.	-0.	0.	8.8	0.0	Ø.	-0.	0.
	1216 06 Z	12.2 134.0	40 1		40.	6.	0. 1		131.2	50 .	171.	5.	13.4	128.5	65.	555.	40.	0.0	0.0	e.	-0.	Ø.
<i>(</i> 25)	121 606 Z	12.9 133.9		2.8 134.6	48.	8.	-5. I		132.3	68.	63.	15.	15.5	138.8	68.	589.	45.	0.0	9.6	9.	-0.	Ð.
12.5	1216122	13.5 133.6		3.8 133.7	45.	19.	0. 1		129.7		236.	20.	0.0	0.0	ø.	-0.	ø.	0.0	9.0	ø.	-0.	8.
	121619Z 1217 00 Z	14.1 133.4	50 1 55 1	4.6 133.1 4.6 133.2	45. 55.	35.	-5. 1		129.4 131.9		328. 313.	25. 30.	0.0	0.0	0. 0.	-0. -0	Ø. Ø.	0.0 0.0	0.0 0.0	v.	-0. -8.	8. 8.
	1217 8 62	15.2 133.3		4.6 133.2 5.6 133.0	55.	30.	10. I		131.3		499.	30. 48.	8.8	6.0 0.0	ø. Ø.	-0. -0.	0. 8.	0.0	0.0	ø.	-0.	Ø.
l`	1217122	16.1 133.8		5.6 133.2	50.		15.	8.8	8.8	9.	-D.	Ð.	8.9	9.8	e.	-0.	Ð.	9.8	8.8	Đ.	-0.	Ð.
	1217182	16.8 135.1		6.2 133.3	45.		15.	8.8	8.8	8.	-8.	8.	0.0	0.0	ø.	-6.	e.	0.0	8.8	ø.	-0.	ē.
	121886Z	17.3 137.2		7.7 136,4	35.		10.	0.0	9.0	ē.	-8.	0.	0.0	0.0	ē.	-0.	e.	0.0	0.0	ø.	-0.	8.
24	1219062	17.6 140.8	15 1	7.7 140.0	20.	6.	_	0.6	8.8	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-8.	0.

	ALL	FORECAS	TS		TYPHO	ONS WHIL	E OVER	35 KTS
	LIRNG	24-HR	48-HR	72-HR	LIRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	32.	268.	572.	0.	8.	0.	0.	Ð.
AVG RIGHT ANGLE ERROR	16.	151.	239.	ð.	0.	0.	0.	ø.
AVG INTENSITY MAGNITUDE ERROR	7.	23.	43.	8.	0.	0.	0.	0.
AVG INTENSITY BIAS	5.	23.	43.	ē.	8.	Ð.	0.	ø.
NUMBER OF FORECASTS	10	6	2	0	9	Ð	8	8

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1165. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 13. KNOTS

TROPICAL STORM THELMA
FIX POSITIONS FOR CYCLONE NO. 24

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
1	138988	7.2N 151.8E	PCN 6		ULCC FIX	PGTW
ż	132821	18.9N 145.9E	PCN 6		acad (IV	PGTW
3	140035	6.9N 148.4E	PCN 6	T8.5/8.5	INIT DBS ULCC FIX 11.8N 150.3	PGTW
4	140300	6.8N 148.8E	PCN 6		ULCC 11.9N 149.2E	PGTW
5	140500	12.2N 148.5E	PCN 6		ULCC FIX	PGTW
6	140955	9.5N 145.3E	PCN 6		ULCC FIX	PGTW
7	141600	9.5N 142.1E	PCN 6		ULCC FIX	PGTW
8	141753	9.6N 141.4E	PCN 6			PGTW
9	142100	10.1N 139.9E	PCN 6			PGTW
10	142235	9.0N 140.2E	PCN 5			PGTW
* 11	150015	7.7N 140.8E	PCN 5	T1.0/1.0 /D0.5/24HRS		PGTW
12	1 506 37	10.0N 138.5E	PCN 6		ULCC FIX	PGTW
13	150840	11.0N 137.7E	PCN 6		ULCC FIX	PGTW
14	150933	11.2N 137.4E	PCN 6		ULCC FIX	PGTW
15	151200	11.5N 136.9E	PCH 6		ULCC FIX	PGTW
16	151255	11.5N 136.5E	PCH 6		ULCC FIX	PGTW
17	151600	12.5N 135.8E	PCN 6	T2.5/2.5	INIT OBS	PGT⊎
18	151922	12.5N 135.0E	PCN 5			PGTW
19	152120	12.4N 134.6E	PCN 5			PGTW
28	160136	12.1H 134.4E	PCN 5	T2.5/2.5 /D1.5/25HRS		PGTW
21	160300	12.4H 134.3E	PCH 6			PGTW
22	160625	13.0H 134.0E	PCH 3			PGTW
23	168988	13.3N 133.8E	PCN 6			PGTW
24	161001	13.4N 133.8E	PCN 6			PGTW
25	161200	13.8N 133.7E	PCH 6			PGTW
26	161417	13.9H 133.5E	PCH 6		ULCC FIX	PGTW
27	161600	14.4N 133.3E	PCN 6	T3.8/3.8 /D8.5/24HRS	18 CC C19	PGTW
28 29	161989	14.6N 133.1E 14.7N 133.0E	PCN 6 PCN 5		ULCC FIX	PGTU
* 38	162859	15.4H 132.9E	PCN 6			PGTW PGTW
31	162332	14.9H 133.2E	PCH 6	T3.8/3.8 /D8.5/22HRS		PSTW
32	162333	14.5N 133.6E	PCN 3	T3.8/3.8 /D1.8/22HRS		RPMK
33	178388	15.5N 133.4E	PCN 6	13.0/3.0 /DI.0/22NRS		PGTW
34	178613	15.6N 133.2E	PCN 5			PGTW
35	178613	15.5N 133.2E	PCN 5	T2.8/2.8	INIT OBS	RODH
-		1991EF				20011

36	178939	15.9N 133.3E	PCN 5		PGTW
37	171031	16.1N 133.5E	PCN 5		₽GTW
38	171356	15.8N 133.7E	PCN 5		PGTW
39	171600	15.8N 135.2E	PCH 6		PGT₩
48	171857	16.2N 135.6E	PCN 5	T2.8/3.0 /W1.0/27HRS	PGT⊎
41	172311	17.7N 136.BE		T1.5/2.5 /U1.5/24HRS	PGTW
42	188056	17.9N 137.0E	PCN 5		PGTW
43	180300	18.1N 139.1E	PCH 6	ULCC FIX	PGTW

AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT		MAX-SFC- VEL/BRG/			FLT-L\ VEL/8I				EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) DUT/ IN/ DP/SST	MSN NO.
3 4 5			700MB 700MB 700MB 1500FT	3028 3045 3067	996 990 1006 1005 1004	45 138 50 270 55 210 25 280 20 040	9 3 70	170 020	24 2	90 13 70 125 30 11	5 4 15	2 10 10	CIRCULAR	12	+24 +26 +25 28 +18 +16 +18 +14 +14 + 7 +25 +26 +23 +28 +28 +22	3 4 4 5 7

TROPICAL DEPRESSION 02 BEST TRACK DATA

	BEST TRA	CK		U F	IRH ING	ED	RORS		24 H	IOUR F		ST RORS		48 H	OUR F	ORECA	ST RORS		72 H	IOUR F		ST RORS
MD/DA/HR	POSIT	MIND	, pr	DSIT	MIND	DST	MIND	Pf	SIT	WIND			Pf	DSIT	WIND		CHIM	Pno	SIT	MIND	DST	MIND
0830062	18.1 186.8		0.0	0.0	8.	-8.	W1.12	0.0	0.0	B.	_6	0.	0.0	0.8	0.	-0.	WIND	0.0	0.8	0.	-0.	0.
683812Z	10.7 185.7	20	0.0	0.0	ø.	-8.	0.	0.0	0.0	8.	-0.	8.	8.8	8.8	8.	-8.	8.	8.8	8.8	8.	-0. -8.	ø.
683818Z			8.0				Ð.	0.0	0.0		-0.				D.				0.0			
				0.0		-0.				0.		ø.	0.0	0.0		-0.	Ø.	0.0		0.	-0.	0.
003100Z	11.7 183.6		0.0	0.0		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
693106 Z	12.0 182.7	25	0.0	0.0		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
683112 2	12.4 181.9	30	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
083 118Z	12.7 181.2	30	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
898 188Z	13.0 180.7	30	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
898186Z	13.3 180.3	30	13.3	179.8	30.	29.	ø.	14.8	177.3	35.	118.	10.	15.9	175.7	40.	276.	20.	0.0	0.0	0.	-0.	0.
090 112Z	13.5 180.1	30	13.5	179.5	30.	35.	ø.	14.8	177.9	35.	99.	10.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
890118Z	13.8 179.9	30	13.8	179.9	30.	8.	ø.	16.1	179.2	35.	227.	10.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Ø.
090200Z	13.8 179.4	30	14.0	179.1	30.	21.	0.	15.2	177.5	30.	230.	10.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
090206Z	13.6 178.9	25	13.7	180.5	30.	93.	5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
898212Z	13.2 178.3	25	9.8	8.8	0.	-0.	0.	9.9	9.8	8.	-0.	Ð.	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	ø.
696218Z	12.8 177.3	25	0.0	0.0		-0.	ø.	0.0	0.0	ø.	-0.	ø.	9.0	0.0	ø.	~0.	ø.	0.0	0.0		-0.	ø.
690300Z	11.5 176.5		0.0	0.0		-0.	ē.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ŭ.
698386Z	11.3 175.7		0.0	0.0		-0.	ø.	0.0	0.0	ø.	-0.	Đ.	0.0	0.0	ø.	-0.	ē.	0.0	0.0	ø.	-0.	ø.

	ALL	FORECAS	ITS		TYPHO	ONS WHIL	E OVER	35 KTS
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	36.	168.	276.	ø.	0.	0.	0.	0.
AVG RIGHT ANGLE ERROR	17.	117.	205.	ð.	0.	0.	0.	Ø.
AVG INTENSITY MAGNITUDE ERROR	1.	10.	20.	0.	0.	0.	0.	0.
AVG INTENSITY BIAS	1.	10.	20.	ð.	0.	0.	0.	0.
NUMBER OF FORECASTS	5	4	1	8	0	0	Ø	Ð

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 773. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 8. KNOTS

TROPICAL DEPRESSION TD02C FIX POSITIONS FOR CYCLONE NO. 2

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
1	300546	10.2N 173.9U	PCN 6	T1.5/1.5	INIT OBS ULAC 10.1N 174.3W	KGWC
2	301826	11.1N 174.8W	PCN 6			KGWC
3	381845	11.0H 177.5W		T1.5/1.5	INIT OBS	PHNL
4	362145	11.8N 176.7U		T2.0/2.0 /D0.5/03HRS		PHNL
5	382345	12.8N 176.6W		T2.0/2.0 /S0.0/02HRS		PHNL
6	310245	12.8N 177.0W		T2.5/2.5 /D0.5/03HRS		PHNL
7	310520	12.4N 177.9U	PCN 6	T2.5/2.5 /D1.8/24HRS		KGWC
8	310545	12.6N 177.8W		T2.5/2.5 /S0.0/03HRS		PHNL
9	311145	12.8N 177.4W		T2.5/2.5 /S0.0/06HRS		PHNL
18	311540	12.2N 177.9W	PCH 6		ULAC 12.9N 178.3W	KGWC
11	311665	12.2N 177.6W	PCN 6			KGWC
12	311015	12.5N 178.2W		T3.0/3.0 /D0.5/06HRS		PHNL
13	312345	12.6N 180.0W		T3.0/3.0 /S0.0/06HRS		PHNL
14	010000	12.8N 179.7W	PCN 6	T2.0/2.8	INIT OBS	PGTW
15	010249	13.1N 179.6W	PCN 6	T2.5/2.5 /S0.0/24HRS	ULAC 13.2N 179.8W	KGWC
16	010300	13.1N 179.9U	PCN 6		ULCC FIX	PGT₩
17	010545	12.3N 179.7E		T3.0/3.0 /S0.0/06HRS		PHNL
10	010600	12.9N 179.6W	PCN 6			PGTW
19	0 1 0 9 0 0	13.1N 179.8W	PCN 6			PGTW
× 28	811145	11.5N 176.5E		T3.0/3.0 /S0.0/06HRS	ULCC 12.0N 179.0W	PHNL
* 21	011200	13.3N 178.6E	PCN 6	T1.5/1.5	INIT OBS	PGTW
22	011534	13.5N 179.7W	PCN 6		ULAC 12.7N 178.8W	KGWC
23	011600	13.5N 179.3W	PCN 6			PGT₩
24	011744	13.5N 179.2W	PCN 6			KGWC
25	611745	13.8N 179.9E		T2.5/3.0 /WB.5/06HRS		PHNL
26	611 906	14.8N 179.4W	PCN 6			PGTW
27	012100	14.0N 179.6W	PCN 6			PGTW
28	812345	13.6N 179.6E		T2.0/2.5 /W0.5/06HRS		PHNL
29	820000	13.9N 179.9E	PCH 6			PGTW
38	020236	13.4N 179.8W	PCH 6	T2.8/2.5 /W0.5/24HRS		KGWC
31	020300	13.6N 179.4E	PCN 6	T1.5/1.5	INIT OBS	PGTW
32	020600	13.7N 179.5E	PCN 6			PGTW
33	020 624	13.1N 179.7W	PEN 4		EXP LLCC	KGWC

34	821521	12.9N 177.8E	PCN 4			KGWC
					EXP LLCC	KGWC
* 36	030224	13.9N 176.1E	PCN 4	TB.5/1.5 /U1.5/24HRS	ULAC 13.5N 179.2E	KGWC
37	030300	12.BN 175.9E	PCN 4			PGT⊎

TROPICAL CYCLONE 81-83 BEST TRACK DATA

	BES	T TRA	CK		WA	RHING		RORS		24 H	OUR FO		ST RORS		48 H	IOUR FO		ST RORS		72 H	OUR F		ST RORS
MO DAZHR	POS	ΙŤ	WIND	P	DSIT	MIND			PO:	SIT	MIND	DST		PO	SIT	MIND	DST	– –	P05	iT.	WIND		MIND
888988Z	22.0	65.6	25	0.0	0.0	0.	-0.	9.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.8	0.		0.
090906 Z	21.5	64.2	25	0.0	0.0	8.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.
6669 12Z	21.2	62.9	30	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	9.	-0.	0.	0.0	0.0	0.	-0.	0.
0 80918Z	20.9	61.7	48	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
88 1 88 8 Z	20.8	60.2	45	21.5	61.0	40.	61.	-5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.8	0.0	0.	-0.	0.
0 81006Z	20.7	58.9	40	20.2	58.5	45.	37.	5.	9.9	0.0	0.	-0.	Ð.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
081012Z	20.4	57.6	35	19.9	58.2	30.	45.	-5.	0.8	8.8	9.	-0.	Ð.	0.0	0.0	0.	-0.	B.	0.0	0.0	0.	-0.	0.

	ALL	FORECAS	ITS		TYPHOONS WHILE OVER 35 KTS						
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR			
AVG FORECAST POSIT ERROR	48.	0.	0.	0.	0.	₽.	0.	0.			
AVG RIGHT ANGLE ERROR	35.	ø.	0.	8.	0.	8.	0.	0.			
AVG INTENSITY MAGNITUDE ERROR	5.	0.	0.	8.	0.	a.	0.	0.			
AVG INTENSITY BIAS	-2.	0.	0.	0.	0.	ø.	0.	ø.			
NUMBER OF FORECOSTS	3	A	A	Ā.	ā	a	a	a			

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 461. NM
AVERAGE SPEED OF TROPICAL CYCLONE IS 13. KNOTS

TCB1A
FIX POSITIONS FOR CYCLONE NO. 1

SATELLITE FIXES

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CONTIENTS	SITE
1 2	898248 891857	22.0N 65.1E 21.2N 63.3E	PCN 5 PCN 5	T1.5/1.5	INIT OBS ULAC 21.3N 64.4E ULAC 22.0N 63.5E	KGWC KGWC
3	691456	21.4N 62.5E	PCN 5			KGWC
4	100149	21.0N 59.2E	PCN 6	T1.0/1.0 /U0.5/24HRS	ULAC 20.3N 59.6E	KGWC
5	100414	19.7N 58.8E	PCN 5		ULRC 20.6N 54.2E	KGWC
6	101045	19.7N 58.4E	PCN 5		ULAC 20.4N 59.3E	KGUC
7	101429	21.4N 57.6E	PCN 5		ULAC 21.1N 58.1E	KGWC

TROPICAL CYCLONE 82-83 BEST TRACK DATA

	BES	T TRAC	CK		ша	RHING				24 H	IOUR FI	DREC'A!	5 T		48 H	nou≢ ro	RE; A	5.7		72 H	ICUP FO	PECAS	<u>5</u> T
							ER	RORS				ER	RORS				ER	POPS				ERI	POP5
MO/DA/HR	POS	IT	WIND	PC	SIT	WIND	DST	WIND	PO	SIT	MIND	DST	WIND	POS	, 1 T	WIND	DST	MIND	PO	511	WIND	DST	WIN:
100100Z	18.2	88.6	25	0.0	0.0	0.	-0.	Ø.	0.0	8.6	0.	-0.	₩.	€.€	0.0	8 .	- e	₽	P. P	₽.8	₽.	- ft ,	₽.
100106Z	18.1	88.3	25	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	8.	0.0	0.0	0.	- O .	€.	r: e	0.0	₿.	P	0.
1001122	10.1	87.9	30	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Ð.	9.6	0.0	0.		€.	0.8	e.e	0.	θ.	е.
100119Z	18.0	87.6	30	0.0	0.0	0.	-0.	0.	0.0	8.8	0.	-0.	Θ.	0.0	0.0	₿.	· 6	₽.	₫.₿	e. e	₽.	ē.	f.
100200Z	18.0	87.2	30	0.0	0.0	Ø.	-0.	В.	0.0	8.0	0.	-0.	₩.	0.0	0.0	0.	- 0 .	₿.	0.0	8.6	₿.	₽.	0.
100206Z	17.9	86.7	30	0.0	0.0	0.	-8.	0.	0.0	0.0	0.	-8.	₽.	0.0	0.0	0.	- 8 .	₿.	0.0	0.0	Ø.	- € .	₿.
1002122	17.9	86.2	30	0.0	0.0	0.	-0.	0.	0.0	0.0	8.	-0.	₽.	0.0	0.0	₿.	- 0 .	₿.	M. 0	P. H	Ø.	- P.	0.
1002182	17.9	85.7	35	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	₽.	0.0	0.0	₩.	-●.	₿.	0.0	0.0	Ø.	- P	0.
1003002	17.9	85.2	45	18.3	85.3	45.	25.	0.	19.8	84.8	3 5.	162.	- 10 .	0.8	0.0	₽.	~ 0 .	Ø.	11.0	0.0	₿.	0.	0.
1003062	17.9	84.8	50	18.6	85.1	50.	45.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	₩.	- 0 .	₿.	6.6	8.9	₿.	-0.	₽.
1003122	17.9	84.3	50	18.3	84.4	50.	25.	0.	0.0	0.0	0.	-0.	Ð.	0.0	8.8	₿.	~ 0 .	₿.	0.0	0.0	0.	0.	0.
100318Z	18.0	83.3	50	18.2	83.2	50.	13.	0.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0 .	-0.	₿.	Ø.0	0. i	0.	0.	0.
1004002	18.5	82.3	45	10.6	82,4	45.	8.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	₩.	- 0 .	₽.	0.0	Ø.9	₿.	-0.	ø.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 I'TS						
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48 HP	72-HR			
AVG FORECAST POSIT ERROR	23.	162.	0.	0.	₽.	Ð.	₿.	●.			
AVG RIGHT ANGLE ERROR	25.	114.	0.	0.	Ð.	0.	₿.	₿.			
AVG INTENSITY MAGNITUDE ERROR	0.	10.	0.	0.	0.	₿.	₽.	Ð.			
AVG INTENSITY BIAS	0.	~10.	0.	0.	0.	0.	Ð.	₽.			
NUMBER OF FORECASTS	5	1	0	ð	8	Ð	Ð	B			

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 370. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

CONTRACTOR CONTRACTOR

5. KNOTS

TC02B-83 FIX POSITIONS FOR CYCLONE NO. 2

SATELLITE FIXES

FIX NO.	TIME (2)	FIX POSITION	ACCRY	DYORAK CODE	COMMENTS	SITE
1	272348	16.0N 94.0		T1.0/1.0	INIT DBS	KGWC
2	282327	15.7N 90.5	E PCN 6	T1.0/1.0 /S0.0/24HRS	ULAC 15.0N 91.6E	KGWC
3	300047	18.1N 89.5	E PCN 5	T1.5/1.5 /D0.5/25HRS		KGWC
4	010026	18.9N 88.8	E PCN 5	T2.5/2.5+/D1.0/24HRS	ULAC 18.1N 87.7E	KG₩C
5	010600	17.5N 8B.8	E PCN 6			PGTW
* 6	010831	18.3N 86.5	E PCN 5		ULAC 17.8N 86.7E	KGWC
* 7	011306	18.0N 86.4			ULAC 17.7N 86.2E	KGWC
* 8	920000	17.7N 85.1	E PCN 6			PGTW
9	020005	17.8N 87.5	E PCN 4	T3.0/3.0 /D0.5/24HRS		KGWC
10	020151	17.7N 86.8	E PCN 3			KG₩C
11	020300	18.0N 86.7	E PCN 6	T2.5/2.5	INIT OBS	PGTW
12	020600	17.8N 86.0	E PCN 6		ULCC 17.6N 83.3E	PGTW
* 13	021245	17.4N 85.2	E PCN 5		ULAC 17.2N 83.8E	KGWC
14	022103	17.9N 85.5	E PCN 6			KGWC
15	022344	18.3N 85.3	E PCN 6	T3.5/3.5 /D0.5/24HRS	ULAC 17.4N 84.3E	KGWC
16	030130	18.3N 85.1	E PCN 6			KGWC
17	030948	18.0N 84.8	E PCN 3		ULAC 17.2N 83.4E	KGWC
18	031200	10.2N 83.7	E PCN 6			PGTW
19	031224	10.0N 83.9	E PCN 6		ULAC 17.8N 83.3E	KGUC
20	031410	18.0N 93.6	E PCN 4		ULAC 17.7N 83.2E	KGWC
21	031600	19.3N 82.9	E PCN 6		ULCC FIX	PGTW
22	832188	18.5N 82.0	E PCN 6		ULCC FIX	PGTW
23	032233	18.6N 82.6	E PCN 6		ULAC 17.6N 82.0E	KGWC

TROPICAL CYCLONE 83-83 BEST TRACK DATA

	BES	T TRA	CK		ua.	RHING				24 H	OUR F	ORECA	IST		48 H	OUR F	ORECA	IST		72 H	OUR FO	RECAS	ST
							ER	RORS				ER	RORS				ER	RORS				ERI	RORS
MD/DA/HR	POS	IT	UIND	PO	SIT	MIND	DST	UIND	PO	SIT	WINI) DS1	MIND	PO	SIT	WIND	DST	THIM T	PO	SIT	WIND	DST	MIND
1185862	9.6	91.2	20	8.8	8.8	Ð.	-8.	0.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ø.	-0.	Θ.
118512Z	18.4	91.2	20	0.0	0.0	Ð.	-0.	Ð.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	8.	-0.	0.
1105182	11.2	91.0	20	0.6	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	8.	0.0	0.0	0.	-0.	0.
110600Z	12.3	90.1	25	8.8	8.8	Θ.	-0.	θ.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
110606Z	13.3	89.3	25	8.8	8.6	8.	-0.	0.	8.8	8.8	Ð.	-0.	Ð.	0.0	0.0	0.	-0.	₽.	0.0	0.0	Ð.	-0.	0.
118612Z	14.3	88.7	30	0.6	8.8	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.6	0.	-0.	0.
1106182	14.9	88.5	38	8.8	0.0	٥.	-0.	0.	0.0	0.0	ø.	-0.	0.	0.0	0.0	Ø.	-0.	0.	0.0	0.0	0.	-0.	0.
110700Z	15.6	88.4	30	0.0	0.0	0.	-8.	0.	0.0	0.0	8.	-0.	8.	0.0	0.0	0.	-0.	8.	0.0	0.0	0.	-0.	0.
1107062	16.0	88.7	35	0.0	8.9	0.	-0.	0.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	8.	0.0	0.0	0.	-0.	0.
1107122	16.3	89.0	35	16.2	88.8	35.	13.	ø.	18.8	89.4	45,	52.	Ø.	21.3	89.6	50.	132.	-5.	0.0	0.0	0.	-0.	0.
110719Z	16.6	89.3	40	17.0	89.0	35.	30.	-5.	18.9	89.8	45,	42.	-5.	20.9	90.0	50.	174.	15.	0.0	0.0	0.	-0.	0.
110000Z	16.9	89.6	40	17.5	89.5	40.	36.	8.	19.4	90.1	50.	33.	-5.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.
110006Z	17.4	90.0	45	16.B	89.9	40.	36.	-5.	10.4	91.1	50.	127.	-5.	8.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
110912Z	17.9	90.3	45	17.4	89.3	40.	65.	-5.	19.2	90.0	40.	189.	-15.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1 188 18Z	18.5	98.4	50	17.8	89.9	50.	51.	0.	19.B	90.2	50.	210.	15.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	θ.
110900Z	19.0	90.5	55	18.4	90.1	55.	43.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
110906Z	20.5	90.8	55	19.9	90.7	55.	36.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
11 09 12Z	21.8	91.9	55	21.7	91.1	50.	45.	-5.	8.6	8.8	8.	-0.	8.	0.0	9.8	9.	-0.	0.	0.0	9.9	Θ.	-0.	0.
110910Z	22.5	92.6	35	22.8	93.8	35.	69.	0.	0.0	0.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS						
	WRNG	24-HR	48-HR	72-HR	WRNG	24-i iR	48-HR	72-HR			
AVG FORECAST POSIT ERROR	42.	109.	153.	0.	0.	Ð.	0.	0.			
AVG RIGHT ANGLE ERROR	21.	35.	67.	0.	0.	0.	0.	0.			
AVG INTENSITY MAGNITUDE ERROR	2.	Θ.	10.	0.	a .	₽.	0.	Ø.			
AVG INTENSITY BIAS	-2.	-3.	5.	в.	Θ.	Ø.	0.	0.			
NUMBER OF FORECASTS	10	6	2	0	0	0	9	8			

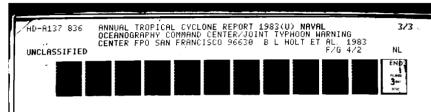
DISTANCE TRAVELED BY TROPICAL CYCLONE IS 988. NM

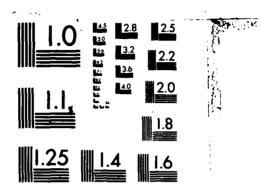
AVERAGE SPEED OF TROPICAL CYCLONE IS

8. KNOTS

TC832 FIX POSITIONS FOR CYCLONE NO. 3

FIX		FI					
NO.	(Z)	POSIT	'IDN	ACCRY	DVORAK CODE	CONTENTS	SITE
			•				
1	050947	10.2N	91.2E	PCN 6	T1.0/1.0	INIT 085 ULAC 11.5N 89.7E	KGWC
2	0520 10	11.6N	90.8E	PCH 6		ULAC 12.6N 59.5E	KGWC
3	060935	14.2N	89.9E	PCN 5	T2.0/2.0 /D1 0/24HRS	ULAC 14.2N 87.8E	KGWC
4	0 62220	15.4N	98.4E	PCN 5			KGWC
5	07 000 0	15.9N	88.1E	PCN 6		ULCC FIX	PGTW
6	070056	15.7N	88.4E	PCN 5			KGWC
7	070216	15.9N	88.5E	PCN 5			KGWC
8	070300	15.7H	88.1E	PCH 6			PGT₩
* 9	070600	15.5N	87.6E	PCN 6			PG~3
* 10	070900	15.5N	87.3E	PCN 6			PG≀⊎
11	070923	15.BN	68.8E	PCN 5	T3.0/3.0 /D1.0/24HRS		KGWC
12	071154	16.4H	89.8E	PCN 6		ULAC 16.IN 89.2E	KGWC
* 13	071200	15.6N	87.1E	PCH 6			PGTW
14	071315	16.5N	89.1E	PCN 6		ULAC 16.4N 89.6E	KGWC
* 15	071800	16.7N	87.5E	PCN 6			PGTW
16	672166	16.9N	89.3E	PCH 6			PGTW
17	872287	16.6N	90.1E	PCN 5			KGWW
10	000000	17.3N	89.7E	PCN 6			PGTW
19	080035	16.4H	98.4E	PCH 5		ULAC 17.6N 89.6E	KGUC
20	698154	16.4N	90.1E	PCN 5		ULAC 17.4N 89.4E	KGUC
21	000300	16.6N	89.8E	PCN 6	73.8.2.8	WIT 000	PGTW
22	090600	17.1N 17.2N	89.2E	PCN 6	T3.0/3.0	INIT OBS	PGTW
23 24	888998 888918	17.4N	89.3E	PCN 6 PCN 5	T3 F 4 F 40 F 40 NO	ULAC 17.5N 89.2E	PGTW KGWC
25	081200	17.49	89.5E 89.3E	PCN 5	T3.5/3.5 /D0.5/24HRS	ULHC 17.3N 89.2E	PGTW
26	891315	17.2N	90.0E	PCN 5			KGWC
27	091600	17.2N	89.7E	PCN 6	T3.0/3.0	INIT OBS	PGTW
28	081800	17.8N	89.9E	PCN 6	13.0/3.0	1411 082	PGTW
29	682166	18.1N	90.3E	PCH 6			PGTU
30	082155	18.8N	90.5E	PCN 6			KGWC
31	690000	18.4N	98.4E	PCN 6		ULCC FIX	PGTW
32	090014	18.7N	91.2E	PCN 6		ULAC 19.0N 91.0E	KGUC
33	090133	19.1N	90.4E	PCN 5		OLDE 13.01 31.05	KINC
33	020133	12.10	70 . ME	FUN 3			Kindu





MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

34	090300	18.98	90.5E	PCN 6		PĠTW
35	090600	20.4N	90.9E	PCN 6		PGTU
36	690838	21.2N	91.3E	PCN 5	T4.0/4.8 /D0.5/24HRS	KGWC
37	091200	21.7N	91.1E	PCN 6		PGTW
38	091253	22.1N	92.8E	PCN 5		KG UC
39	091600	22.4N	93.2E	PCN 6		PGTW
40	091660	22.9N	94.6E	PCN 6		PGTW

APPENDIX I CONTRACTIONS

ACCRY	Accuracy	GOES	Geostationary Operational Environmental Satellite
ACFT	Automated Data Processing	HATTRACK	Hurricane and Typhoon Tracking (Steering) Program
AFGWC	Air Force Global Weather Central	нст	Height
AIREP	Aircraft Weather Report(s) (Commerical and Military)	нрас	Mean of XTRP and CLIM Techniques (Half Persistence and Climatology)
ANT	Antenna	HR	Hour(s)
AOR	Area of Responsibility	HVY	Heavy
APRNT	Apparent	ICAO	International Civil Aviation
APT	Automatic Picture Transmission		Organization
ARWO	Aerial Reconnaissance Weather Officer	INIT INJAH	Initial North Indian Ocean Component
ATT	Attenuation	Thom	of TYAN
AVG	Average	INST	Instruction
AWN	Automated Weather Network	IR	Infrared
BPAC	Blended Persistence and Climatology	KM	Kilometer(s)
BRG	Bearing	KM/HR	Kilometer(s) per Hour
CDO	Central Dense Overcast	KT	Knot(s)
CI	Cirriform Cloud or Cirrus	LLCC	Low-level Circulation Center
	also Current Intensity (Dvorak)	LVL	Level
CINCPAC	Commander-in-Chief Pacific AF - Air Force, FLT - Fleet (Navy)	M	Meter(s)
CLD	Cloud	M/SEC	Meter(s) per Second
CLIM	Climatology	MAX	Maximum Milliham (a)
CLSD	Closed	MB	Millibar(s)
CM	Centimeter	MET	Meteorological
CNTR	Center	MIN	Minimum
CPA	Closest Point of Approach	MOHATT	Modified HATTRACK
csc	Cloud System Center	MOVG	Moving
CYCLOPS	Tropical Cyclone Steering Program	MSLP	Minimum Sea Level Pressure
	(HATTRACK and MOHATT)	MSN	Mission
DEG	Degree(s)	NAV	Navigational
DIAM	Diameter	NEDN	Naval Environmental Data Network
DIR	Direction	NEDS	Naval Environmental Display Station
DMSP	Defense Meteorological Satellite Program	NEPRF	Naval Environmental Prediction Research Facility
EL	Elongated	NESS	National Environmental Satellite Service
ELEV	Elevation	NET	Near Equatorial Trough
EXP	Exposed	NM	Nautical Mile(s)
FI	Forecast Intensity (Dvorak)	N/O	Not Observed
FLT	Plight	NOAA	National Oceanic and Atmospheric
FNOC	Fleet Numerical Oceanography Center		Administration
FT	Feet (Foot)	NOCC	Naval Oceanography Command Center
GMT	Greenwich Mean Time	NWOC	Naval Western Oceanography Center

NR	Number	TC	Tropical Cyclone
NRL	Naval Research Laboratory	TCARC	Tropical Cyclone Aircraft Reconnaissance Coordinator
NTCM	Nested Tropical Cyclone Model	TCFA	Tropical Cyclone Formation Alert
OBS	Observation(s)		
OTCM	One-way (Interactive) Tropical	TCM	Tropical Cyclone Model
	Cyclone Model	TD	Tropical Depression
PACOM	Pacific Command	TDO	Typhoon Duty Officer
PCN	Position Code Number	TIROS	Televison Infrared Observation Satellite
PSBL	Possible	ТS	Tropical Storm
PTLY	Partly	TY	•
QUAD	Quadrant		Typhoon
RADOB	Radar Observation(s)	TYAN	Typhoon Analog Program
RECON	Reconnaissance	TYFN	Western North Pacific Component (Revised) of TYAN
RNG	Range	TUTT	Tropical Upper-Tropospheric Trough
RT	Right	ULAC	Upper-level Anticyclone
SAT	Satellite	VEL	Velocity
SFC	Surface	vis	Visual
SLP	Sea Level Pressure	VSBL	Visible
SPOL	Spiral Overlay	WESTPAC	Western (North) Pacific
SRP	Selective Reconnaissance Program	WMO	World Meteorological Organization
STNRY	Stationary	WND	Wind
SST	Sea Surface Temperature	WRNG(S)	Warnings
ST	Subtropical	WRS	Weather Reconnaissance Squadron
STR	Subtropical Ridge	XTRP	Extrapolation
STY	Super Typhoon	z	Zulu Time (Greenwich Mean Time)
TAPT	Typhoon Acceleration Prediction Technique		(Glechwich rican line)

APPENDIX II

DEFINITIONS

BEST TRACK - A subjectively smoothed path, versus a precise and very erratic fix-to-fix path, used to represent tropical cyclone movement.

CENTER - The vertical axis or core of a tropical cyclone. Usually determined by wind, temperature, and/or pressure distribution.

CYCLONE - A closed atmospheric circulation rotating about an area of low pressure (counterclockwise in the Northern Hemisphere).

EPHEMERIS - Position of a body (satellite) on space as a function of time; used for gridding satellite imagery. Since ephemeris gridding is based soley on the predicted position of the satellite, it is susceptible to errors from vehicle pitch, orbital eccentricity, and the oblateness of the earth.

EXPLOSIVE DEEPENING - A decrease in the minimum sea level pressure of a tropical cyclone of 2.5 mb/hr for 12 hrs or 5.0 mb/hr for six hrs (ATR 1971).

EXTRATROPICAL - A term used in warnings and tropical summaries to indicate that a cyclone has lost its "tropical" characteristics. The term implies both poleward displacement from the tropics and the conversion of the cyclone's primary energy sources from release of latent heat of condensation to baroclinic processes. The term carries no implications as to strength or size.

EYE - "EYE" is used to describe the central area of a tropical cyclone when it is more than half surrounded by wall cloud.

FUJIWHARA EFFECT - An interaction in which tropical cyclones within about 700 nm (1296 km) of each other begin to rotate about one another. When intense tropical cyclones are within about 400 nm (741 km) of each other, they may also begin to move closer to each other.

MAXIMUM SUSTAINED WIND - Maximum surface wind speed averaged over a one-minute period of time. Peak gusts over water average 20 to 25 percent higher than sustained winds.

RAPID DEEPENING - A decrease in the minimum sea level pressure of a tropical cyclone of 1.25 mb/hr for 24 hrs (ATR 1971).

RECURVATURE - The turning of a tropical cyclone from an initial path toward the west or northwest to a path toward the northeast.

RIGHT ANGLE ERROR - The distance described by a perpendicular line from the best track to a forecast position. (See Figure 4-1).

SIGNIFICANT TROPICAL CYCLONE - A tropical cyclone becomes "significant" with the issuance of the first numbered warning by the responsible warning agency.

SUPER TYPHOON/HURRICANE - A typhoon/hurricane in which the maximum sustained surface wind (one-minute mean) is 130 kt (67 m/sec) or greater.

TROPICAL CYCLONE - A non-frontal low pressure system of synoptic scale developing over tropical or subtropical waters and having a definite organized circulation.

TROPICAL CYCLONE AIRCRAFT RECONNAISSANCE COORDINATOR - A CINCPACAF representative designated to levy tropical cyclone aircraft weather reconnaissance requirements on reconnaissance units within a designated area of the PACOM and to function as coordinator between CINCPACAF, aircraft weather reconnaissance units, and the appropriate typhoon/hurricane warning center.

TROPICAL DEPRESSION - A tropical cyclone in which the maximum sustained surface wind (one-minute mean) is 33 kt (17 m/sec) or less.

TROPICAL DISTURBANCE - A discrete system of apparently organized convection--generally 100 to 300 nm (185 to 556 km) in diameter--originating in the tropics or subtropics, having a non-frontal migratory character, and having maintained its identity for 24 hours or more. It may or may not be associated with a detectable perturbation of the wind field. As such, it is the basic generic designation which, in successive stages of intensification, may be classified as a tropical depression, tropical storm or typhoon (hurricane).

TROPICAL STORM - A tropical cyclone with maximum sustained surface winds (one-minute mean) in the range of 34 to 63 kt (17 to 32 m/sec) inclusive.

TROPICAL UPPER-TROPOSPHERIC TROUGH (TUTT) - "A dominant climatological system, and a daily synoptic feature, of the summer season over the tropical North Atlantic, North Pacific and South Pacific Oceans," from - Sadler, J.C., Feb. 1976: Tropical Cyclone Initiation by the Tropical Upper-Tropospheric Trough (NAVENVPREDRSCHFAC Technical Paper No. 2-76).

TYPHOON/HURRICANE - A tropical cyclone in which the maximum sustained surface wind (one-minute mean) is 64 kt (33 m/sec) or greater. West of 180 degrees longitude they are called typhoons and east of 180 degrees they are called hurricanes. Foreign governments use these or other terms for tropical cyclones and may apply different intensity criteria.

VECTOR ERROR - The distance described by a straight line from the forecast position to the position at verification time as found on the best track. (See Figure 4-1).

WALL CLOUD - A organized band of cumuliform clouds immediately surrounding the central area of a tropical cyclone. The wall cloud may entirely enclose or only partially surround the center.

APPENDIX III NAMES FOR TROPICAL CYCLONES

Column 1	Column 2	Column 3	Column 4
ANDY	ABBY	ALEX	AGNES
BESS	BEN	BETTY	BILL
CECIL	CARMEN	CARY	CLARA
DOT	DOM	OINAH	DOYLE
ELLIS	ELLEN	ED	ELSIE
FAYE	FORREST	FREDA	FABIAN
GORDON	GEORGIA	GERALD	GAY
HOPE	HERBERT	HOITA	HAZEN
IRVING	IDA	IKE	IRMA
JUDY	JOE	JUNE	JEFF
KEN	KIM	KELLY	KIT
LOLA	LEX	LYNN	LEE
MAC	MARGE	MAURY	MAMIE
NANCY	NORRIS	NINA	NELSON
OWEN	ORCHID	OGDEN	ODESSA
Pamela	PERCY	PHYLLIS	PAT
ROGER	RUTH	ROY	RUBY
SARAH	SPERRY	SUSAN	SKIP
TIP	THELMA	THAD	TESS
VERA	VERNON	VANESSA	VAL
WAYNE	WYNNE	WARREN	WINONA

NOTE:

Source: USCINCPACINST 3140.1 (series)

APPENDIX IV

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APPENDIX V PAST ANNUAL TYPHOON/TROPICAL CYCLONE REPORTS

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20. ABSTRACT (Continue on reverse side if necessary and	A identify by block number	ircraft reconnaissance
Annual publication summarizing the tropical cyclone season in the w		lone season in the western
North Pacific, Bay of Bengal and Arabian Sea. A brief narrative is given or		
each significant tropical cyclone including its best track. All reconnais-		
sance data used to construct the	best tracks a	re provided. Forecast verifi-
cation data and statistics for t the JTWC and recent NOCC/JTWC pu		
2.52 02.52 2.52 2.00 NOO, 01 NO	-DIIGGEIONS ALC	oricity discussed.

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Block 19, (Continued)

Dynamic tropical cyclone models Typhoon analog model Tropical cyclone steering model Climatology/persistence techniques

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